#### The SEAMAN's

# Daily Assistant,

BEING

A Short, Easy, and Plain Method

OF KEEPING

## A JOURNAL at SEA;

In which are contain'd

### RULES,

SHEWING

How the Allowances for Lee-way, Variation, Heave of the Sea, Set of Currents, &c. are to be made, and to Correct the Dead-Reckoning by an Observation, in all Cases: And also all the Tables that are any ways necessary for the Seaman's Use in keeping a Journal.

By THOMAS HASELDEN,
Late Teacher of the MATHEMATICKS in the
ROYAL-NAVY.

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1608/5280



#### TO THE

# READER.



AVING been educated in the Theory of Navigation, almost from my Childhood, and having had about Sixteen Years Experience of the practical Part (at Sea) both in the Merchants Service, and also as Teacher of the Mathematicks in the Royal-Navy; and baving in the

Course of that Time made a general Observation, that there are Numbers of Seamen who would gladly keep a Reckoning, bad they any Short, Easy, and Plain Method to do it by, but are deterr'd from it by the want of such a Thing: And also that there are many who have thrown their Money away to little or no Purpose, by going to School to some Masters (of which Sort there are too many) that they have only got a Smattering of the Theory, and a few Terms of Art by Rote, which enables them to talk in such a manner to deceive those that go to learn of them; by having never been at Sea, cannot know any Thing of the Practice.

Therefore for the Use of such in particular, and of all other Seafaring Men in general, I have written the following Treatise, in which I think I have inserted all the Rules, and all the Tables with their Uses, that are necessary to be used in any Case at Sea: And also particular Rules for keeping a Journal, with the manner of Correcting the Dead-Reckoning by an Observation, either for one Day, or for a longer Time; the first of which, viz. Correcting for one Day, has been treated of by several Authors; but the latter, viz. Correcting for a longer Time; I know has been barely mentioned in several, but not particularly explain'd in any Author at all I believe, at least in none that I have A 2 Read,

#### To the READER.

Read; And for that Reason I have done it in the Journal at the latter end of this Book, it being absolutely necessary for every Man that keeps a Reckoning to know it, because they are more likely to be out in their Reckoning, when they have been some Days without an Observation, then when they have one every Day, and consequently more likely to have Occasion to correct for three or four Days, than for a single One.

I have not begun this Book with Arithmetic, as most of the Books on this Subject do, because I think, that if any Person has had so little Education as not to be capable of Adding, Subtracting, Multiplying and Dividing, he will hardly be able to make any Progress, either in Arithmetic or Navigation, by the help of Books alone, without the Assistance of a Master (so that I think putting such Things into Books of this kind, serve only to enhance the Price, and are of no Service to the Reader.) And now having given an Account of the Reasons that enduced me to publish this Book (which I hope, and are pretty well assured, will be found the most useful Book of its kind, now in Print) for the daily Practice at Sea, I have nothing more to add, but to beg the Readers kind Acceptance of my Endeavours.

And am,

Their humble Servant,

Thomas Haselden.



#### THE

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A

# TABLE

OF

DIFFERENCE of LATITUDE

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And as far as 300 Miles DISTANCE.

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26	26.6		76	75.9		126	125.8		176	175.8		226	225.7	11.8	276	275.6	14.4
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32	32.0	01.7	83		04.3	32	132.8		83	181.7	09.5		231.7			281,6	
33	24.0	8.10	84		04.4	34	133.8	07.0		183.7	00.6		232.7	12.2	84	283.6	14.0
35	35.6	01.8	85	84.9		35	134.8	07.1		184.7			234.7	S. T	85	284.6	14.0
36	_	019	86	85.0	W. C.	136	135.8		186	185.7		/	235.7	-		285.6	
37		01.9	87	86.9			136.8			186.7			235.7	12.4	87	286.6	15.0
38	37.0	02.0	88	87.9	04.6	38	137.8	07.2	88	187.7	09.8	1 38	137.7	12.5	88	287.6	15.1
39	38.9	62.C	89	88.9	04.7	39	1 38.8	07.3		188.7	109.9	39	238.7	12.5	89	288.6	15.1
40	39,9	02.1	90	89 9	04.7	40	139.8	07.3	90		09,9		239.7			289.6	
41		02.1	91	90.9	04.8	141	140.8	07.4		190.7	10.0		240.7	-	-	290.6	-
42	41.9	02.2	52	91.9	04.8	42	141.8	07.4		191.7			241.7			291.6	
43	42.9	02.2		92 9		43	142.8	07.5	93	192.7	10.1	43	242.7	12.7		292.6	
44	43.9	02.3			04.9		143.8	07.5		193.7			243.7		94	293.6	15.4
45	44.9	02.4	-	-	050		144.8		-	-	-	45	244.7	12.8	95	294.6	15.4
46		02.4	96	95.9	05.0	146	145.8	.07.6	196		10.3	246	245.7			295.6	
47		02.5		96.9	05.1	47	146.8	07.7		196 7		47	246.7			296.6	
		62.5		97.9	05.1	48	147,8	07.7	98	197.7	10.4	48	247.7	13.0	98	297.6	15.6
49	JAX.0	02.6			05.2						10.4			13.0	99	298.6	15.6
	140.9	100 6	11200	100 0	OF	III EC	IIAO -										
50	19.9	02,6 Lat	1	99.9 Dep			Dep.	-		199.7 Dep		250	249.7 Dep	-		299.6 Dep	

for 87 Deg.

### Difference of Latitude and Departure for 4 Deg.

													D 1	0.4	7-4	D-1	D:4		10-
D	ALL.	al	De	111	Mic	Lat	Dep	Dift	Lat	Dei		Lat	-	-	Lat		Ditt	Lat	Deb
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		30					03.7	03	102.8	07.2	53	152.6	10,7		202.5			252.4	
1		4.0					03,8	04		07.2	54	153.6	10 7		203.5	1		253 4	
		5.0			55	54 9	03.8	95	104	07.3	55	154.6	10 8	-	204.5	-	-	254.4	
-	6 0	6.0	20	4	50	_	03.9	106	105	107.4	156	155.6			205.5			255.4	
1	-	7.0			57	- 2	04 0	07		07.5	57		10.9		206.5			256.4	
		80		211	58		04 0	08		7 27.5	58	157	11.0		207.5			257.4	
1	9 0	9.0	00	.6	59		04 1			7 07.6	1 .	158.	11.1			14.6		258.4	
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1	1	11.0	00	5	61		04.3	111		7 07.7		160		11	210.		100	260.4	
1	2	12.0	00	18.	62		04.3	12		7 07.8		161			212.	14.		261.4	
11	3	13,0	00	.9	63		8 04.4			7 07.9		163			213.			4 263	
1		14			64		8 04.5			7 07.9		164.						5 264	
1	5	15	01	.0	65	-	04.5		-	7 08 0	-	-	_		-	5 15.1		6 265	
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	22		90		72	71.	8 05.	1 2	1 122	.7 08.	1 2	3 172	.6 12.	1 2	1 12 Acres 10 Acres 10	5 15.5			3 19.0
	23		90		7		8 05.		1 123	.7 08.		4 173	.6 12.	1 2		5 15.6			3 19.1
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	33			2.3	8		.8 05.			2.7 09.	311		6 12			4 16,	2	3 282	-3 19.7
	34			2.4	8		.8 05.			1.7 09.	311		1.6 12			4 26.			1.3 19.9
	35			02.4		_	.8 05			4.7 09	-1  -		1.6 12			4 16.	_		
	36			02.5			.8 06			5.7 09	311		5.6 13		36 235		4 2	87 -97	.3 19.9
	37	136	.9	02.6			5.8 06			6.7 09,	311	87 18	6.6 13	,0	28 12	14 16.	6	88 28	7.3 20.0
	38	37	1.9	02.7		8 8	7.8 06	1	13	7.7 09		89 18	8.5 12	.2	30 23	3.4 16.	7	80 285	8.3 20.1
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19   18   901.7   70   69   68.7   66.0   19   118.5   10.4   70   169   14.8   20   219.2   19.1   70   269.0   23.5   2			211					1					1 2					
20	19						19		-	69	168.4	2.3	1				268.c	23.4
21       20.9       01.8       71       70.7       06.2       121       120.5       10.5       171       170.4       14.9       221       220.2       19.2       271       270.0       23.6         23       21.5       02.0       73       72.7       06.4       23       122.5       10.7       73       172.3       15.1       23       222.2       19.4       73       272.0       23.8         24       23.9       02.1       74       73.70.6.5       24       123.5       10.8       74       173.3       15.1       23       222.2       19.4       73       272.0       23.8         25       24.9       02.3       76       76.7       06.6       126       125.5       11.0       176       175.3       15.3       226       225,1       19.7       77       77       276.9       27.2       22.1       19.7       77       77       77.6       76.7       26.8       11.7       11.0       176       175.3       15.3       226       225,1       19.7       77       77.2       27.2       22.1       19.2       27.2       226.1       19.7       77       27.2       226.1       19.7       27.2 </td <td></td> <td>19 901</td> <td>.7</td> <td>70</td> <td>69.7</td> <td>06.1</td> <td>20</td> <td>119.5</td> <td>10.4</td> <td>70</td> <td>169 4</td> <td>14.8</td> <td>20</td> <td>219.2</td> <td>19.1</td> <td>70</td> <td>269.0</td> <td>23.5</td>		19 901	.7	70	69.7	06.1	20	119.5	10.4	70	169 4	14.8	20	219.2	19.1	70	269.0	23.5
22       21.9   01.9   72   71.7   06.3         22   121.5   10.6         72   171.5   15.0         22   221.2   19.3         72   271.0   23.7         73   72.7   272.0   23.8         73   72.7   273.0         23.8   22.5   10.7         73   172.3   15.1         23   222.2   19.4         73   72.7   272.0   23.8         74   73.7   06.5         24   123.5   10.8         74   173.3   15.1         24   22.3   19.5         74   72.0   23.8	2000 4 100	20.9 01	.8	71	70.7	06.2	121	120,5	10.5	171	170.4	14.9	221	220.2	19.2	271	270.0	23.6
24       23.9       02.1       74 73.7 06.5       24 123.5 10.8       74 173.3 15.1       24 223.1 19.5       74 273.0 23.8         25       24.9 03.2       75 74.7 06.5       25 124.5 10.9       75 174.3 15.2       25 226 225.1 19.7       75 74.0 23.9         27       26.9 02.4       77 76.7 06.7       27 126.5 11.0       176 175.3 15.3       226 225.1 19.7       77 77 275.9 24.1         28       27.9 02.4       78 77.7 06.8       28 11.7 5 11.1       78 177.3 15.5       28 227.1 19.8       78 276.9 24.1         29       28       90.2.5       79 78 7 06.9       28 11.2 5 11.2       79 178.3 15.6       29 228.1 19.9       79 277.9 24.3         30       29.9 02.6       80 79.7 07.1       30 129.5 11.3       80 179.3 15.7       30 229.1 20.0       80 278.9 24.4         31       30.9 02.7       81 80.7 07.1       131 130.5 11.4       181 180.3 15.7       30 229.1 20.0       80 278.9 24.4         32       31.9 02.8       82 81.7 07.2       32 131.5 11.5       82 181.3 15.8       32 231.1 20.2       82 280.9 24.5         33       39.0 02.7       83 82.7 07.2       33 133.5 11.6       83 183.3 15.9       33 232.1 20.2       82 82.9 24.5         34       33.9 03.6       84 83.7 07.2       33 133.5 11.7       84 183.3 16.0	22	21.901	.9	72	71.7	06,3	22			72	171.3	15,0	22	221.2	19.3		271.0	23.7
25         24.9         03.2         75         74.7         06.5         25         124.5         10.9         75         174.3         15.2         25         224.1         19.6         75         274.0         23.9           26.9         02.3         76         75.7         06.6         126         125.5         11.0         176         175.3         15.3         226         225,1         19.7         77         275.9         24.0           28         27.9         02.4         75         77.7         06.8         28         127.5         11.1         78         177.3         15.5         28         227.1         19.8         776.9         275.9         24.2           29         28.9         9.2.6         80         79.7         9.7         30         129.5         11.3         18.1         177.3         15.5         28         227.1         19.9         277.9         24.3           31         30.9         22.7         81         80.7         97.2         32         131.5         11.5         82         181.3         15.7         231         230.1         20.1         281         279.9         24.4           32 <t< td=""><td>1</td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td>7 1 1 1</td><td>1000</td><td></td><td></td><td></td></t<>	1						-							7 1 1 1	1000			
26       25.9       02.3       76       75.7       06.6       126       125.5       11.0       176       175.3       15.3       226       225.1       19.7       275.0       24.0         27       26.9       02.4       77       76.7       06.8       28       127.5       11.1       78       177.3       15.5       28       227.1       19.8       78       276.9       24.2         29       28.9       02.6       8c       79.7       07.2       30       129.5       11.3       8o       179.3       15.7       30       229.1       28.1       19.7       77.9       277.9       24.2       277.9       28.7       277.9       24.2       228.1       19.9       79       277.9       24.2       229.1       28.1       19.9       79       277.9       24.2       229.1       28.1       29.0       28.1       28.1       29.1       28.1       28.1       29.1       28.1       28.1       29.1       28.1       28.1       29.1       28.1       28.1       29.1       28.1       28.1       29.2       28.1       29.2       28.1       29.2       28.1       29.2       28.1       29.2       28.1       29.2																		
27   26.9   02.4   77   76.7   06.7   27   126.5   11.0   77   176   3   15.4   27   226.1   19.7   77   275.9   24.1   28   27.9   02.4   78   77.7   06.8   28   127.5   11.1   78   177.3   15.5   28   227.1   19.8   78   276.9   24.2   29.9   02.6   80   79.7   07.6   30   129.5   11.3   80   179.3   15.7   30   229.1   20.0   80   278.9   24.4   31.3   30.9   02.7   81   80.7   07.1   31   130.5   11   41   180.3   15.7   30   229.1   20.0   80   278.9   24.4   31.3   31.9   02.8   83.2.7   07.2   33   131.5   11.5   83   181.3   15.8   32   231.1   20.1   281   279.9   24.4   33.9   03.6   84   83.7   07.3   34   133.5   11.7   84   183.3   16.0   34   233.1   20.4   84   282.9   24.7   35   34.9   03.1   86   85.7   07.5   36   135.5   11.8   38   31.5   31.5   32.3   32.1   20.3   83   28.9   24.8   37.9   03.3   88   87.7   07.5   38   137.5   12.0   88   187.3   16.2   37.9   38.9   03.4   89.8   87.7   07.7   38   137.5   12.0   88   187.3   16.2   38   237.1   20.5   286   284.9   24.9   38.9   38.7   07.8   39   138.5   12.1   39   188.3   16.3   38   237.1   20.5   38   285.9   25.1   39   39.8   03.5   90.8   97.7   77.8   141   140.5   12.3   191   190.3   16.6   241   240.1   21.0   291   289.9   25.5   44.8   30.3   93.8   03.8   93.9   03.6   08.2   44   143.5   12.5   94   193.3   16.9   42.4   241.1   21.1   93   290.9   25.4   44.8   03.9   95.9   96.0   08.5   47   146.4   12.6   95   194.3   17.0   45   244.1   21.2   94   299.9   25.8   47.8   04.9   99.9   96.0   08.5   49   148.4   13.0   99   198.2   17.3   49   248.1   21.7   99   297.9   25.8   49   248.8   247.9   248.8   247.1   21.6   98   296.9   25.8   49   248.8   247.9   248.8   247.1   21.6   98   296.9   25.8   49   248.8   247.9   248.8   247.1   21.6   98   296.9   25.8   49   248.8   247.9   248.8   247.1   21.6   98   296.9   25.8   49   248.8   247.9   248.8   247.1   21.6   98   296.9   25.8   49   248.8   247.9   248.8   247.1   21.6   98   296.9   25.8   49   248.8   247.9   248.8   247.1   21.6   248.8   247.1   2	_		- 11	_	_	-	-		-			_	_	-	-			_
28       27.9   02.4   72   77.7   06.8   28   127.5   11.1   78   177.3   15.5   28   227.1   19.8   78   276.9   24.2   29   28.5   11.2   79   178.3   15.6   19   228.1   19.9   79   277.9   24.3   30   29.9   02.6   80   79.7   07.0   30   129.5   11.3   80   179.3   15.7   30   229.1   20.0   80   278.9   24.4   31.9   02.9   81.8   17.7   32   131.5   11.5   82   181.3   15.8   32   231.1   20.2   82   28.7   07.2   33   132.5   11.6   83   182.3   15.8   32   231.1   20.2   83   281.9   24.6   33   90.3   84   83.7   07.3   34   133.5   11.7   35   14.9   03.1   36.8   84.7   07.5   37   36.5   11.8   36.9   03.1   36.9   03.2   37.9   03.3   38.8   37.7   07.7   38   137.5   11.8   186   185.3   16.2   236   235.1   20.5   286   284.9   24.9   37.9   03.3   38.9   03.4   89.88.7   07.8   39   138.5   11.9   87   186   316.3   37   236.1   20.6   87   285.9   25.0   38.8   37.9   03.3   38.9   03.4   39.8   88.7   07.8   39   138.5   12.1   39.8   39.8   39.5   39.8   39.7   07.8   39   138.5   12.1   39.8   39.8   39.5   39.8   39.7   07.8   39   138.5   12.1   39.8   39.8   39.7   07.8   39.8   39.5   12.2   39.8   39.8   39.7   07.8   39.8   39.5   12.2   39.8   39.		1 2 1	-11															
29       28       9 02.5       79       78       7 06       9       29       128       5 11.2       79       178.3       15.6       29       228,1       19.9       79       277,9       24.3         30       29.9       02.6       80       79.7       07.2       30       129.5       11.3       80       179.3       15.7       231       230.1       20.1       281       277.9       24.4         31       30.9       02.7       81       80.7       07.1       131       130.5       11.4       181       180.3       15.7       231       230.1       20.1       281       279.9       24.4         32       31.9       02.8       81.7       07.2       32       131.5       11.5       82       181.3       15.8       32       231.1       20.2       82       280.9       24.5         33       32.9       02.9       83       82.7       07.3       34       133.5       11.7       84       183.3       16.0       34       233.1       20.4       84       282.9       24.7         35       34.9       03.1       86       85.7       07.5       136       135.5       1																		
30 29.9 02.6 8c 79.7 07.6 30 129.5 11.3 80 179.3 15.7 30 229.1 20.0 80 278.9 24.4 31.3 0.9 02.7 81 80.7 07.1 131 130.5 11.4 181 180.3 15.7 231 230.1 20.1 281 279.9 24.4 31.9 02.8 82 81.7 07.2 32 131.5 11.5 82 181.3 15.8 32 231.1 20.2 82 280.9 24.5 33 132.9 02.9 83 82.7 07.2 33 132.5 11.6 83 182.3 15.9 33 232.1 20.3 83 281.9 24.6 34 33.9 03.0 84 83.7 07.3 34 133.5 11.7 84 183.3 16.0 34 233.1 20.4 84 282.9 24.7 35 34.9 03.1 86 85.7 07.5 136 135.5 11.8 186 185.3 16.1 35 234.1 20.4 85 283.9 24.8 37.9 03.1 86 85.7 07.5 136 135.5 11.8 186 185.3 16.2 236 235.1 20.5 286 284.9 24.9 37 36.9 03.2 87 86.7 07.6 37 136.5 11.9 87 186 3 16.3 37 236.1 20.6 87 285.9 25.0 38 37.9 03.3 88 87.7 07.8 39 138.5 12.1 89 188.3 16.4 38 237.1 20.7 88 286.9 25.1 39 38.9 03.4 89 88.7 07.8 39 138.5 12.1 89 188.3 16.4 39 238.1 20.8 89 287.9 25.1 40. 39.8 03.5 90 89.7 07.8 40 139.5 12.2 90 189.3 16.5 40 239 1 20.9 90 288.9 25.2 41 40.8 03.6 91 90.7 07.8 40 139.5 12.2 90 189.3 16.6 241 240.1 21.0 90 288.9 25.2 44 14.8 03.7 92.9 16.8 24 141.5 12.4 92 191.3 16.7 42 241.1 21.1 92 290.9 25.4 43.8 03.8 94 93.6 08.2 44 143.5 12.5 94 193.3 16.9 44 243.1 21.1 93 291.9 25.5 45 44.8 03.8 94 93.6 08.2 44 143.5 12.5 94 193.3 16.9 44 243.1 21.1 99 290.9 25.4 41.8 03.9 95.94.6 08.3 45 144.4 12.6 95 194.3 17.0 45 244.1 21.1 99 290.9 25.6 45 44.8 03.9 95.94.6 08.5 45 144.4 12.6 95 194.3 17.0 45 244.1 21.1 99 290.9 25.6 45 44.8 03.9 95.94.6 08.5 45 144.4 12.6 95 194.3 17.0 45 244.1 21.1 99 290.9 25.5 45 44.8 04.0 96 95.6 08.4 146.4 12.8 97 196.3 17.1 47 240.1 21.5 99 295.9 25.5 48 47.8 04.2 98 97.6 08.5 47 146.4 12.8 97 196.3 17.1 47 240.1 21.5 99 295.9 25.5 48 47.8 04.2 98 97.6 08.5 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 25.5	1												10000					
31 30.9 02.7 81 80.7 07.1 131 130.5 11 4 181 180.3 15.7 231 230.1 20.1 281 279.9 24.4 31.9 02.8 82 81.7 07.2 32 131.5 11.5 82 181.3 15.8 32 231.1 20.2 82 280.9 24.5 33 32.9 02.9 83 82.7 07.2 33 132.5 11.6 83 182.3 15.9 33 232.1 20.3 83 281.9 24.6 35 34.9 03.1 86 83.7 07.4 35 134.5 11.7 85 184 3 16.0 34 233.1 20.4 85 283.9 24.7 35 34.9 03.1 86 85.7 07.5 136 135.5 11.8 186 185.3 16.2 236 235.1 20.4 85 283.9 24.8 37.9 03.2 87 86.7 07.6 37 136.5 11.9 87 186 3 16.3 37 236.1 20.6 87 285.9 25.0 38 37.9 03.3 88 87.7 07.7 38 137.5 12.0 88 187.3 16.4 38 237.1 20.7 88 286.9 25.1 39 38.9 03.4 89 88.7 07.8 39 138 5 12.1 89 188.3 16.4 39 238.1 20.8 89 287.9 25.1 40.8 03.6 91 90.7 27.5 141 140.5 12.3 191 190.3 16.6 239 120.9 90 288.9 25.2 41 40.8 03.6 91 90.7 27.5 141 140.5 12.3 191 190.3 16.6 239 120.9 90 288.9 25.2 44 14.8 03.7 92 91.6 28.6 42 141.5 12.4 92 191.3 16.7 42 241.1 21.1 92 290.9 25.4 43.8 03.8 94 93.6 08.2 44 143.5 12.5 94 193.3 16.9 44 243.1 21.2 94 292.9 25.5 44.8 03.9 95 94.6 08.3 45 144.4 12.6 95 194.3 17.0 45 244.1 21.3 95 293.9 25.7 46 45.8 04.0 96 95.6 08.5 44 143.5 12.5 94 193.3 17.0 45 244.1 21.3 95 293.9 25.5 47 46.8 04.1 97 96.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.8 47 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.9 48 8.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0	1													11000				
32 31.9 02 8 82 \$1.7 07 2 32 131.5 11.5 82 181.3 15.8 32 231.1 20.2 83 281.9 24.6 33 32.9 02.9 83 82.7 07.2 33 132.5 11.6 83 182.3 15.9 33 232.1 20.3 83 281.9 24.6 35 34.9 03.1 86 84.7 07.4 35 134.5 11.7 85 184 3 16.1 35 234.1 20.4 85 283.9 24.7 35 36.9 03.2 87 86.7 07.5 136 135.5 11.8 186 185.3 16.2 236 235.2 20.5 286 284.9 24.9 37 36.9 03.2 87 86.7 07.6 37 136.5 11.9 87 186 3 16.3 37 236.1 20.6 87 285.9 25.0 38 37.9 03.3 88 87.7 07.7 38 137.5 12.0 88 187.3 16.4 38 237.1 20.7 88 286.9 25.1 39 38.9 03.4 89 88.7 07.8 39 138 5 12.1 89 188.3 16.4 39 238.1 20.8 89 287.9 25.1 40.8 03.6 91 90.7 77.5 141 140.5 12.3 191 190.3 16.6 241 240.1 21.0 291 289.9 25.3 42.8 03.8 93.8 03.5 90 89.7 07.8 40 139 5 12.2 90 189.3 16.5 40 239 1 20.9 90 288.9 25.2 41 40.8 03.6 91 90.7 77.5 141 140.5 12.3 191 190.3 16.6 241 240.1 21.0 291 289.9 25.3 42.8 03.8 94 93.6 08.2 44 143.5 12.4 92 191.3 16.7 42 241.1 21.1 93 291.9 25.5 44.8 03.9 95 94.6 08.3 45 144.4 12.6 95 194.3 17.0 45 244.1 11.3 95 293.9 25.7 46 45.8 04.0 96 95.6 08.4 146 145.4 12.7 196 195.3 17.1 47 246.1 21.5 97 295.9 25.8 47 46.8 04.1 97 96.6 08.5 47 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.8 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0		-	-11	-	-	_	-			-							-	_
33 32.9 02.9 83 82.7 07.2 33 132.5 11.6 83 182.3 15.9 33 232.1 20.3 83 281.9 24.6 34 33 9 0 3.c 84 83.7 07.3 34 133.5 11.7 84 183.3 16.0 34 233.1 20.4 84 282.9 24.7 35 14.9 03.1 86 85.7 07.5 136 135.5 11.8 11.7 85 184 3 16.1 35 234 1 20.4 85 283.9 24.8 37 36.9 03.2 87 36.7 07.6 37 136.5 11.9 87 186 185.3 16.2 236 235.2 20.5 286 284.9 24.9 24.9 38 37.9 03.3 88 87.7 07.7 38 137.5 12.0 88 187.3 16.4 38 237.1 20.7 88 285.9 25.0 39 38.9 03.4 89 88.7 07.8 39 138 5 12.1 89 188.3 16.4 39 238.1 20.8 89 287.9 25.1 40.8 03.6 91 90.7 07.8 40 139 5 12.2 90 189.3 16.5 40 239 1 20.9 90 288.9 25.2 41 40.8 03.6 91 90.7 07.8 40 139 5 12.2 90 189.3 16.5 40 239 1 20.9 90 288.9 25.2 41 40.8 03.8 93.6 08.6 42 141.5 12.4 93 192.3 16.8 43 242.1 21.1 93 290.9 25.4 43.8 03.8 94 93.6 08.2 44 143.5 12.5 94 193.3 16.9 44 243.1 21.2 94 292.9 25.6 45 44.8 03.9 95 94.6 08.3 45 144.4 12.6 95 194.3 17.0 45 244.1 21.3 95 293.9 25.7 46 45.8 04.0 96 95.6 08.4 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 48 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.8 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0		10 01					7											
34       33       9       3.6       84       83.7       07.3       34       133.5       11.7       84       183.3       16.0       34       233.1       20.4       84       282,9       24.7         35       34.9       03.1       86       85.7       07.5       136       135.5       11.8       186       185.3       16.2       236       235.2       20.5       286       284.9       24.9         37       36.9       03.2       87       36.7       07.6       37       136.5       11.9       87       186       316.3       37       236.1       20.6       38       237.1       20.6       38       237.1       20.6       37       236.5       11.9       87       186.3       16.3       37       236.1       20.6       37       236.1       20.6       37       236.1       20.6       37       236.1       20.6       37       236.1       20.6       37       236.1       20.6       37       236.1       20.6       37       236.1       236.1       236.1       236.1       236.1       236.1       236.1       236.1       236.1       236.1       236.1       236.1       236.1       236.1       23			. 11		82.7	07.2												
35       34.9       03.1       85       84.7       07.4       35       134.5       11.7       85       184.3       16.1       35       234.1       20.4       85       283.9       24.8         36       35.9       03.1       86       85.7       07.5       136       135.5       11.8       186       185.3       16.2       236       235.1       20.5       286       284.9       24.9         37       36.9       03.2       87       86.7       07.6       37       136.5       11.9       87       186.3       16.3       37       236.1       20.6       87       285.9       25.0         38       37.9       03.2       88       87.7       07.7       38       137.5       12.0       88       187.3       16.4       39       238.1       20.6       88       287.9       25.1         39       38.9       03.5       90       89,70.7       40       139.5       12.2       90       189.3       16.5       40       239.1       20.8       89       287.9       25.1         40       39.8       03.5       91.90.7       7.9       141.1       140.5       12.3       191.1	34	33 9 03	.c	84	83.7	07.3				84	183.3			233.1	20.4		282,9	24.7
37       36.9 03.2       87 86.7 07.6       37 136.5 11.9       87 186 3 16.3       37 236.1 20.6       87 285.9 25.0         38       37.9 03.3       88 87.7 07.7       38 137.5 12.0       88 187.3 16.4       38 237.1 20.7       88 286.9 25.1         39       38.9 03.4       89 88.7 07.8       39 138 5 12.1       89 188.3 16.4       39 238.1 20.8       89 287.9 25.1         40       39.8 03.5       90 89.7 07.8       40 139 5 12.2       90 189.3 16.5       40 239 1 20.9       90 288.9 25.2         41       40.8 03.6       91 90.7 27.9       141 140 5 12.3       191 190.3 16.6       241 240.1 21.0       291 289.9 25.3         42       41.8 03.7       92 91.6 28.0       42 141.5 12.4       92 191.3 16.7       42 241.1 21.1       92 290.9 25.4         43       42.8 03.8       93 92.6 28.1       43 142.5 12.4       93 192.3 16.8       43 242.1 21.1       93 291.9 25.5         44       43.8 03.8       94 93.6 28.2       44 143.5 12.5       94 193.3 16.9       44 243.1 21.2       94 292.9 25.6         45       44.8 03.9       95 94.6 28.3       45 144.4 12.6       95 194.3 17.0       45 244.1 21.3       95 293.9 25.7         46       45.8 04.0       96 95.6 28.4       47 146.4 12.8       97 196.3 17.1       47 246.1 21.5 <td< td=""><td>35</td><td>14.9 03</td><td>.1</td><td>85</td><td>84.7</td><td>37,4</td><td>35</td><td>134.5</td><td>11.7</td><td>85</td><td>184 3</td><td>16.1</td><td>35</td><td>234.1</td><td>20.4</td><td>85</td><td>283.9</td><td>24.8</td></td<>	35	14.9 03	.1	85	84.7	37,4	35	134.5	11.7	85	184 3	16.1	35	234.1	20.4	85	283.9	24.8
37       36.9 03.2       87 86.7 07.6       37 136.5 11.9       87 186 3 16.3       37 236.1 20.6       87 285.9 25.0         38       37.9 03.3       88 87.7 07.7       38 137.5 12.0       88 187.3 16.4       38 237.1 20.7       88 286.9 25.1         39       38.9 03.4       89 88.7 07.8       39 138 5 12.1       89 188.3 16.4       39 238.1 20.8       89 287.9 25.1         40       39.8 03.5       90 89.7 07.8       40 139 5 12.2       90 189.3 16.5       40 239 1 20.9       90 288.9 25.2         41       40.8 03.6       91 90.7 27.9       141 140 5 12.3       191 190.3 16.6       241 240.1 21.0       291 289.9 25.3         42       41.8 03.7       92 91.6 28.0       42 141.5 12.4       92 191.3 16.7       42 241.1 21.1       92 290.9 25.4         43       42.8 03.8       93 92.6 28.1       43 142.5 12.4       93 192.3 16.8       43 242.1 21.1       93 291.9 25.5         44       43.8 03.8       94 93.6 28.2       44 143.5 12.5       94 193.3 16.9       44 243.1 21.2       94 292.9 25.6         45       44.8 03.9       95 94.6 28.3       45 144.4 12.6       95 194.3 17.0       45 244.1 21.3       95 293.9 25.7         46       45.8 04.0       96 95.6 28.4       47 146.4 12.8       97 196.3 17.1       47 246.1 21.5 <td< td=""><td>36</td><td>35.903</td><td>. 1</td><td>86</td><td>85.7</td><td>07.5</td><td>136</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>286</td><td>284.9</td><td>24.9</td></td<>	36	35.903	. 1	86	85.7	07.5	136									286	284.9	24.9
39   38.9   03.4   89   88.7   07.8   39   138   5   12.1   89   188.3   16.4   39   238.1   20.8   89   287.9   25.1   40   39.8   03.5   90   89.7   07.8   40   139   5   12.2   90   189.3   16.5   40   239   1 20.9   90   288.9   25.2   41   40.8   03.6   91   90.7   27.5   41   140   5   12.3   191   190.3   16.6   241   240.1   21.0   291   289.9   25.3   42   41.8   03.7   92   91.6   28.6   42   141.5   12.4   92   191.3   16.7   42   241.1   21.1   92   290.9   25.4   43.8   03.8   93   92.6   08.1   43   142.5   12.4   93   192.3   16.8   43   242.1   21.1   93   291.9   25.5   44.8   03.8   94   93.6   08.2   44   143.5   12.5   94   193.3   16.9   44   243.1   21.2   94   292.9   25.6   45   44.8   03.9   95   94.6   08.3   45   144.4   12.6   95   194.3   17.0   45   244.1   21.3   95   293.9   25.7   46.8   04.1   97   96.6   08.5   47   146.4   12.8   97   196.3   17.1   47   246.1   21.5   97   295.9   25.8   48   47.8   04.2   98   97.6   08.5   48   147.4   12.9   98   197.2   17.2   48   247.1   21.6   98   296.9   25.9   49   48.8   04.3   99   98.6   08.6   49   148.4   13.0   99   198.2   17.3   49   248.1   21.7   99   297.9   26.0				87	36,7	07.6		136.5	11.9	87	186 3	16.3	37	236.1	20.6	87	285.9	25,0
40 39.8 03.5 90 89,7 07.8 40 139 5 12.2 90 189.3 16 5 40 239 1 20.9 90 288.9 25.2 41 40.8 03.6 91 90.7 27.5 141 140 5 12.3 191 190.3 16.6 241 240.1 21.0 291 289.9 25.3 42 41.8 03.7 92 91.6 28.1 43 142.5 12.4 92 191.3 16.7 42 241.1 21.1 92 290.9 25.4 43.8 03.8 93 92.6 08.1 43 142.5 12.4 93 192.3 16.8 43 242.1 21.1 93 291.9 25.5 44.8 03.9 95 94.6 08.3 45 144.4 12.6 95 194.3 17.0 45 244.1 21.3 95 293.9 25.7 46 45.8 04.0 96 95.6 08.4 146 145.4 12.7 196 195.3 17.1 246 245.1 21.3 95 293.9 25.7 46.8 04.1 97 96.6 08.5 47 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 48 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.9 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0		37.903	.3	88	87,7	37.7			12.0	88	187.3	16.4	38	237.1	20.7	88	286,9	25.1
41 40.8 03.6 91 90.7 27,6 141 140 5 12.3 191 190.3 16.6 241 240.1 21.0 291 289.9 25.3 42 41.8 03.7 92 91.6 28.0 42 141.5 12.4 92 191.3 16.7 42 241.1 21.1 92 290.9 25.4 43 42.8 03.8 93 92.6 08.1 43 142.5 12.4 93 192.3 16.8 43 242.1 21.1 93 291.9 25.5 44 43.8 03.8 94 93.6 08.2 44 143.5 12.5 94 193.3 16.9 44 243.1 21.2 94 292.9 25.6 45 44.8 03.9 95 94.6 08.3 45 144.4 12.6 95 194.3 17.0 45 244.1 21.3 95 293.9 25.7 46.8 04.1 97 96.6 08.5 47 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 48 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.9 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0	1 39	38.903	.4	00	88.7	37.8		138 5	12.1	89	180.3	16.4				89	287.9	25.1
42       41.8 0 3.7   92 91.6						-	14						-	-	-	90	200.9	25.2
43 42.8 03.8 93 92.6 08.1 43 142.5 12,4 93 192.3 16.8 43 242.1 21.1 93 291.9 25.5 44 43.8 03.8 94 93.6 08.2 44 143.5 12.5 94 193.3 16.9 44 243.1 21.2 94 292.9 25.6 45 44.8 03.9 95 94.6 08.3 45 144.4 12.6 95 194.3 17.0 45 244.1 21.3 95 293.9 25.7 46.8 04.0 96 95.6 08.4 146 145.4 12.7 196 195.3 17.1 246 245.1 21.4 296 294.9 25.8 47 46.8 04.1 97 96.6 08.5 47 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 48 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.9 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0		40.803	.6	91	90.7	27,9				191	190.3	16.0				29 I	289.9	35.3
44 43.8 03.8 94 93.6 08.2 44 143.5 12.5 94 193.3 16.9 44 243.1 21.2 94 292.9 25.6 45 44.8 03.9 95 94.6 08.3 45 144.4 12.6 95 194.3 17.0 45 244.1 21.3 95 293.9 25.7 46 8 04.1 97 96.6 08.5 47 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 48 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.9 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0		41.803	.7							92	191.3	16.8				92	290.9	25.4
45   44,8   03.9   95   94,6   08.3   45   144.4   12.6   95   194.3   17.0   45   244.1   21.3   95   293.9   25.7   46   45.8   04.0   96   95.6   08.4   146   145.4   12.7   196   195.3   17.1   246   245.1   21.4   296   294,9   25.8   47   46.8   04.1   97   96.6   08.5   47   146.4   12.8   97   196.3   17.1   47   246.1   21.5   97   295.9   25.8   48   47.8   04.2   98   97.6   08.5   48   147.4   12.9   98   197.2   17.2   48   247.1   21.6   98   296.9   25.9   49   48.8   04.3   99   98.6   08.6   49   148.4   13.0   99   198.2   17.3   49   248.1   21.7   99   297.9   26.0			.8	94	92.6	08.2	1			93	192.2	16.9						
46 45.8 04.0 96 95.6 08.4 146 145.4 12.7 196 195.3 17.1 246 245.1 21.4 296 294,9 25.8 47 46.8 04.1 97 96.6 08.5 47 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 48 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.9 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0			.0	95	94,6	08.3		144.4	12.6	95	194.2	17.0						
47 46.8 04.1 97 96.6 08.5 47 146.4 12.8 97 196.3 17.1 47 246.1 21.5 97 295.9 25.8 48 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.9 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0	46							OR SHALL SEE										
48 47.8 04.2 98 97.6 08.5 48 147.4 12.9 98 197.2 17.2 48 247.1 21.6 98 296.9 25.9 49 48.8 04.3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0	1 47	46.8 04					47	146.4	12.8	97	196.3	17.1	47	246.1	21.5			
49 48.8 04,3 99 98.6 08.6 49 148.4 13.0 99 198.2 17.3 49 248.1 21.7 99 297.9 26.0	48	47.8 04	.2	98	97.6	08.5		147.4	12.9	98	197.2	17.2	48	247.1	21.6			
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8	08.000 8		7 06.0		106.4	11.3			16.5	08	206,9		57	255 6	
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13	12 9 01.4		.7 06.6			11.8	63	162.1	17.0	13	211.8	22,3		261.6	
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27	26.902 8		.6 08.0	27	125.3	13.3	77	176.0	18.5		225,8		276 77	274.5 275.5	
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29	28.8 03.0		6 08.3	29	128 3	19.5	79	178.0	18.7	29	227.7		79	277.5	10000
30	29.8 03.1	80 79	6 08.4			13.6	80	179 0	18,8	. 30	228,7		80	278.5	
31	30.8 03.2	8180	.6 08,5	131	130.3	13.7	181	180.0	18.9	231	229.7	24.1	281	279.5	-
32	31.803.3		.5 08.6			13.8		181.0			230.7	24.2	82	280.4	
	32.8 03.4	83 82	.5 08.7	33	132 3	13.9	23	182.0			231.7		83	281.4	29.6
	33.803.6		.5 08.8		P33-3	14.0	84	183.0			232.7		84	282,4	
35	34.8 03.7		5 08.9	35	134.3	14,1	85	184.0		35	233.7	-	85	283.4	29.8
36	35.8 03.8	86 85	5 09 0		135.3	14.2	186	185,0			234.7		286	284.4	
	36.803.9	87 86	509.1	37		14.3		186 0			235.7		87	285.4	30.0
	38.8 04.1	80 88	509.2	38	137.2	14.5	80	183.0	19.8	38	236.7	25.0	88	286,4	30.1
	39.8 04.2	90/80	5 09,4	39 40	139 2	14 6	90	189.0	199	40	238.7	25.1	90	287.4 288.4	30.2
40	40.8 04,3		5 09.5		140 2						239 7				-
42	41.8 04.4		509.6	141	141.2	14.8	191	189.9	20.1		240.7		29 I 92	289.4	30 4
43	42.8 04,5		5 09.7		142.2		02	191.9	20.2		241.7		93	290.4 291.4	
44	43.8 04.6		509.8	44	143.2	15,0	94	192.9	20.3		242.7		94	292.4	
45	44,8 04.7	95 94	509.9	45	144.2	15,2	95	193.9	20.4		243.7		95	293.4	30,8
46			5 10.0		145.2		196	194.9	20.5		244.6		296	294,4	_
45 46 47	45.7 04 8 46.7 04.9	97 96.	5 10.1	47	146.2	15.4	97	195.9	20.0	47	245.6	25.8	97	295.4	
48	47.7 05.0	98 97.	5 10.2	48	147.2	15.5	98	196.9	20.7	48	246.6	25.9	98	296.4	
	48.7 05.1	99 98.	5 10.3		148.2		99	197.9	20,8		247.6		99	297.4	31.2
	49.7 05.2				149.2			198.9			248.6		300	298.4	31.4
Dift	Dep Lat	Diff De	p Lat	Ditt	Dep	Lat	Diff	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat

Difference of Latitude a	nd Departure for	7 Deg.
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4 04.5 06.5 5 54.6 06.7 05 104,2 12.8 55 153.8 18.9 05 203.5 25.0 55 253.1 31.0 06.9 00.9 57 56.6 06.9 07 106.2 13.0 57 155.8 19.1 07 205.4 25.2 57 255.1 31.3 9 08.9 01.1 59 58.6 07.2 09 108.2 13.3 58 156.8 19.4 09 207.4 25.4 59 257.1 31.5 9 08.9 01.1 59 58.6 07.2 09 108.2 13.3 59 157 8 19.4 09 207.4 25.4 59 257.1 31.5	275	1	1	-7									11.44		Sel No	0	AL STATE	/
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7 06.9 don.9   58 57.6 dos.9   08 107.2   13.1   09 08.2   13.2   09 08.2   13.3   10 09 9 01.2   10 09 9 01.2   10 09 9 01.2   10 09 9 01.2   10 09 01.3   10 10 00.3   10 10 00.2   13.3   10 10 00.3   10 10 00.2   13.4   10 10 00.3   10 10 00.2   13.4   10 10 00.3   10 10 00.2   13.4   10 10 00.3   10 10 00.2   13.4   10 10 00.3   10 10 00.2   13.4   10 10 00.3   10 10 00.2   13.4   10 10 00.3   10 10 00.2   13.4   10 10 00.3   10 10 00.2   13.4   10 10 00.3   10 10 00.3   10 10 10 10 10 10 10 10 10 10 10 10 10	-	-		-				_		1		_	-	_	_		-	-
\$ 07. 0 01.0   9 08.0 01.2   10 09.0   107.2   13.1   13.0   10.0 0 01.3   13.3   10.0 09.0   13.0   10.0 09.0   13.4   10.0 01.3   13.3   10.0 09.0   13.4   13.3   10.0 09.0   13.4   13.3	100	- 10														7		
9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		07.9	01,0	7.0	57.6	07.1	08	107.2	13.1	58				206.4	25.3	100		
10 0 9 0 1 2		08.9	01.1								157	19.4	09	207.4	25.4		200.00	
12 11.9 01.6 62 61.5 07.5 12 111.2 13.6 62 160 8 19.7 12 210.4 5.7 8 25.0 3.8 14 113.1 13.6 13.9 8 13 211.4 25.9 63 62.5 07.8 14 113.1 13.9 64 162.8 20.0 16 15 90.1 9 65 64.5 07.9 15 114.1 14.0 65 163.8 20.1 16 15 90.1 9 66 65 5 08.2 17 116.1 14.2 67 166.8 20.0 16 17 17 16.9 01.1 67 66 5 08.2 17 116.1 14.2 67 165.7 20.3 17 215.4 16.4 68 17 9 92.2 68 67.5 08.3 18 117.1 14.4 68 166.7 20.5 18 216.4 16.5 20.2 19 19 20.4 7.0 50.5 08.5 18 117.1 14.4 68 166.7 20.5 18 216.4 16.5 20.2 19 19 20.4 7.0 50.5 08.5 20 119.1 14.6 70 168.7 20.5 18 216.4 16.5 68 266.0 13.4 21.8 21.8 21.8 21.8 21.8 21.8 21.8 21.8	10	_		-	-	-	-		_	-	_		10	208.4	25.6			
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14				V			11									1 2 7	260.c	31.9
15																	261.c	32.0
16				65					1					Same and the same		65	262.0	32.1
17   16.9   02.1   68   67.5   08.2   17   116.1   14.2   68   165.7   20.3   17   215.4   26.5   68   26.5   23.2   18   117.1   14.4   68   165.7   20.5   19   117.4   26.7   20.6   19   117.4   26.7   20.6   19   117.4   26.7   20.6   19   117.4   26.7   20.6   19   117.4   26.7   20.6   19   117.4   26.7   20.6   19   117.4   26.7   20.6   20.7   20.8   22   21.2   20.2   27.0   20.8   22   21.2   20.2   27.0   20.8   22   21.2   20.2   27.0   20.8   22   20.2   27.0   27.2   27.0   20.8   22   20.2   27.0   27.2   27.0   20.8   22   20.2   27.0   27.2   27.0   20.8   22   20.2   27.0   27.0   27.2   27.2	16		_	66	65 5	08.0	116	115.1	14.1	-	-	-	216		_			
18 17 9 92.2   08 67.5 08.3   18 117.1 14.4   68 166.7 20.5   18 216.4 26.5   68 266 c 32.6   20 19.9 02.4   70 39.5 08.5   20 119.1 14.6   70 168.7 20.6   72 20 218.4 16.8   70 268 c 32.9   21 20.8 02.6   71 70.5 08.6   121 120.1 14.7   171 169.7 20.8   22 12.19.3 26.9   27 26.8 c 32.9   24 23.8 02.9   74 73.4 09.6   24 123.1 15.1   74 77.7 12.1   23 221.3 27.2   27.0 13.4   27.1 12.2   24.8 22.3   27.0   27.0 13.4   27.1 12.2   24.8 22.3   27.0   27.0 13.4   27.1 12.2   24.8 22.3   27.3   27.4   27.1 12.3   25.8 03.2   76 75.4 09.3   27.1 15.0   27.1 15.0   27.1 15.0   27.8   27.9   27.8		16.9	02.1		66 5	08,2	1 2	116.1		67			17	215.4	26.4	67	265.0	22.5
19 13 9 02-3									1		166.7	20.5	18	216.4	26.5		266 c	12.6
21								A STATE OF THE PARTY OF							26,7			
22 21.8 02.7 72 71.5 08.8 22 121.1 14.9 72 170.7 20.9 22 220.3 27.0 72 270.0 33.1 23.2 24.8 02.9 74 73.4 09.6 24 123.1 15.1 74 172.7 21.2 24 222.3 17.3 74 271.9 33.4 271.6 25.8 03.2 76 75.4 0.9.1 25 124.1 15.2 75 173.7 21.3 22 22.3 27.4 75 272.9 33.5 27 26.8 03.3 77 76.4 0.9.4 27 126.0 15.5 77 175.7 21.6 27 22.5 3 27.6 72.4 19.3 3.9 27.8 27.8 03.4 78 77.4 09.5 27 126.0 15.5 77 175.7 21.6 27 22.5 3 27.6 77 274.9 33.7 28 27.8 03.4 78 77.4 09.5 29 128 c 15.7 79 177.7 21.8 22 22.7 3.7 76 27.9 33.9 29.8 03.7 78.4 09.6 29 128 c 15.7 79 177.7 21.8 29 22.7 3.9 27.9 33.9 27.4 99.5 29 128 c 15.7 79 177.7 21.8 29 22.7 3.9 27.9 36.2 27.9 36	-	-		-	-	-	-	-	-			_	20	218.4	168	70	268 c	32.9
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27	26	25.8	03.2	76	75.4	9 3	126	125.1	15.3	176	174.7	21.4					7. 7. 7. 7. 7.	
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29       29       8   3   5   79   79   79   79   79   77   72   18   80   79   30   228   328   38   277   93   31   30   80   81   80   40   99   131   30   80   328   81   40   100   32   131   160   82   180   622   32   230   328   328   34   34   328   34   34   34   34   34   34   34   3													28	226.3	27.8			
31       30 8 03.8       81 80.4 09 9       131 130.c 16.0       181 179.6 22.0       231 229 3 28.1       28.1 278.9 34.2         32       31.8 03.9       82 81.4 10.0       32 131 c 16.1       82 180.6 22.2       32 230.3 28.3       82.2 279.9 34.5         34       33 7 04.1       84 83.4 10.2       34 133.c 16.3       84 182.6 22.4       34 232.2 28.5       84 281.9 34.6         35 34.7 04.3       86 85.4 10.4       35 134.c 16.4       85 184.6 22.5       35 233 2 28.6       85 182.9 34.7         37 36.7 04.5       87 86.3 10.6       37 136.c 16.7       87 185.6 22.8       37 235.2 28.9       87 284.8 34.9         39 38.7 04.8       88 87.3 10.7       38 137.c 16.8       88 186.6 22.9       38 236.2 29.0       88 285.8 35.1         39 38.7 04.8       89 88.3 10.8       39 138.c 16.9       89 187.6 23.0       39 237.2 29.1       89 286.8 35.2         40 39 7 04.9       90 89.3 11.6       40 139.0 17.1       191 189.6 23.3       22.1 23.2       29.2 29.3       89 286.8 35.2         41 40.7 05.0       91 90.3 11.1       141 139.9 17.2       191 189.6 23.3       22.3       29.1 288.8 35.5       92 287.8 35.3         44 43.7 05.4       94 93.3 11.5       44 142.9 17.5       94 192.5 23.6       44 242.2 29.9       92 29.8 35.5         44 4.7 0		23.8	03.5				1 1 -						29	227.3	27,9	79	276.9	34 0
32 31.8 03.9 82 81.4 10.0 32 131 c 16.1 82 180.6 22.2 32 230.3 28.3 82 279.9 34.3 32.8 04.0 83 82.4 10.1 33 132.c 16.2 83 181.6 22.3 33 231.3 28.4 33 280.9 34.5 35 34.7 04.1 84 83.4 10.4 35 134.c 16.4 85 183.6 22.5 35 233 2 28.6 85 182.9 34.7 36.7 04.5 86 85.4 10.5 136 135.c 16.6 186 184.6 22.7 236 234.2 18.7 286 283.9 34.8 37.7 04.6 88 87.3 10.7 38 137.c 16.8 88 186 6 22.9 38 236.2 29.0 88 88.3 10.8 39 138.c 16.9 89 187.6 23.0 39 237.2 29.1 88 286.8 35.1 39.7 04.9 90 89.3 11.c 40 139.0 17.1 90 188.6 23.1 40 238.2 29.2 90 287.8 35.3 44.7 05.1 92 91.3 11.2 42 140.9 17.3 92 190.6 23.4 42 240.2 29.5 91.3 11.2 42 140.9 17.3 92 190.6 23.4 42 240.2 29.5 92 287.8 35.6 44.7 05.5 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.9 99 29.8 35.6 45.4 47.0 05.5 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.9 99 29.8 35.6 47.4 6.6 05.7 97 96.3 11.8 47 145.9 17.9 97 195.5 24.0 47 245.1 30.1 99 296.8 36.4 47.6 05.8 98 97.3 11.9 48 146.9 18.0 98 196.5 24.1 48 246.1 30.2 98 295.8 36.5 99 98.3 12.1 10.9 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 100 297.8 36.5 59 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 100 297.8 36.5				-	_	-		_	_	-	_	-		-		-		
33 32.8 04.0 83 82.4 10.1 33 132.c 16.2 83 181.6 22.3 33 231.3 28.4 85 280.9 34.5 35 34.7 04.3 85 84.4 10.4 35 134.0 16.4 85 183.6 22.5 35 233 2 28.6 85 182.9 34.7 36.7 04.5 87 86.3 10.6 37 136.0 16.7 87 185.6 22.8 37 235.2 28.9 87 86.3 10.6 37 136.0 16.7 87 185.6 22.8 37 235.2 28.9 88 87.3 10.7 38 137.0 16.8 88 186 6 22.9 38 236.2 29.0 88 285.8 35.1 38.7 04.8 89 88.3 10.8 39 138.0 16.9 89 187.6 23.0 39 237.2 29.1 89 286.8 35.2 40 39 7 04 9 90 89.3 11.6 40 139.0 17.1 90 188.6 23.1 40 238.2 29.2 90 287.8 35.3 44 40.7 05.0 91 90.3 11.1 141 139.9 17.2 191 189.6 23.5 43 241 239.2 29.5 92 287.8 35.4 44.7 05.5 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.8 95 292.8 35.5 45 44.7 05.5 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.8 95 292.8 35.5 46 45.7 05.6 96 95.3 11.7 146 144.9 17.8 196 194.5 23.0 194.5 24.1 30.1 97 294.8 35.6 29.8 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 99 296.8 36.4 59.4 60.6 1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 90 297.8 36.5	-															1 - 1	278.9	34.2
34       33       7       04.1       84       83.4       10.2       34       133.0       16.3       84       182.6       22.4       34       232.2       28.5       84       281.9       34.6         35       34.7       04.4       86       85.4       10.5       136.0       16.6       186.1       184.6       22.7       236.2       234.2       18.7       286.9       34.7         37       36.7       04.5       87       86.3       10.6       37       136.0       16.6       186.1       184.6       22.7       236.2       234.2       18.7       286.9       34.8       34.8       38.3       39.3       13.6       16.6       186.1       186.6       22.9       38.2       23.2       28.9       38.2       285.8       39.3       48.8       285.8       35.1       39.3       38.7       24.8       39.3       10.8       39.1       13.6       16.9       89.1       187.6       23.0       39.2       237.2       29.1       89.2       286.8       35.2         40       39.7       24.9       90.3       11.1       141.1       139.0       17.1       90.1       188.6       23.1       40.2       2								-									279.9	34.3
35         34.7         04.3         85         84.4         10.4         35         134.0         16.4         85         183.6         22.5         35         233.2         28.6         85         182.9         34.7           36         35.7         04.5         87         86.3         10.6         37         136.0         16.7         87         185.6         22.7         37         235.2         28.9         34.8           38         37.7         04.6         88         87.3         10.7         38         137.0         16.8         88         186.6         22.9         38         236.2         29.0         88         285.8         35.1           39         38.7         04.8         89         88.3         10.8         39         138.0         16.9         89         187.6         23.0         39         237.2         29.1         89         286.8         35.5           40         39.7         04.9         90.8         31.1.1         141         139.0         17.1         90         188.6         23.1         40         238.2         29.2         90         287.5         35.3           41         40.7         05.0 </td <td></td> <td>1-</td> <td>04.1</td> <td>84</td> <td>83.4</td> <td>10.2</td> <td></td> <td>281:0</td> <td>34.5</td>		1-	04.1	84	83.4	10.2											281:0	34.5
36  35  7  04.4  86  85.4  10.5  136  135.0  16.6  186  184.6  22.7  236  234.2  18.7  286  283.9  34.8  36.7  04.5  87  86.3  10.6  37  136.0  16.7  87  185.6  22.8  37  235.2  28.9  38  236.2  19.0  38  88,3  10.8  39  138.0  16.9  89  187.6  23.0  39  237.2  29.1  40  238.2  29.2  40  139.0  17.1  90  188.6  23.1  40  238.2  29.2  90  287.8  35.3  42  47  05.1  92  91.3  11.2  42  140.9  17.3  92  190.6  23.4  42  240.2  29.5  43  42  240.2  29.5  43  42.7  05.2  93  92.3  11.5  44  142.9  17.4  93  191.6  23.5  43  241.2  29.6  95  94.3  11.6  45  143.9  17.7  95  193.5  23.7  45  243.2  29.8  95  292.8  35.6  44  43.7  05.6  96  95.3  11.7  146  144.9  17.8  196  194.5  23.9  246  244.2  29.9  95  292.8  35.6  44  47.6  05.8  98  97.3  11.9  48  146.9  18.0  98  196.5  24.1  48  246.1  30.2  98  293.8  36.2  49.4  6.6  05.7  97  96.3  11.8  47  145.9  17.9  97  195.5  24.0  47  245.1  30.1  97  294.8  36.2  49.4  6.6  05.7  97  96.3  11.8  47  145.9  17.9  97  195.5  24.0  47  245.1  30.1  97  294.8  36.2  98  48.6  06.0  99  98.3  12.1  49  147.9  18.1  99  197.5  24.2  49  247.1  30.3  99  296.8  36.4  49.6  06.1  100  99.3  12.2  150  148.9  18.2  200  198.5  24.3  250  248.1  30.4  100  297.8  36.5	-	34.7	04.3	85	84.4	10.4	35	134.0	16.4	85			0.2.0					
37       36.7       04.5       87       86.3       10.6       37       136.c       16.7       87       185.6       22.8       37       235.2       28.9       87       284.8       34.9         39       38.7       04.8       89       88.3       10.8       39       138.c       16.9       89       187.6       23.0       39       237.2       29.1       89       286.8       35.1         40       39.7       04.9       90       89.3       11.6       40       139.0       17.1       90       188.6       23.1       40       238.2       29.2       90       287.8       35.3         41       40.7       05.0       91       90.3       11.1       141       139.9       17.2       191       189,6       23.3       241       239.2       29.3       29.1       287.8       35.3         42       41.7       05.1       92       91.3       11.2       42       140.9       17.3       92       190.6       23.4       42       240.2       29.5       92       289.8       35.5         43       42.7       05.1       94       93.3       11.5       44       142.9	-				85.4	10.5	136						236	234.2	18.7			
39 38.7 04.8 89 88,3 10.8 39 138.c 16.9 89 187.6 23.0 39 237.2 29.1 89 286,8 35.2 40 39.7 04.9 90 89.3 11.6 40 139.0 17.1 90 188.6 23.1 40 238.2 29.2 90 287.8 35.3 41 40.7 05.0 91 90.3 11.1 141 139.9 17.2 191 189.6 23.3 241 239.2 29.3 291 288.8 35.6 42 41.7 05.1 92 91.3 11.2 42 140.9 17.3 92 190.6 23.4 42 240.2 29.5 92 189.8 35.5 43 42.7 05.2 93 92.3 11.3 43 141.9 17.4 93 191.6 23.5 43 241.2 29.6 93 190.8 35.5 44 242.2 29.7 191 189.5 23.6 44 242.2 29.7 191 189.5 23.6 44 242.2 29.7 191 189.5 23.6 44 242.2 29.7 191 189.5 23.6 44 242.2 29.7 191 189.5 23.6 45 143.9 17.7 95 193.5 23.7 191 191 191 191 191 191 191 191 191 19	37			87	86.3	10.6	37			87	185.6	22,8	37	235.2	28.9	87	284.8	34.0
40 39 7 04 9 90 89.3 11.6 40 139.0 17.1 90 188.6 23.1 40 238.2 29.2 90 287.8 35.3 41 40.7 05.0 91 90.3 11.1 141 139.9 17.2 191 189.6 23.3 42 240.2 29.5 92 188.8 35.4 42 27 05.2 93 92.3 11.3 43 141.9 17.4 93 191.6 23 5 43 241.2 29.6 95 290.8 35.7 44 43.7 05.4 94 93.3 11.5 44 142.9 17.5 94 192.5 23.6 44 242.2 29.7 94 291.8 35.8 44.7 05.5 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.8 95 292.8 35.5 46 45 \$\tau\$ 05.6 96 95.3 11.7 146 144.9 17.8 196 194.5 23.9 146 244.2 29.9 95 292.8 35.6 47 46.6 05.7 97 96.3 11.8 47 145.9 17.9 97 195.5 24.0 47 245.1 30.1 97 294.8 36.2 48.4 7.6 05.8 98 97.3 11.9 48 146.9 18.0 98 196.5 24.1 48 246.1 30.2 98 295.8 36.3 50.4 48.6 06.0 99 98.3 12.1 49 147.9 18.1 99 197.5 24.2 49 247.1 30.3 99 296.8 36.4 50.4 96.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 30.4 30.4 297.8 36.5		37.7	04.6	80	88.	10.7	38	137.0	16.8	88	186 6	22,9	38	236.2	29.0	88	285.8	35.1
41 40,7 05 0 91 90.3 11,1 141 139.9 17.2 191 189,6 23.3 241 239,2 29,3 291 288.8 35.6 42 41 7 05.1 92 91.3 11.2 42 140.9 17.3 92 190.6 23.4 42 240.2 29.5 43 42 140.9 17.3 92 191.6 23 5 43 241.2 29.6 93 290.8 35.7 44 43.7 05.4 94 93.3 11.5 44 142.9 17.5 94 192.5 23.6 44 242.2 29.7 94 291.8 35.8 45.6 45.7 05.6 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.8 95 292.8 35.6 47 46.6 05.7 97 96.3 11.8 47 145.9 17.9 97 195.5 24.0 47 245.1 30.1 97 294.8 36.2 48 47.6 05.8 98 97.3 11.9 48 146.9 18.0 98 196.5 24.1 48 246.1 30.2 98 295.8 36.2 49 48.6 06.0 99 98.3 12.1 49 147.9 18.1 99 197.5 24.2 49 247.1 30.3 99 296.8 36.4 50 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 100 297.8 36.5	40	30.7	24.0	10	80.2	11.6		130.0	17.1	89	188 6	23.0		237.2	19.1	1 69	286,8	35 2
42       41       7       05.1       92       91.3       11.2       42       140.9       17.3       92       190.6       23.4       42       240.2       29.5       92       289.8       35.5         43       42       7       05.2       93       92.3       11.3       43       141.9       17.4       93       191.6       23       5       43       241.2       29.6       95       290.8       35.7         44       43.7       05.4       94       93.3       11.5       44       142.9       17.5       94       192.5       23.6       44       242.2       29.7       94       291.8       35.5         45       44.7       05.5       95       94.3       11.6       45       143.9       17.7       95       193.5       23.7       45       243.2       29.8       95       292.8       35.5         46       45       9       95.3       11.7       146       144.9       17.8       196       194.5       23.9       246       244.2       29.9       292.8       36.0         47       46.6       05.7       97       96.3       11.8       47       145.9 <t< td=""><td>41</td><td></td><td></td><td>1</td><td></td><td></td><td></td><td></td><td>_</td><td>_</td><td>180 6</td><td>-3</td><td></td><td>-</td><td>_</td><td>90</td><td>287.8</td><td>35.3</td></t<>	41			1					_	_	180 6	-3		-	_	90	287.8	35.3
43 42 7 05.2 93 92.3 11.3 43 141.9 17.4 93 191.6 23 5 43 241.2 29.6 95 290.8 35.5 44 43.7 05.4 94 93.3 11.5 44 142.9 17.5 94 192.5 23.6 44 242.2 29.7 94 291.8 35.8 45 44.7 05.5 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.8 95 292.8 35.6 47 46.6 05.7 97 96.3 11.8 47 145.9 17.9 97 195.5 24.0 47 245.1 30.1 97 294.8 36.2 48 47.6 05.8 98 97.3 11.9 48 146.9 18.0 98 196.5 24.1 48 246.1 30.2 98 295.8 36.2 49 48.6 06.0 99 98.3 12.1 49 147.9 18.1 99 197.5 24.2 49 247.1 30.3 99 296.8 36.4 50 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 100 297.8 36.5									17.2		100.6	23.3	42	140 2	9,3	291	88.8	35.4
44 43,7 05.4 94 93.3 11.5 44 142.9 17.5 94 192.5 23.6 44 242.2 29.7 94 291.8 35;8 45 44.7 05.5 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.8 95 292.8 35.9 46 45 \$\sigma\$ 05.6 96 95.3 11.7 146 144.9 17.8 196 194.5 23.9 146 244.2 29.9 296 293.8 36.0 47 46.6 05,7 97 96.3 11.8 47 145.9 17.9 97 195.5 24.0 47 245.1 30.1 97 294.8 36.2 48 47.6 05.8 98 97.3 11.9 48 146.9 18.0 98 196.5 24.1 48 246.1 30,2 98 295.8 36.3 49 48.6 06.0 99 98.3 12.1 49 147.9 18.1 99 197.5 24.2 49 247.1 10.3 99 296.8 36.4 50 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30,4 100 297.8 36.5	43	42 7	05.2	93	92.3	11.3	43									92	200.8	35.5
45 44.7 05.5 95 94.3 11.6 45 143.9 17.7 95 193.5 23.7 45 243.2 29.8 95 292.8 35.6 47 46.6 05.7 97 96.3 11.8 47 145.9 17.8 196 194.5 23.9 146 244.2 29.9 296 293.8 36.2 48 47.6 05.8 98 97.3 11.9 48 146.9 18.0 98 196.5 24.1 48 246.1 30.1 97 294.8 36.2 49 48.6 06.0 99 98.3 12.1 49 147.9 18.1 99 197.5 24.2 49 247.1 30.3 99 296.8 36.4 50 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 100 297.8 36.5	44	43.7	05.4	94	93.3	11.5	44	142.9	17-5							94	291.8	35.8
46 45 \$\( \cdot \) 05.6 96 95.3 11.7 146 144.9 17.8 196 194.5 23.9 146 244.2 29.9 296 293.8 36.c 47 46.6 05.7 97 96.3 11.8 47 145.9 17.9 97 195.5 24.0 47 245.1 30.1 97 294.8 36.2 48 47.6 05.8 98 97.3 11.9 48 146.9 18.0 98 196.5 24.1 48 246.1 30.2 98 295.8 36.3 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 100 297.8 36.5	45	_	_		_	11.6	45	143.9	17.7									
47 40.6 05.7 97 98.3 11.8 47 145.9 17.9 97 195.5 24.0 47 245.1 30.1 97 294.8 36.2 48 47.6 05.8 98 97.3 11.9 48 146.9 18.0 98 196.5 24.1 48 246.1 30.2 98 295.8 36.3 49 48.6 06.0 99 98.3 12.1 49 147.9 18.1 99 197.5 24.2 49 247.1 30.3 99 296.8 36.4 50.4 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30.4 100 297.8 36.5		45 9	05.6	96	95.3	11.7	146	144.9	17.8	196	194,5	23.9	246	244.2	9.9			
49 48.6 06.0 99 98.3 12.1 49 147.9 18.1 99 197.5 24.2 49 247.1 30.3 99 296.8 36.4 50 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30,4 100 297.8 36.5							47	145.9	17,9	97	195.5	24.0	47 2	45.1 7	0.1	97	294.8	36.2
50 49.6 06.1 100 99.3 12.2 150 148.9 18.2 200 198.5 24.3 250 248.1 30,4 100 297.8 36.5								140.9	18.0				48	40.1	0,2	98	295.8	36.3
				100	99.3	12.2	150	148.0	18.2	200	198.5	24.2	250	48.1	0.3	99	296.8	36.4
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	05.0		55	54.5	07.7	05	104,0	14.6	55	153.5	21,6	05	203.0	28.5	55	252.5	35.5
	05.9	00 8	56	55,5	07,8	106	105.0		156	154.5	21.7		204.0		256	253.5	35.6
		01,0		56.4		07	106.0		57	155.5	21.9	1	205.0		57	254.5	-
		01,1	58		08.1	08	107.0	15,0	58	156.5		30	206.0		58	255.5 256.5	
		01.4	60		08.4	IO	108.9		60		22.3	1 .	208.0		60	257.5	
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12		01.7			08,6	12		156	62	1 2	22.6		209,9	1	62	259.5	
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14		01.9	64		08.9	14		15.9	64		122,8	14	1	1 - 1	64	261.4	100
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16		02.2	66	1 3	39,2	116		16.3	166		23.1	17	213.9		67	263.4	
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38	37.	6 05.3	8		1 12.	3		7 19.2		180.	2 26,	33		7 33.3	80	285.2	10.
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44		6 06.1			1 13.1	4	142.	6 20.0	94		1 27.0		241.	6 34.0			
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1	-		00.3	52	51.4		02	100.7			150.1		02	199.5	_	52	248.9	39.4	
1			00 5	53		08.3	03	101.7			151.1		1	200.5	0		249.9		
1			00.6	54	54.3	08.4	05	102.7		54	152,1	120 20	04	201.5			250.9		
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1	9	03.9	01.4	59	58.3	39,2	09	107.7		59	157.0	24.9	09	206.4			255.8		
1	10	09 9	01.6	60	-	9 4	10	108.6	_	60	158.0	250	10	207.4	-	60	256.8	407	
1	11	10.9	01.7	61	1	09.5	111	109.6		161	159.0	25.2	211	208.4	33.5		257.8	40.8	
1	12		01.9	62		09.7		110.6		62		25.3		209,4				41.0	
1	13		02.0		1.	10,0	13		17.6	63	161.0	1	13	100 20			259.8		
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1	17		02.5		1 3	10.5	17		18.3	67		26.1	17	213.3		67	262.7		
1	18		8 02.8				18		18,5	68		26 3		215.3		100	264.7		
1	19	18.	8 03.0	69	1	10.8	19		18.6	69		26,4		216.3		69	265.7		
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1	21		7 03.3				121	131		171	168.9	26.7	221	218.3	34,6	271	267.7	4214	
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	24	100	7 03.8	1 1		1 11.6			5 19.4	11	1	27.2	24	1	33	74	270.6	42,9	
	26	-		-	-	-		-	5 19.7	176	-	27.5			33	276			
	27	1 . 7	7 04.1	11		1 11,9	1	- T	4 19.9			8 27.7	226		1333	77	272.6	1	
	28	1	7 04.	11 -		0 12.2	1 1 2		4 20.0			8 27.8		225.	1333	78	274.6		
	29		6 04.		9 78.	0 12 4	29		4 20.2	11	176.	8 28.0		1. 7	33	79	275.6	43.6	
	30	29	6 04.	7 8	79,	0 12.5	30	128.	4 20.3	80	177-	8 28.2	30	227.2		82	276.6	43.8	
	31		6 04			0 12.7			4 20.5	181		8 28.3		228.2	36.1	281	277-5	43.9	
	32		6 05			0 12.8			4 20.6			8 28,5	1 1 1 1 1 1 1		13 3	82	278.5		
	33	1-	6 05.	1 1	9	C 13.1	1 1		4 20,8	11 -		7 28.6	11			83	279-5		
-	34		6 05.			0 13.			3 21.1	11			11 .			85	280.5		
	36		6 05.		-	_		-	3 21.3		1	-		233.1	-	286	182.4		
2 7	37	1	5 05.	71.		9 13.			3 21.4	1		7 29.2	11	234.	10	87		44.9	
	38	37	5 05.	9 8	8 86	9 13	8 3		3 21.6			7 29.4	38	235.1	37.2	88	284.4	45.0	
	39		5 06.	1 8	9 87.	9 13.	9 39	137.	3 21,	89	186.	7 29.6	39	236.	37.4	89	285.4	145 2	-
	40	39	5 06.		_	9 14.		138.	3 21.	90		7 29,7		237			280,4	45 4	
	41	40	,5 06.	4 9	1 89	9 14.	14		3 22.		138.	7 29.5	24	238.			287.4	45.5	
	42		.5 06.	6 9	2 90.	9 14.	4		3 22.			6 30.0		2 39,				45.7	
	43		,5 06.	7 9	3 91	9 14.	4		2 22.			6 30.		240			289.		1
	44		.4 07.	9 9	5 92	8 14.	9 4		2 22.			6 30.	4		0 38.3	95		4 46.0	
	45	AF	4 07.			8 15.		-	2 22.			6 30.		6 243,			-	4 46.3	1
	47	46	4 07.	4 0	7 95	8 15.	2 4		2 23.	0 9	104	6 30,	4	7 244.	0 38,6	97	202	3 46.5	Ì
	48	47	4 07.	5 9	8 96.	8 15.	3 4		2 23,	1 9	195.	6 31.0	4	8 244.	9 38.8	95	294	3 46.E	I
	49	48	4 07.	7 9	9 97	8 15,	5 4	9 147	2 23.	3 9	1196	.6 31,	1 4	9 245	9 38.9	9	295	3 46.8	l
	50		4 07,			8 15.		0 148	2 23.	5 200		5 31		0 246			296	3 46.9	١
	Dif	t L'e	pLa	D	ft De	Lat	D	ft De	plL	Di	filDer	La	t  Di	A De	pl La	ı Di	it' De	r La	1
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Dift	Lat	Dej	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dei	Diff	Lat	De	Dift	Lat	De
1	01.0	00.2	51	Terror 11	08.8	101		17.5	151	148 7		201	197.9		251	347.2	
2		00.3	52		09.0	02	100.4		52	149.7			198.9			248.2	+3
3	03.0		53	4 200	09,2	03	101.4	1	53	150.7		100000	199 9			249.2	
4	039	00.9	55	17.5	09.5	04	103.4		100	151.7	26.0	04	200.9		54	250.1	
5			- 54	-	-	-	_		55	-		05			55	251 1	-
6		01,0	56	1 -	09.7	106	104,4	18.4	156	153.6	27.1	200	202.9	35.7	256	252.1	
7	07 9		58	1	10,1	08	106.4		57	155.6		08	204 8	26.1	57	253.3	
9		01.0	59		10.2	09	107.3		59	156.6			205.8		59	255.1	
10	39 8	01.7	60	59 1	10.4	10	108.3		60	157 6			206.8	10	60	256 c	45
11	108	01.9	61	60,1	10.6	111	109.3	19.2	161	158.6	27.9	211	207.8	36.6	261	257.0	_
12		02 1			10.8	12	110.3		62	159.5	28.1	12	208.8		62	258.c	
13		02.3			10.9	13	111.3	196	63	100.5	28.3		209,8			259.0	
14		02 4	64	1 -	11.1	14	112.3		64	161 5			210.7		64		
15	1	02 6	65	-	11,2	15	113.3	19.9	65	-	28,6	15	411.7	37.3	65	261.0	_
16		02 8	66	650		116	114,2		166	163.5				10.	266	262.c	
17		02.9	68	1	11.8	18	115.2		67		29.0		213.7			262.9	
19		03.1	69		12.0	19	116.2		69	165 4	29.1		214.7		68	264.9	
20		03.5	70		12.1	20	118.2		70		29.3		216.7		70	265.9	
21	-	03.6	71		12.3	121	119,2	-	171	168.4	_	-	217,6	-	271	266 9	-
22		03.8	72		12.5	22	1	21.2	72		29 8	22	218.6			267.9	
23		04.0	73			23	121.1		73		300		219.6			268.8	4
24		04.2	74	72.5	12.8	24	1	21.5	74	171 4	-		220.6		74	269.8	
25	24,6	04 3	75		13.0	25	123.1	21,7	75	172.3	30.5	25	221.6	19.0		270.8	4
26	25.6	04.5	96	74.8	13.2	126	124 1	21.8	176	173,3	30.5	226	222.6	39.2	276	271.8	4
27		04 7	77		13.4			22.0	77		30.7		123.5	39 4		272.8	148
28		04.9	78		13.5	28		22.2	78		30,9		224.5			273.8	
29		050	79 80		8 13.7	30		22.4	79		31.0		225.5		79	274.8	
30	-	05.2	-			-	-	12.5	-	177.3	31,2	30	226.5	-	80	275.7	-
31	1 2 2 2 2 3	05.4	81		14.0	131	1	22.7	181	178.2			227.5		82	276.7	
32	1-	05.5	83		14.4	33		22.9	83	1 -	31.6		228.5		83	277.7	
34	1	05.9	84		14.6	34	1	23,2	84		21.9		230.4		11 0	279.7	
35		06.1	85	83.7		35		23:4	85				231.4		85	280.7	
36	-	06.2	86		-	136	122.0	23.6	186	183 2	32.3		232.4	_	286	281.6	-
37		06.4	87	85.7	15.1	37	134.0		87				233 4		87	182.6	40
38	37.4	06.6	88	86.7	15.3	38	135.9	23,9	88	185.1	32.6	38	234.4	41,3	88	283.5	40
39	38.4	06 8	89	87.6	15,4	39	130.9		89	186.1			235.4	41.4		284.6	150
40	-	06.9		-	15.6	40			90	187.1			236.3	_		285.6	
41		07.1	91	89.6	15.8	141	138.9		191	188.1	33.1	243	237.3	41.8	291	286,6	5
42		07.3	92	90.0	16.0	42	139.8		92	189,1			238.3		92	287.6	50
43 44		07.5	93	02.6	16,3		140.8	24.0		190.1			239,3 240.3		93	288.5	55
45		07,8	95		16.5	44	142.8		94	191.0			241.3			289.5	
46	45.3				16,6				-						-	-	-
47	46.3	08.1	97	94.5	16.8	146	143.8	25.5	97	193.0			242.3 243,2			291.5	
18	47.3	08.2	98	96.5	17.0	48	145.7		98	195.0			244.2		98	293.5	
19	48.3	08.5	99	97.5	17.2	49	146.7	25.8		196.0			245.2		99	294.5	51
0	49.2	08.7	100	98.5	17.3		147.7			197.0			246.2			2954	
ift	I'e,	Lat				Dift				_	_					_	_
Dift	I'e, l	Lat	Dift	Dep	Lat	Dift	Dep	La	Ditt	Dep	La	it	Dift	Dift Dep	Dift Dep La.	Dift Dep La. Dift	Diff Dep La. Diff Dep

for 80 Deg.

Ditt Lat  De	e, I Dift	Lat	Depl	DiA	Lat	Depl	DA	Lat	Der	Dift	Lat	Dep	Dift	Lat	De
		50,1	_	101	99.1			148.2		201	197.3	38,4	251	246.4	47.4
2 02.000		51.0		02	100.1	WEY SE	52	149.2		03	198.3	38.5	52	247 4	
02		52.c		03	101.1	19.7	53	150.2		03	199 3		53	248.3	
4 03.9 30	.8 54	53.0	10.3	04	102.1	19.8	54	151.2		04	200.2		54	249 3	48.5
5 04 9 01	.0 55	54.0	10.5	05	1031	20.0	55	152.1	_	05	201.2	_	55	250.3	
6 05 9 31	1 56	55 4			104.0		156	153 I	29.8	206	292.2		256	251.3	
	.3 57	56.c	109	1				154 1		07	203.2		57	252.3	
8 07 9 01		56.9		4	106.0		7	155.1			204.2			253,2	
9 08.8 01		57.9			107.0	0.00		156.1		10	205.2		59	254.2 255 2	
10 09 8 01		58.9	-	-	-		_			-		-	261	456.2	
11 10.8 02		59,9	11.0	111	109.0		161			12	203.1		200	257,2	
12 11.8 02	211 - 1	60.9 51.8		12	110.9		14 14 1 1 1	160.0			209.1	7 1 2		258,2	
1 3	3   -	52.8		14	111.9		64	161,0		14	210 1			259 1	
	111 - 1	53.8		15	112.9		65	162.0		15	211.0	41.0	65	260.1	50.6
-   -   -		64,8		116	113.9		166	162 9	_	216	212.0	41.2	266	261.1	50.8
16 15 7 03		65 8	128	17	114.8	22.3	67	163 9		17	213.0			262.1	50.9
18 17.70	1 201	66,7		18	115.8	22.5	68	164.9	32.1	13	214.0		68	263.1	
19 18 7 0	3.6 69	67.7		19	1168		69	165.9		19	215.0			264.0	
20 19.60	3.8 70	68,7	13.4	20	117.8		70	166.9	_	20	215.9	_	70	265.0	_
21 20.6 04	4.0 71	69.7	13.5	121	118.8		171	167.9	32 6	221	216.9		271	266.0	
22 21.6 04		70.7		22	119.8		72	168.8		22	217.9			267.0	
23 22.6 04		71.7	13.9	23	120,7		73	169 8	33.C	23	218.9		73	168.0 269.0	
24 23.6 04		72.6		24	121.7		74	170.8	33.2	24	219.9			269 9	TO TO THE R. P. LEWIS CO., LANSING, MICH.
25 24 5 04		73.6		25	122.7		75	-			221.8		_		
26 25.50			14.5	126	123.7		176	172.8		226	222.8	43.1	276 77	270 9 271.9	
27 26.50	- 11 -		14.7	27	124.7		77 78	173.7		28	223.8	43.3		272.9	
19 28.50	2 2 1 1	77.5		29	126.6	1		175.7	2000	29	224.8	43.7	79	273.9	
	- 1 0	78.5	15.3	30	127.6		80	176 7	34.3	30	225,8	43.9	80	274.8	
-   -   -		_	15,5	131	128 6		181	177,7		231	226 7		281	275.8	53,6
31 30.4 0			15.6	32	129.6		82	178.6		32	227.7		82	276.8	53.8
33 32.40			15,8	33	130.6		83	179 6	54.9	33	228,7		83	277.8	
34 33 4 0	6 5 84	82,5	160	34	131.5		84	180.6		34	229 7		84	278.8	
35 34.4 0	6.7 85	83.4	16.2	35	132 4	25.8	85	180.6	-	35	230.7	44.8	85	279.8	-
36 35.30	6.9 86	84 4		136	133.5		186	182.6			231.7		286	280.7	
37 36.30	7.1 87		16 6	37	134.5	26.1		183.6		37	232.6	45 2	87	281.7	
38 37.30		86.4	16.8		135.5			184 5		38	233.6	45.4	88	282,7	
39 38.30		88 3	17.0		136.4	26,5		185,5	26.2	1 40	234 6 235 6	45.8	90	283.7	55.2
40 19.30		-	17.2	40	137.4					75	1	16.0	-	285.6	
41 40.20	7.8 91	89.3	17.4	141	138 4	20.9	191	187.5	26.6	241	237.5	16.0	29 I 92	286,6	55.7
42 41.20		90.3	17.6	42	139 4		92	189.4	36 8	41	238.5	46 4	93	287.6	55 9
43 42.20		92.3	17.7	43		27.5	93	190.4		44		\$5.6	94	188.6	56.0
45 44,2 0	8.6 95	91.3	18.1	45	142.	27.7	95	191.4		45		46.7	95	289.6	56.3
46 45.20			18.3	146		27.9	196	192 4			241.5		296	290.5	56.6
47 46.10	0.6 07	95 2	18.5	47	144.	28,0	97	193.4	37.6	47	242.5	47.1	97	291.5	56.7
48 47.1 0		96.2	18.7	48	145.	28.2	98	1:94.4	137.8	48	243.4	47.3	98	292.5	56.9
49 48.10	9.3 99	97.2	18.9	49	146.	28.2	99	195.4	38.0	49	244.4		99	293.5	57.0
	9.5 100	98.2	19,1	150	147.	28,6	200		38.2		245 4		300	294,5	
Din Dei	at Dif	De	Lat	Dit	Dep	Lat	Dit	De	Lat	Dif	Dep	Lat	DiA	Dep	Lat
			-				-							-	

					*		19-2	That I go			13.600		and the same			
Diff	Lat  Dep	Dift	Lat	Dep	Din	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Det
	01.0 00.2	51	49.9	10.6	IOI	98.8	21.0	151	147.7	31 4	201	196,6	41.8	251	245.5	52.2
2	02.000.4		50,9	10.8	02	99.8	21.2		148.7			197.6		52	246.5	
3	02.9 00.6	53	51.8	11.0	03	100.7			149.6			198.5			247.4	52.6
4	03.9 00.8		52.8	11.2	04			54	150.6		04	199 5		54	248.4	
5	04.9 01.0	55		11.4	05	102.7	21.8	55	151.6		05	200.5	_	55	249 4	53,0
6	05.9 01.2	56	54.8	11.6	106	103.7		156	152,6		206	201.5	42.8	256	250.4	
1 7	06.8 01.5		55.7		97	104.6		57	153.5		07	202.4		57	251.3	53.5
8	07.8 01.7		56.7			105.6		58	154 5		08	203.4		58	252.3	
9	08.8 01.9		57.7		10				155.5		10	204.4		60	253,3	
10	09.8 02.1	-	58.7			107 6	-	_	156.5	-	-	205.4		-	254.3	-
11	10.8 02.3	61	13001	12.7	1111	108.6		161	157.5		211	206,4		261	255.3	
12	11.7 02.5		61.6		12	1 00			158.4		13	207.3	44.1	62	256.2	
13	12.7 02.7		62.6		13	111.5		64	160.4		14	208.3		64	257,2	54.7
14	14.703.3	65		13.5	15	112.5		65	161,4		15	210.3		65	259.2	
15		-	_		116	113.4	-	166	162.3		216			266	260.1	
16	15.6 03.3	62	64,5	13.7	17	114.4		67	163.3	34.7	17	211.2		67	261.7	55.5
17	17.6 03.7			14.1	18	115.4		68	164.3		18	213.2		68	262.1	55.7
19	18.6 04.0			14 4	19	116.4		69	165.3		19	214.2		69	263.1	56.0
20	- 1			14.6	20	117.4		70	166.3	35,4	20	215.2		70	264.1	
21			-	14,8	121	118.3	_	171	167.2	-	221	216.1	_	271	265.0	c6 4
22				15.0	22		25.4	72	168.2		22	217.1		72	266.0	
23	22.5 04.8			15.2	23		25.6	73	169 2	36.0	23	218.1		73	267.0	
24	23.505.0		72.4		24	121.3	25.8	74	170.2		24	219.1	46.6	74	268.0	57.0
25	The state of the state of the state of	75		15.6	25	122.3	26.0	75	171.2	36.4	25	220.I	46.8	75	269.0	57.2
26		76	74.3	15,8	126	123.2	26.2	176	172.1	36.6	226	221.0	47.0	276	269 9	57.4
27	1 2 1 2			16.0	27	124.2	26,4	77	173.1	36.8	27	222.0		77	270.9	57.6
28		78	76.3	16.2	28	125.2	26 6	78	174.1	37.0	28	223.0	47.4	78	271.9	
29	28.4 06.0	7.9	77.3	16.4	29		26.8	79	175.1		29	224.0		79	272.9	58,0
30	29.3 06,2			16.6	30	-	27.0	80	176 0	-	30	2249		80	273.8	-
31	30.3 06.4			16.8	131	128 1	27.2	181	177,0	37.6	231	225,9	48.0	281	274.8	
32	31.3 06.7		80.2		32			82	178.0	37.9	32	226.9	48.3	82	275.8	58.7
33				17.3	33	130.1		83				227.9		83	276.8	
34				17,5	34	131.1		84	180.0			228,9		84	277.8	59.1
35			83.1		35	132.0		-	-	_	35	229.8	_	_	278.7	-
36				17.9	136	133.0	28.3	186	1		236	230.8		286	279.7	59.5
37	36.2 07.7		85.1	18.0	37	134.0	28.7	89	182.9	30.9	37	231.8	49.3	87	280.7	59.7
38		8.	87.0	18.5	30	135.0	28.0	80	184.8		39	232.8	49.5	89	281 7	60.1
39			88.0	18.7	40		20 1	90	185,8	39.5		234.7		90	283.6	
40			_					1	186 8	20.7	241		-		284.6	
41				18.9	141		29.3	191	187.8	39.7	42	235 7	50.2	92	285.6	
42		92		19.3		139 9	20.7		188.8	40.1		237.7			286,6	
44				19.6	44		30.0	94	189.7	40.4	44			94	287.5	
45		94	92.0	19.8	45	141.8	30.2	95	190.7		45	239 6	51.0	95	288.5	61.4
46				20.0	146	-		196				240.6		296	289.5	
47				20.2		143.8	30.6	97	192.7	41.0	47	241.6	51.4	97	290.5	61.8
48		98	95.8	20.4	48	144.7	30.8		193.6		48	242.5	51.6	93	291.4	
49		99	96.8	20.6	49	145.7	31.0	99	194.6	41.4		243.5	51,8	99	292.4	62.2
50		100	97.8	20.8		146.7	31.2	200	195.6	41.6	250			100	293.4	62.4
	Dep Lat	Dif		Lat	Diff	Dep	Lat		Dep	Lat	Did	Dep	Lat	Diff	Dep	Lat
1-	120/1201	-	1	1				-		'		902		5.2. X		

	Lat	Depl	Dift	Lat	Depf	Dift	Lat	Depl	Dift	Lat	Dep	Dift	Lat	Depl	Dift	Lat	Dep
)111		00,2		49.7		101	98.4	22.7	-		34.0	-	195.9	-	251	244.6	56.5
1		00.4	52		11.7	02	99.4			148.1	34.2	02	196.8	45.4		245.5	
		00.7	53		11.9	03	100.4		_	149.1	34.4	03	197.8	45.7		246.5	
3		00.9	54	52.6	12.1	04	101.3	234		150.1	34.6	04	198.8	45,9	54	247.5	1. A. S. W.
•		01.1	55		12.4	05	102.3	23.6		151.0	34 9	05	199.7	46.1	55	248.5	57.4
- 1		01.3	56		12.6	106	103.3	23.8		152.0	35.1	206	200.7	46.3		249.4	57.6
- 1		01,6	57	55,5		07	104.3	24.1		153.0		1.	201.7			250.4	
7 8		01.8	. 58		13,0	-	105.3			154.0			202.7			251.4	
9.00		02.0	59		13.3	09	106.2	24.5	59	154.9			203.6			252.4	
10		92.2	60		13.5	10	107,2	24.7	60	155.9	36.0	10	204.5	47.2	60	253.3	58.5
-	_	02.5	61	59.4	13.7	111	108.2	25.	161	156.9	36.2	211		47.5	261	254.3	58.7
11		02.7	62	13.	13.9	12	109.1		62	157 9		12	205.6	47.7	62	255.3	58.9
9 1		02.9	63	61.4		13	110.1	25.4		158.8		13	207.5	47.9	63	256.3	59.2
13	12.6	03.1	64			14	111.1	25.6		159.8		14	208.5		64	257.2	59.4
15		03.4	65	63.3	14 6	15	112.1	25.9	65	160.8	37.1	15	209.5	48.4	65	258.2	59.6
16	_	03.6	66	64.3	14.8	116	113.0	26.1	166	161.7	37.3	216	210.5	48.6	266	259.2	59.8
7		03.8		65.3		17	114.0	26.3	67	162.7	37.6	17	211.4		67	260.2	60.1
17		04.0	1 60			18	115.0	26.5		163.7			212.4		68	261,1	60.
19		04.3	69		1	19	116 .	26.8		164.7			213.4			262.1	
20		04,5	70	68.2	15.7	20	116.9	27.0	70	165.6		20	214.4	49,5	70	263.1	60.7
-	_	04.7	71	60.2	16.0	121	117.9	27.2	171	166.6	38.5	221	215.3		271	264.1	61.0
11	21.4	24.9	72			22	118.9		72	167 6	38.7		216.3	49.9		265.0	
22	22.4				16 4	23	119 8	27.7	73	1 00 6	38.9	23	217.3	50.2		266.0	
23	23 4			72.1		24	120.8		74		39.1	24	218.3	50.4	74	267.0	61.6
		05,6	11			25	125.8	28.1	75	170.5	39 4	25	219.2	50 6	75	268.0	61
25	_				17.1	126	122.8	23 3	176	171.5	39.6	226	220.2	50.8	276	268.9	62.1
27	25 3	06.1				27	123.7	28.6	77			27	221.2			269.9	
28	27.1	06.3		76.0	17.5	28	124.7	28.8	78	173 4		11	222.2	51.3		270.9	
29	28.	06.5			17.8	29	125.7	29.0	79				223.1		79	271.9	62.
	29.	06.7	80	78.0	180	30	126,7	29 2	80	175.4	40,5	30	224.1	51.7		272.8	
30	-	07.0	110	78.9	18,2	131	127.6	29.5	181	176.4	40.7	231	225.1	52.0	281	273.8	63.
31	21.3	07,2	82		18.4	32	128.6		82		40 9		226.1		82	274.8	63.
32		07.4			18.7	33	129.6		83		41.2		227.0		83	275.8	63.
34	22.	07.6	11 0	81.8	18.9	34	130.6		84		41.4	1	228.0		84	276.7	63.
35	34.			82.8	19.1	35	131 9	30.4	85	180.	41.6		229.0	52.9		277.7	
36	35.	- 0	86	83.8	19.3	136	132.5	30.6	186				230.0	53,1	286	278.	64.
37		08 3			19.6	37	133.5	30.8	87		42.1		230.9		87	279.	64,
38	27.0	08.5	88		19.8	38	134.5	31,0	88		42.3	38	231.9		88	280.	64.
39	38.	08.8	1 09	86.7	20.0	39	135.4	31.3	89	184.	2 42.5	39	232.9	53.8	84	281.	65.
40	39.	090	90	87.7	20.2	40	136:4	31 5	90		42.7			54.0	99	202.	65.
41	-	09.2		88.	20.5	141	137.4	31.7	191	186.	43.0	241	234.8	54.2	29	283.	65.
42	40	909.4	11		20.7		138.4	31.9	92	187.	1 43.2	42	235.8	54.4	9:	204.	165.
43	41	9 09.7		190.6	20.9	43	139-3	32.2	93	188.	1 43.4	43	236.8	54.7	9	285.	165.
44	42.	009.0	94	191.6	21.1	44	140.3	32.4	94	189	43.6			54.9	94	286.	66.
45	43.	8 10.	9		21.4	1 45	141.	32,6	95	190.0	43.9	45	238.7	55.1		287	
46		8 10.			21.6	146	143.	32.8	196		44.1			55.3	29	288.	1 66.
	44	8 10.		94.	21.8	47	144304	33.1	97	192		47	240.7	55.6		289.	
47	45	8 10.	9	8 95	5 22.0			33.3	98	192.0	44.5	48	241.6	55.8	9	8 290.	4 67.
49	47.	7 11,			5 22.3		145.2	33.5	99	193.9	44.8	49	242.	56.0	9	9 291.	
50	48.	7 11.	100	97.	4 22.5	150	146	33-7	200	194.9	45.0	250		56.2		0 292.	-
		pla		0 5	Lat		Dep	La:	Dia	Dep	Lat	IIn:6	Dep	Lat	ID:	H Dep	La

### 14 Difference of Latitude and Departure for 14 Deg.

Dit	Lat	Depl	Dift	Lat	Dep	Dift	Lat	Dell	Ditt	Lat	Dep	Ditt	Lat	Dei	Dift	Lat	Dep
1	01 0	30.2	-	49.5		101	98.0	24.4	154	146 5	36.5	201	1950	48.6	251	243.5	60 7
	01.9	30.5		50.5	12.6	02	990		52	147 5	36.8	02	196 0		52	244 5	610
3		00.7		51 4		03	99,9		53	148.5		03	W 20 10 10 10 10 10 10 10 10 10 10 10 10 10			245.5	
4		01.0		52.4	11/11/2007	04	100.9		54	149.4		44.1	197.9			246.4	
_5	-	01.2	55	53.4		05	101.9		55	150.4	-	05	198.9		-	247-4	
6		01.5	56	54 3	13.0	106	102.8			151.4			199.9			248.4	
1 7	1	01,7	57		13.8	07	103.8	259	57	152.3	30.0		200.8			249.4	
8		01.9	58		14.0	08	105 8	26.4	58	154.3	38.5		202.8			251.3	
10	1	02.4	60		14 5		106 7		60	155.2	38 7		201.8			252.3	
ii		02.7	61	-	14,8	111	107,7		161	156.2		211	204.7		261	-	-
12		02.6	62		15.0		108.7	27.1		157.2		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	205.7	-		254.2	
13	1	03.1	63	61.1			109.6			158.2		13	206.7	51.5	63	255.	63 6
14	13,6	03.4	64		15.5	14	110.6	27.6	64				207.6		64	256.2	63.9
15	14.6	03.6	65	63.1	15.7	15	111.6	1	65	160.1	39.9	15	208.6	_		257-1	
16		03.9	66		16.0	116	112.6	28.1		161.1		216	209.6	1		258.1	
17		04.1	67	650	16.2	17	113.5	28 3		162.0		17				259.1	
18		04.4	68		16 5	18	114.5	28.0	68			18	211.5			260.0	
19	18.4	04,6	70		16.7	19	115.5	29.0	69		41.1		213.5			261.0	
20	-			-				_	-	-	-	-		-	-	-	-
21	20.4		71		17.2	22	117.4	29.3	72	1	41.4		214.4			263.9	
22		05,6	72		17.7		119 3				41.9					264	
24		05.8			17.9	24	120.3	30.0	74	1 00 0	42.1	24			74	265.9	66.3
25	24	06.0	75			25	121.3	30.2	75	1	42.3	25	- 0		75	266.8	66.5
26		06.3	76		18.4	126	122.3		176	170.8	42.6	226	219.3	54-7	276	267.8	66.8
27		06.5	77		18,6	27	123.2	30.7	77		42.8		6 3 2 7 7			268.8	
28		06.8	78	1			124.2						231.2			269.7	
29	100000	07.0		76.7			125.2				43.3		222.2			270.	
30		07.3	80	-	19.4		126,1		80		43.6	-	-			271.	-
31		07.5	81		19.6	131	127.1	31.7	181		13.8	231				272.	
32	31.0	07:7	82		19.8		128.1		82		44.0	32	225.1	56 4		273.	
33	32.0	08.0	83		20.1	34	129.0	32.4	84		44.5			56.6	8	275.	
35	33.	03.5	85	82.		35	131.0	32,7	85		44.8		1 0 -	56.9	8	276	
36		08.7	86	-		136	132.0		186	_	45.0			57.1	280	277.	60.2
37	34.	09.0		84.4			132.9				45.3	37	230.0				69.5
38		909.2	88	85.4	21.3	38	133.9	33.4	88	182 4		38	230.9	57.6	88		69.7
39	37.	8 09 4	89	86.4	21.5	39	134.9	33.6		183.4	45.7	39	231.9	57.8	8	280.	1699
40		8 09.7	90		21.8	40	135.8	33.9	90		46.0	40	232 9	58.1	90	281.	
41	39,	8 09.9	91	88.	22.0	141	136.8	34.1	191	185.	46 2	141	133.8	58.3	29	282,	3 70.4
42	40.	8 10.2	92	89.3	22.3	42	137.8	34 4	92	186.	40.5	42	234.8	58.0	9:	283.	3 70.7
43	41.	10.4		90.2	22.5	43	138.7	34.0	93	187.	46.7	43		59.0		284.	70.9
44		10.6	94	91.2	22.7	44	139.7	35.1	94		46,9				94	285.	2 71.4
45	43.		95						95							287.	
46	144.	6 11,1	96			146	141.7	35.3	196		47-4		238.7			288	2 71.9
47		6 11.6	97		23.5	48	143.6	35.8	97				240.6	60.0	0	289.	
49		11.9		96.1	24.0	40	144.6	36.1	99	193.1	48.2	49	241.6	60.3	9		72.4
50	48.	12.1		97.0		150	145.5	36.3	200	194.1	48.4	250		60.5			72.6
Dif	2.0	Lai		Der			Dep	La		Dep	Lat	Diff	Dep	Lat	Di	Dep	Lat
-	100		1	, , ,		1	-1						7/1				-

for 76 Deg.

1.14					-	D:A	1	IDan.	ID A	Lat	(Da I	in:a	T	100.11	0:4		-
D A	_	-	Diff	Lat	-	-	Lat		-	Lat		-	-		Dift		
	0.0	00,3	51	49,3	13.2	101			151	145,8	39 1		194.1			242.4	
- 1	01.9		52	50.2		02		26.4		147.8		03	195.1		0.000	243.4	65.2
	02.9		The Control of the	51.2	14.0	03	100.5			148.7		04	197.0		53 54	244.4	65.5
	03.9		54	53.1	14.2	05	101.4		55	149.7		05	198.0		55	246 3	66.0
	05.8	_	56		14.5	106	102.4	-	156	150.7	_	206	199.0		256	247.3	66.3
	05.8		57		14.8	07	103.4			151,6		07			57	248.2	
	07.7	1.00	158				104.3			152 6		- 08	200.9			249 2	
	08.7			57.0	15.3	09	105.3	28.2	1 2	153.6	41.1	09	201.9		59	250.2	
		02.6	60	58.0	15.5	10	106.2	_	60	154.5	41.4	10	202.8		60	251.1	67.3
11	10,6	02,8	61	58,9	15.8	111	107.2		161	155,5		211	203.8	54.6		-	67.5
12	11.6		62	59 9	16.c		108.2		62	156 5	41.9	12		54.9	62		67.8
13		03 4		60.9						157,4		2.7	205.7			254.0	
14		03.6				14		29 5	65	158.4		114				255.0	
15	14 5	03.9	05	-	-	15	-	19.8	166	-	-	-	-	55.6			-
16		04.1	66	1-3/	17.1		112.0		67		43.0	216	209 6	55.9	67		
17		04.4	68	64.7	17.3		113		68	152.	43.5	18		56.4	68	1	
18	1 m . W	04.7	60				114.	30.8	69		43.7	19		56.7	69		
19	March 1	05 2	1			20				164.	44,0	20				260.8	
-	-	-	11-	68,6	-	121	-	31.3	171	165.	44 3	221	213.	5 57,2	271	261.8	70.1
21		05.7		69.5		1 1					1 44.5	22		1 57.5	72		
23	22.2	1 3	1 1 1		10			8 31.8	73		1 44.8	23		4 57.7	73	263.7	
24	23.2	1 .	11					8 32.1			1 45.0	24		4 58.0		264.7	
25	24.1	06 5	7	5 72,4	19.4	25	120	7 32.4	75	-	45.3	25				265.6	-
26	25 1	06.7	7	6 73.4	197			7 32.6			0 45.5	226	218.	3 58.5	276		- 10
27	1 2	07.0	7	7 74.4				7 32.9			0 45.8	27		3 58 7		267.6	
28		07.2						6 33,1		171.	9 46.1	28		2 59.0		268.	- 1.
29		07.5			-			6 33.4		172.	9 46.3	30	0.00	2 59.3		270.	
30	29.0	07.8	-11 =	- 1/	_	-	-	_			8 46.8		-	_		271.	- management
31	29 9			1/		11 3	120.	5 33.9	18		8 47.1			1 59.8			4 72.7
32	30.	08.	8		2 21.2	1		5 34,2	8		8 47.4			1.			4 73.2
33		08,		3 80.3				4 34 7			7 47.6			0 60.6			11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
35		09,	11.					4 34 9		178.	7 47.9		1.0	0 60.8	8	5 275.	
36	34,		- 0	_	-			4 35.2		6 179	7 48,1	23	6 228.	0 61.1	28	6 271,	2 74.0
37		09,	2 0	1-30	0 22.5	1 1 -		3 35	8	180	6 48.4	1 3	7 228.	9 61.3		7 277.	2 74.3
38	36.	09.			0 22.8	3	8 122.	3 35 7	7 8	8 181	6 48,7	3		9 61,6		8 278.	
39	37.	7 10,	1 8		0 23 0		134	3 36 0	8	9 182	6 48.9	3	9 230	9 61.9	8		1 74.8
40	38.	10.	4 9	0 86.	9 23.3	4	135	2 30.	9		5 49.2			8 62.1			75.0
41	39.	6 10,	6 9	1 87.	9 23.6	14	1 136.	2 36.	19	1 184	.5 49,4	24	1 232	8 62.4	29		1 75.3
42	40.	6 10.	0 9	2 88.	9 23.2	4	137	2 36,	9		5 49 7		2 233	7 62.6	9	2 282.	0 75.6
43		5 11.	1 9	3 89.	8 24.1	1 4	3 138	37.0	9	-	4 49.9			.7 62.9 .7 63.1	9	4 284	0 76.1
44		5 11,	4 9	4 90.	8 24.3			1 37.	3 9		4 50.		5 236	6 63.4	9	5 284	9 76.3
45	-	5 11		5 91.				_	_		_	-		.6 63.		6 285	_
46		4 11.		6 92.	7 24.	8 14	141	0 37.	8 19		.3 50.		7 228	.6 63.	1 29	7 286	9 76.9
17		4 12.		7 93.	7 25.	4 4	8 142	0 38,	3 0		.2 51.		8 239	.5 64.	2 6	8 287	.8 77.1
48		4 12.		9 95.	6 25.	6 4	9 142	9 38	6 6	9 192	.2 51.		9 240	.5 64.	4 9	9 288	.8 77.4
50		3 12,	0 10	oc   06.	6 25	9 15	0 144	.9 38.	8 20			8 25	0 241	.5 64.	7 39	00 289	.8 77,
		l.a	15		D 1.a		A D	ep La			ep La	_		La		if De	
-	De	hill's	11	00	D 11.4	110			11-			1	70 115		11		

		The State of				14				and the same							
A C	Lat	Dep	Diff	Lat	Dep	Dift	The second	-	-	Lat	Dep	-	Lat.	-	Ditt	Lat	De
1	01.0	00,3	51	49,0	14.1	101	97.1				41.6		193.2		251	241.2	69.
2	01.9		52	50.0	14.3	02	98.0			146.1			194.1		52	242.2	69.
3	02.9			50,9	14.6	03		28.4		147.1			195.1			243.2	69.
4	03.8			51.9	14.9	04	100.0			148.0	20 10	04	196.1	-		244.1	70.
5	04.8	_	55	52.9	15.2	-05	100.9	20.9	55	149.0	42.7	05	197.0	-	55	245.1	70.
6	05.8	01.7	56	53.8	15.4	106	101.9			149.9		206	198 0		256	246 0	70.
7	06.7	01.9	57	54 8	15.7	07	102.8			150.9		07	1990			247.0	70.
8		02.2	58	55,7	16.0		103.8			151,9	1	08	199.9			248.0	71.
9		02.5	59	56.7	16.3		104.8			152.8		10	201.8		59	248.9	71.
10		02.8	60	57.7			105.7	-				-			1	249.9	71
11		03.0	61	58.6	16.8	111	106.7	30.6	161	154.7		231	202.8	58.2	261	250.9	71
12		03.3	62		17.1	12		30.9	63	155,7	14.0	12	203.8	50.4	6.	251.8	72
13		03.6			17.4	13	108.6		1 .	156 7		13	204.7	100	11 /	252.8	72
14		03.9	64	61.5	17.6	14	110.5		1 -	158.6		15	205.7		65	253 7	72.
15	14.4	04.1		62.5	17,9	-	-	-	_		-	-			_	1-3	73
16	1	04.4	66	63.4	18,2	116	111.5		166	159.5		216	207.6		266	1-33.1	73
17		04.7	67	64.4	18.5	17	112.5	100	68	160.5		18	208.6				73
18		050	68	65.4			113.4		69			19	209.5			1-21	
19		05.2		66.3		19	114.4		70	163.4		20	211.4			258.5	1
20	-	05 5		-		-	-		-	_	-		1	-	1	-	
2 I	1	05.8	71			121	116.3		171			221	212.4		11		1
22		06.1				22	117.3		72			22	213.4		11 '	1 4	1.00
23		06.3	73			23	118.2		73		48,0	23		61.7	73		100
24	23.1	06 6	74		20.4	25	120.1		75		48.2			62.0	75		
25	-	-	-	-		1	-		-		-	1		-		-	
26		07.2	76	1,3		126	121.1		176				1		11 '	1	
27		07.4	77			27	122.1			170.1			1			1 - 2	11
28		08.0	78		0	29	123.0		79	-			1	1 -	79		
30		08.3	80	1, 2 2	100			35.8	80				1.1.	63.4	11 0	1 -	
_	-	-	-	1/3/3	-				181		-		-	-			-
31		08,5	81	11/1.2		131	125.9	36.1			49.9		1	1-	11 -		
32	1-	08,8		1/	22.6	32		36.7		175.9			-	10		272.0	
33 34	100	09,1		80.7		33		36,9		176.8	50.7	34	The second				
35		09,6	85		23.4	35	129.8			177.8			1 2			1 10	1' 0
_	-	-	86	-			-	-	186	_				-			-
36	34,6	09 9		102./	23.7	136	130.7			179.7			227.				
37 38	35.	10,2	88	84.6	24.3	1 28	132,6		88	180.	51.8		128.			276,8	79 79
39		10.5	80	80.0	24,5	39		38.2	89		52,1	39	229.			277.8	70
		11.0	90	86.5	24.8	40	134.6	38.6	90	182.6	5 52.4	40	230			278.7	79
40	-		1	9-	24.8	141	125	28 0	191		52.6		231.			279.7	
41	39.4	11,3	91	87.5	25.1	42	135.5	30.1	02	184.	52.0	42	232.			280.6	80
43	41.	11.9		89.4		42	137.4	130.4	92	185.	53.2	41	233,			281.6	80
44		12.1			25.9		138.4	39.7		186.			234.			282.6	81
45		12.4		91.3		45	139,4	40.0	95		53.7	45	235.	67.5	95	283.5	81
46					_		140.	-		188.4			236.			284.5	
47		12,7	97	92.3	26.5	47	141.			189.		47	237.	68.	97	285.5	8
48		13.2	08	93.2	27.0	48	142.2	40.8	08	190.	54.6	48		68.	98	286.4	8
49	1 2 2 2 2 2	13.5		95.2	27.3		143.2	41.1	99		54.8	40	239.	68.6	90	287.4	
50		13,8	100	96.1	27.6	150	144.2			192.2			240.	68.9	300	288.3	
		1-3,	The same of	. 10	Lat	11		-1	1			1 1		Lat	11-		1-

### Difference of Latitude and Departure for 17 Deg.

n a	Lat	Dep	Dia	Lat	Depl	Dift	Lat	Dep	Dift	Lat	Day 1	ID	let .	115			1
-	_		_		-	-			-	-	Dep	-	Lat.	-	Dift	Lat	De
1	01.0	1 2	51	100	14.9	101		29,5	151	144.4		1	1191.2	1-	251	240.c	73.3
2		00.6	52	49,7	15.5	03	97.5	30.1	52	45,3	44 4	02	1 ,,	1	52	241.0	73.6
3		01.2			15.8	04		30.4	54	146.3		03	1		53	241.9	739
5		01.5	55	52.6	16.1	05	100.4		55	148.2		04	100		54	242.9	74.1
-6	-	01.8	56	53.5	16.4	106	101 4	-	156		-	-	-	-	55	243.8	74.4
7		02.0	57	54 5	16.7	07	102.3		1	149.2		206	1 21		256	244.8	74.7
8		02.3	58	55,5	17.0	08	103.3		100	151,1		08			57		75.0
9	1 2 2	02.6		56.4	17.2	09	104.2			152.0		09	1			246 7	75.3
10	09.6	02.0	60	57.4	17.5	10	105.2	32.2	60	-	46.8	10	1		60	248.6	75.6
11	10,5	03.2	61	58.3	17,8	111	106.1	32.4	161	154.0	47.1	211	-	-	261		75 9
12		03.5	62	59.3	18,1	12	107.1		62	154.9		12			62	249.6 250 5	76.2
13		03.8	63		18.4	13			63	155.9	47.6	13		62.3	11 1 1 1 1 1 1 1	251.5	76,5
14	13.4	04.1		61.2	18.7		109 0	33.3	04	156 8	47.9	14		62.6		252.4	77.1
15	14.3	04.4	65	62.2	19.0	15	110.0	33.6	65	157,8	48,2	15			65	253 4	77.4
16	15.3	04.7			19.3	116	110.9	33 9	166	158.7		216	206.5	63 1	266	2544	77.7
17		05.0			19.6	17	111.9	34,2	67	159.7	48.8	17			67		77.9
18		05.3		1	19.9	18	112.8	34.5		160 6		18				256.3	78.2
19		05.6		66.0	20.2	19				161.6		19	209.4			257.2	78,5
20	-	05.8	1-	66.9	20 5	20	114.7	35.1	76	152.6	49 7	20	2104	64.3	70	258 2	78.8
21		06.1	71	67 9	20 8	121	115.7		171	163.5		221	211.3	64 €	271	259.1	79.1
22	1	06 4		68,8	21.0	22		35 7	72	164.5		2.2	212.3	64 9	72	260.1	79.4
23	1 24	06.7		69 8	21.3	23	117.6		1		50 6	23	-	-	73	261.1	79.7
24		07.0	10000	1	21.6	24	118.6			166.4		24				262 0	800
25	_	07 3	75	71.7	21.9	-	119 5		75	167.3		25	-		75	263.0	80.3
26		07.6	76	72,7	22.2	126	120.5			168.3		226	1				80 6
27		07.9	77	73.6	22.5	27	121.4			169.3		27			77		80.9
29		08.5	79	75.5	23 1	29	123 4	37.7		171.2		29	1				81.2
30		08,8		76.5		30	124.3		0	172.1		30			80	256.8	81 5
31	-	09,1	81	77.5	23.7	131	125.3	-	181	173.1	-	-		-	-		-
32		09.4	82	78.4	24.0	32	126,2	28.6	82	174.0		32				268.7	82.0
33		09,6				33	127.2			175.0	53.5	33	-		82	270.6	82.3
34	1-	09 9	84	80.3	24,6	34		39.2	84	175.9	53.8	34			84	271.6	82.9
35	33.5	10,2	85	81.3	24.8	35	129.1	39.5	85	176.9		35		100	85	272.5	83.2
36	34,4	10.5	86	82.2	25.1	135	130.0	39.8	186	177.9	54.4	236	225.7	69.0	286	273.5	83,5
37	35.4	10 8	87	83,2	25.4	37	1310	40.C	87	178.8	54.7	37	226.6			274.4	838
38	36.3	11.3	88	84.1	25.7	38	132.0	40.3	88	179.8	55.0	38	227.6	69.6	88	275.4	84.1
39	37.3	11.4	89	35. I	20,0	39	132,9	40 6	89	180.7	55.2	. 35	123 5	69.9	89	276,4	84 4
40	38.2	11.7	-	-	26.3		133.9			181.7		40		70,2		277.3	84.7
41		12.0	91	87.0	26.6	141	134 8	41,2	191	182.6	55.8	24	230 5	704	-	278.3	85.0
42		12.3	92		26.9	42	135.8	41.5	92	183.6	56.1	4:	231.4	70.7	92	279.2	85.3
43		12,6			27.2		136.7			184.6					93	280 2	85.5
44		12,0	94	39.9	27.5		137.7	42.1	94	185.5	50.7					281.1	85.8
45		13,2	95	90.8	27.8	45	138 7			186.5		4		-		282.1	86.1
46		13.4	90	91.8	28.1	146	139,6		196	187 4	57.3	24		71.9	1296	283.0	86.4
48	44 9	13.7	97	192.8	28.4	47	140.6		97	188.4	57.6				97	284.0	36.
49	45.9	14.0	90	93.7	28.6	48	141.5		98	189.3	57.9		237.1	72.4	08	285.0	37.0
50		14,3	100	94.7	29.2	49	142.5	43.8	99	190.3	158.5	4				285.9	87.
Did	-						De	13.					239.1		- maria	286.9	-
-	Deb	La	1 711	Del	Lat	11210	Del	179	ווטוו	Dep	1 Ts.	DI	AlDep	Lau	Di	t Dep	La

for 73 Deg.

_								115	12.0		10	10:0	. 7	10	1000		
DA	Lat	Det	Diff	_	_	Dift		_		Lat	- Bridge			Del	Dift		Dep
1			51	48,5	15.8	101		31.2	151	143.6	46.7		191.2			238.7	
2	01.9			49,5	16.1	02	97.0	31.5		144.6		03	1	62.7		239.7	
3	02.9		53	51.4	16.7	04		32.1	54	146.5		04			54	241.6	78,5
5	04.8		55	52.3	17.0	05		32.4	55	147.4		05	- Tr. 10.5		55	242.5	78.8
6	-	01.9	56	53-3	17.3	106	100.8	32.8	156	148.4	48,2	206	195.9	63 7	256	243.5	79.1
7	06.7	02.2	57		17.6	07	101.8		57	149.3	48.5	07			57	244.4	1
8		02.5	58	55,2	17,9		102.7	and the second		150.3	48.9	08	1 20			245.4	
9		02.8	59	56.1	18,2	10	103.7		59	151,2		10			59	246 3	
10	_	03.1	61	31	18.8		105.6		161	153.1	-	211		-	261	248.2	80.6
11		03.4	62	13	19.2		106.5			154.1		12			62	249.2	
13		04.0	63	133.	19.5	13	107.5		63	155,0	50.4	13				250.1	81.3
14		04.3	64	60.9	19.8	14	108.4			156 0		14		66.1			81.6
15		04.6	65	-	20.1	15	109 4	_		156.9	_	15	-			252.0	-
16		04.9	66	100.0	20.4	116	110.3	35.8	166	157,9	51.3	216		65.7	266	253.0	82.2
17		05.3	68	1 0 /	20.7	18	111.3 112.2	26.5		158.8		17	7.77		68	253 9 254 9	82.5
19		05.6		64.7	21.0	19	113 2	36.8		160 7		19	1 0			255.8	
20		06.2	70	1 -		20	114.1		70	161.7		20	1		70	256.8	83,4
21		06.5	71	67.5	21.0	121	115.1	37.4	171	152.6	52.8	221	210.2	68.3	271	257.7	83.7
22		06.8	72	68,5	22.2	22	116.0	37.7		163.6		22		68.6		258.7	84.0
23		07.1	73				117.0	38.0		164.5		23		1 -		259.6	
24		07 4	74	1.		24	117.9	28.6	74	165.5		24		1	75	260.6	84.7
25		07.7	75	-	_	1	119 8		176	_		226		-	_		85.3
26	24.7	08 o 08.3	76		- 0	126	120.8			168.3		27	100			263.4	85.6
28		08,7	78			28	121.7			169.3		28	216.8	70,5	78	264.4	85.9
29	27.6	09,0	79	75.1		29	122.7	39.9		170.2		29				265.3	86,2
30	28.5	09.3	80	/	24,7	30	123.6		80	-	_	30		_	80	266.3	86.
31	29.5		81	11/1-		131	124.6		181	172.1	55.9	231			281 82	267.2	86.8
32		09 9	82	1,		32	125.5	41.1	82	173.1	56.5	32	1				87.1
33	31.4	10,2	84		25.6	33	127.4			175.0		34					87.8
35	33.3	10.8	85		26.3	3.5	128.4			175.9		35	223.5	72.6		271.0	
36	34,2	11.1	86	81.8	26.6	136	129.3	42.0	186			236				272.0	88,4
37	35.2	114	87	82.7	26.9	37	130.3	42.3	87	177.8	57.8	37		73.2	87	272.9	88.7
38	36.1	11.7	88	83,7	27.2	38	131.2	42.0	89	178.8	58.1	39	226.3	73.5	80	273.9 274.8	89.3
39	37.1 38.0		00	85.6	27.5 27.8	40	132,2 133.1	43.3	90	180.7	58.7	40		74.2	90	275.8	89.6
40	-		91	86.5	28.1		134.1	,	191	181.6	50.0	241		-	_	278,7	
	39.0		92	87.5	28.4	42	125.0	43.9	92	182.6	59.3	42	230.1	74.8	92	277.7	90.2
43	40.9		93	88.4	28.7	43	136.0	44.2	93	183.5	59.6	43	231.1	75.1	93	278.6	90.5
44	41.8	13.6	94	89 4	29.0	44	136.9	44.5	94	184.5	59.9		232.0			279.6	
45	42.8	13,9	95	90.3	29.4	45	137 9	44 8	95	185.4		45			-		anuminos
46	43.7	14.2	96	91.3	29.7	146	138 8	45.1	196	186.4	60.6	47	233.9	76.0	290	281.5	91.5
48	44.7	14,5	97		30.0	47	139,8	45.4	97	187.3	61.2	48	235.8	76.6	98		91.0
	46.6	15.1		94.1	30.6		141.7		99	189.2	61.5	49	236.8	76.9	99	284.3	92.4
50	47.6	15.5	100	95.1	30.9	150	142.7	46,4	200	190.2	61.8	250	237.8	77.3	300	285.3	92.7
	Dep	lai	Dift	Dep			De		Dift	Dep	La	Diff	Dep	Lat	Dift	Dep	Lat
-	-	11			1 . 1	1			1				A SE			-	

5.0	Tat	(Dep	IDif	Lat	Dep	Difti	Lat	Depl	Dif	t L	at I	Deply	Dift	Lat	Deple	Dift	Lat	Dep	
-	_	_			16.6	101		32.9	151	14	2.8	19.2	201	190.0	65.4	251	237.3	81.7	1
1,		9 00.3		1.	2 16.9	02		33.2	5:		3.7			191.0		52	238 3	82.1	
3		8 01.0		A SEALON V	1 17.3	03		33.5	5	3 14	4.7	19,8	03	191.9	66.1	53	239.2	82.4	1
1 4		8 01,3		51.	1 17.6	04		33.9	54	4 14		50.1	1112	192.9			240.1		
5	04.	701.6			0 17.9	05	99.3	34.2	5	944	6.5	_	05	193.8	-	-	241.1	-	- 1
6		7 02.0		_	9 18.2		100.2		15	- 1	7.5		206	1 .			242.0		
7		6 02.3			9 18,6	07		34.8	5	7 14	9.4	51.1	07	195.7		57	243.0	83.7	
8		6 02.6			8 18.9 8 19.2			35.2	5	0 1 5	0.2	51.8		197.6		50	244 9	84.	2
9		5 03.3			7 19.5	11		35.8	6	0 15	1.3	52.1		198.			245.8		
10			-	-		111	-	36.1	16	_	_	52 4	-	199.	-		246.8	-	- 1
11		4 03.6	110	2 58	6 20.2		1051	36.5				52.7			69.0		247.7		
13		3 04.2	11 -		.6 20.5		106.	36.8	6			53.1			69.4		248.		
14		2 04.	6 6.		.5 20.8			37.1	1 6			53.4			69.7	64	249.	86.	0
15	14	. 2 04,	9 6	5 61	.5 21.2	15	-	37.4				53.7		-	70.0		250.	_	-
16	1 3	1 05.	11 0		4 21.5		109.	37.8	16			54.0			70.3		251.		
17		.1 05	- 11 -		.3 21.8	11 0	110.	6 38.4	115			54.4			71.0		252.		
18	1 0	.0 06.	7 1 -		.3 22.1	11		5 38.7				55.0			1 71.3		254.		
19		.906.	. 11		.2 22.8		113.	5 39.1				55.4		1	0 71.6		255.		
2		.9 06.		_	.1 23,1	-11-	-	4 39.4	-			55-7	_	1 208.	9 72.0		1 256.	_	
2:		.8 07.	2 7		.1 23.4			3 39.	7	72 1	62.6	56.0	2	2 209.	9 72.3	7:	2 257.	2 88.	.6
2		1.7 07	5 7	3 69	0.0 23.	8 23		3 40.0		73 1	63.€	56.	3 2	-	8 72.6		3 258.		
2.	4 22	.7 07.	.8 7	74 70	0.0 24.	1 24		2 40.				56.		7	8 72.9		4 259		
2	_	6 08		_	0.9 24		-	2 40.				57.0			7 73,3	-	5 260	_	_
2	6 24	4.6 08	5 7		1.9 24.			1 41,				57-	3 22		7 73.6		6 260		
2		5.5 08	.8		2.8 25.			0 41.	7	77	68.	3 57. 3 58.	0 2		6 73.9		7 261		
2		7.4 09			3.7 25. 4.7 25.	.11		.0 42.	-11	79	169.	2 58.	3 2		5 74 6		9 263		
	-	8.4 09			5.6 26.	. 11	-	9 42,		80	170.	2 58.	6 3		.5 74 9		0 264		
	-  -	9.3 10	-11-	_	6.6 26.	_	_	.9 42.	-1 1-			1 58.		1 218	4 75.2	28	1 265	-7 91	1.5
		0.3 10	-		7.5 26		2 124	.8 43.	0	82	172.	1 59.	3 :	32 219	.3 75.5	5 8	2 266		
		1.2 10			8.5 27.		3 125	.7 43	3		C	0 59	-11		-3 75.		3 267		
		2.1 11	1,1		9.4 27			,7 43				0 59			.2 76.		84 268 85 269		
		3.1 11			0.4 27	_	-	.6 44	- 1	-	_	9 60			_		_	-	
		14.0 11			1.3 28			.6 44	21.1	186	175	8 60		36 223	76.		86 270		
	37 3	15,0 12	2,0	87 8	3.2 28	3	7 120	0.5 44	.0			7 61			.0 77.		88 272		
1	39	35.9 I	2.7		4.1 29	.01	9 13	1.4 45	.3	80	178	7 61	.5	39 22	5.0 77.	8	89 27		
	40	37.8	3.0		35.1 29	.3	10 13	2.4 45	.6	90	179	.6 61	.9	40 22	5.9 78.		90 27		
		38.8			86.0 29			3.3 45	25.	191	180	6 62	.2 2	41 22	7.9 78.	5 2	91 27	5.19	4.7
	42	39.7	3.7	92 8	87.0 30	0.0	42 13	4.3 46	.2	92	181	.5 62	. 5	42 22	8.8 78.	9	92 27		
	43	40.7 1	4.0	93	37.9 30	0.3	43 112	5.2 40	1.0		182	5 62	.8	43 22	9.7 79	1	93 27	7.09	5.4
		41.6			88 9 30	0.6	44 13	6.1 46	,9	94		4 63		44 23 45 23	0.7 79	8	94 27 95 27	8.00	5.7 6 T
		42.5		95	89.8	- 9	45 14	7.1 47		95	-	_	-		1.6 79	- 1 -			
1	46	43.5	5.0	96	90.8 3	1.3	46 13	8.0 47	1.5	196		.3 64		46 23	2.6 80 3.5 80	4 2	96 27		
	47	44.4	15.3	97	91.73		47 13	9.94	3.2	97		.2 64		48 23	4.5 80	7	98 28		
	48	45.4	16.0	90	92.7 3		49 14	0.94	8 5	99	188	.1 64	.8	49 27	5 4 81	1	99 28	32.7	97 4
15.	50	47.3	16.3	100	94.53		50 14	1.8 4	8.8	200		1 6		50 2	6.4 81	4	300 2	83.6	97.7
		Dep			Dep			ep I		_		PL		Dinid			Diff	ep	Lat
1 23	-	10col	241			1							-11		-		1000		. 10

for 71 Deg.

		W. E.			11/2							1	100			-	75.75
Diff	Lat	Dep	Dift	Lat	Dep	Din	Lat	Dept	DA	Lat	Del	Dif	Lat	Dep	Dift	Lat	Dep
1	00.0	00.3	51	47.9	17.4	IOI	94.9	34.5	151	141.9	51 6	201	188.9	68.7	251	235.9	85.8
2		00.7		48.9		02	95.8	34,9		142.8			189 8		52	236,8	86.2
3		01.0		49.8		03	96.8	35.2	53	143.8	52.3	03	190.8	69.4	53	237.7	86.5
4	03.8	01.4	54		18.5	04		35.6	54	144.7		04	191.7	69.8	54	238.7	86.9
5		01.7	55	51.7	18.8	05	98.7		55	145.7		05	192.6	70.1	55	239.6	87.2
6	_	02.1	56	52.6	10.2	106	99.6		156	146 6	93.4	206	193.6	70.5	256	240.6	87.6
7		02.4	57		19.5	07	100.5		5.7	147.5		07	194.5		57	241.5	87.9
8	1	02.7	58		19.8	08	101.5		58	148.5			195 5		58	242,4	88.2
9		03.1	59	55 4		09	102.4		59	149.4		09	196,4	71.5	59	243.4	88.6
10		03 4	60			10	103 4	37.6	60	150.4	54.7	10	197.3	71.8	60	244 3	88.9
11	_	03.8	61	57.3	20.0	111	104.3	28.0	161	151.3	55.1	211	198.3	72.2	261	245.3	89.3
12	11.2	04.1	1 2		21,2	12	105.2	28,3		152.2		1.00	199 2		62	246.2	89.6
13		04.4		59,2		13	-			153.2		13	200.2		63	247.1	89.9
14		04.8	110	60.1	1	14	107.1		64	154.1		14		73.2	64	248.1	90.3
15	1	05.1	65	61.1	22.2	15	108.1	39.3	65	155.1		15	202.0		65	249 0	90.6
16	-	05.5	66	62.0	22.6	116	109.0	_		156.0		216	203.0	_	266	250.0	91.0
17		05.8		63.0		17	109.9	1 1	67	156,9			203.9		67	250 9	91.3
18		06.2		63.9		18	110.9		68	157.9		18	204.9		68	251.8	91.7
19		06,5			23.6	19	111.8	1	69	158.8		19	205.8	74.9	69	252.8	92.0
20		06.8		65.8		20	112.8		. 70	159.7			206,7		70	253,7	92.3
21	10.	07.2	73	66,7	-	121	113.7	ATA	171	160.7	-	221	207.7		271	254 7	92.7
22		07.5			24.6	22	114.6			161,6		22	208.6	75.9	72	255.6	93.0
23		07.9			25,0	23	115.6		73	162.6			209.6		73	256.5	93.4
24		08.2	11	69.5		24	116.5		74	163.5		24	210.5	1 1	74	257,5	93.7
25		08.6		70.5		25	117.5		75	164.4		25	211.4		75	258,4	94.1
26		08.9		-	26.0	126	118.4		176	165.4	_	326	212.4	-	276	259 4	94.4
27		09.2			26.9	27		43.4	77	166.3		27	213.3		77	260.3	94.7
23		09.6	11		26.7	28	120,3		78	167.3	60.9		214.3		78	261.2	95.1
29		09.9	11		27.0	29	121.2		79	168.2	61.2	29	215.2		79	262.2	95.4
30	28.	10.3	80		27.4	30	122.2		80	169.1	61.6	30	216.1	78.7	80	263.1	95.8
31	29.	-	1	-	27.7	131	123.1	-	181	170.1	61.0	231	217.1	70.0	281	264.1	96.1
32		10.9	11 2	1/	28.0	32			82	171.0		32	218.0	79.2	82	265.0	96.4
33		11,3	11 0		28.4	33	125.0		83	172.0			219.0		83	265.9	
34		11.6	11 -		28.7	34		45.8	84	172.9		34	219.9		84	266.9	
35		12.0			29.1	35		46.2	85			35	220.8	80.4	85	267.8	97.5
36		8 12.3	-	-	29.4	136	-	46,5	186	174.8		236	221.8	A company	286	268.8	97.8
37		12.7			29.8	37		46 9	87	175.7			222.7		87	269.7	98,2
38		7 13.0	88	82.7	30.1	38	129.		88	176.7	64.3	38	223.6	81.4	88	270.6	0
39	36	6 13.3	1 80	81.6	30.4	39		47.5	1 89	177,0	04.0	39	224.6	81.7		271.6	98.8
40	37.	6 13.7	1 90	84 6	30.8	40	131.6	47.9	90		65,0	40	225,5	82.1	90	272.5	99.
41		5 14,0		-	31.1	141		48.2	191	179.9	65.2	241	226.5		_	273.5	-
42		5 14.4	02	86.	31.5		122.	48,6	92	180.4	65.7	42	227.4	82.8	92	274.4	
43		4 14.7	9	87.4	31.8	43		48.9	93	181.4	66.0	43	228,3	83.1		275.3	
44		315.0	1 94	88,	32.1	44	135.	49.2	94	182.3	66.3	1 44			94	276.3	100
45		3 15.4	9	89	32.5	45	136.	49 6		183.2	66.7	45		83.8	95	277.2	100
46		15.7		00.1	32.8	146		49.9							296	278.2	
47		16.1			33.2		128	50.3	07	184.2	67.4	47	232.1	84.5	97	279.1	
48		164			33.5		130	50.6	98	186.1	67.7	48	2 33.0	84.8	98		101,
49	46	16.8	99		33.9			51.0		187.0		49	234.0	85.2	99		102.
5 8		E 17.1			34.2		140		200	187.	68.4	250	234.9	85.5	300	281,0	102
10	De	Lat		-	La		Dep		Die	Dep	1.3	Dif	Dep	Lar	Diff		Lat
16	1000	Lat	1101	De	Ina.	Ilpin	Inch	Ton.	Ilpin	L'och	Lua	11-11		LDat	1 Page	-Den	1 12

Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dei	Dif	Lat	Dep
1		00.4	51		18,3	101	94-3	36.2		141.0		201	187.6	72.0	251	234.3	90.0
1		00.7		48.5		02	95 3	36.6		14119		02	188.6	72.4		235 3	90.3
3		01.1		49.5		03		36.9	53	- 0		03	189 5	72.8	1 1 2 2	236.2	
4	04.7	01,4	54	51.3		05		37·3 37.6	54			05	191.4			237.1	91.4
5	05.6	-	56	-	20.1	106		38.0	156		-	206	192.3	_	-	239.0	91.8
7	06.5		57	53.2	20.4	07	99.9	38.3	57	146.6		4	193.2			239.9	92.1
8	07.5	02.9	58	54. I		08	100.9	38.7	58	147.5	56.6		194.2			240.9	92,5
9	€8.4			55,1		09	101.8	39.1		148.5			195.1			241.8	92.8
10	09.3	03.6	-	56.0		10	102.7	4	-	149.4	_	10	196.0	75.3	_	242.7	93.2
11	10,3	1		56.9		111	103.7	39.8		150.3		211	197.0		261	243.7	93.5
12	11.2			57-9 58.8			104.6			151.3			197.9			244.6	the state of the state of the
13		04.6	64	59.7		14	106.5			153.1			199.8		1	245.5	94.5
15	14.0	-		60.7		1	107,4		65		59.1		200.7			247.4	95.0
16	14.9	-	_	61.6			108.3		166	-	-		201.6	77.4		248.3	95.3
17	15.9	06.1		62.5		17	109.3			155.9	59.9		202.6			249.3	95,7
1.8	16.8		68	63.5	24 4	18	110.2		68	156.9	60,2		203.5		68	250.2	96.1
19	17.7			64.4		1	111.1		34	157.8	60.6		204.4			251.1	96.4
20	18.7	-	-	65.3	-	20	112.1	43.0	70		_	_	205.4	-		252.1	96.8
21	19.6		71	66.3	25.4	121	113.0		171		61.3		206.3			2530	97.1
22	20.5			67.2			113.9			160.6			207.2			253.9	97.8
24	22.4			69.1	2 2 2 10	23	115.8		73				209.1			254.9	98.2
25	23.3		75	70.0		25	116.7		75	41			210.0			256.7	98.6
26	24.3	-	76	70.9	27.2	126	117.7	-	176	164.3	-	226	211.0	81.0	_	257.7	98.9
27	25.2		77	71.9	27.6	27	118.6		77	165.3	63.4		211.9			258.6	99.3
28	26.1			72.8		28	119 5	45.9	78	166.2	63.8		212.8			259.5	
29	27.1		79	73.7	28.3	29	120.5		79	167.1	64.2		213.8			260.5	
30	23.0		_	74.7		30	121.4	_	-	168.1	-	-	214.7	THE PERSON NAMED IN	_	261.4	
31	28.9			75.6		131	122.3		181	169.0		231	215.6 216.5	82.8	281	262.3	100.7
32	30.8	11.8	1	76.5		32	123.3		1 1	170.9			217.5		82	263.3	101.4
34	31.7	12,2		78.4			125.1			171.8			218.4			265.1	
35	32.7	12.5	1 0 1	79.3		35	126,1		85	172.7	66.3	35	219.4	84.2		266.1	
36	33.6	12.9	86	80.3	30.8	136	127.0	48.7	186	173.7	66.7			84.6	286	267.0	102.5
37	34.5	13.3	87	81.2	31.2	37	127.9	49.1		174.6		37	221.2	84.9	. 87	267.9	102.9
	35,5		88	82.1	31.5	38	128.9	49.5	88	175.5	67.4	38	222.2	85,3	88	268.9	103.2
	36.4		90	84.0	31.9	40	129.8	50.2	00	176.5 177 4	68.1	40	224.1	86.0		269.8	
40	37.3		_			-	-			178.3			225.0		90		
	38.3		91	84.9	32.0	141	131.7	50.0	191	179.3	68.8	42	225.9	86.7	02	271.7 272.6	104.3
	40.1		93	86.8	33.3	43	133.5	51.3	93	180.2	69.2	43	226.9	87.1		273.5	
44	41.1	15.8	94	87.7	33.7		134.5		94	181.1	69.5	44	227.8	87.4		274.5	
45		16.1	95	88.7	34.0	45	135.4	52.0	95	182,1	69.9	-				275.4	
46		16.5	96	89.6	34 4		136.3		196	183.0	70.2	246	229.7	88.2	296	276.3	106.1
47	43.9	16.8	97	90.5	34.8	47	147.3	52.7	97	183.9	70.6	47	230.6	88.5	97	277.3	106.4
48		17.2		91.5			138.2			184.9	71.0	48	231.5	88.9		278.2	
49 50	45.7	17.6	100	92.4	35.5		139.1		99	185.8	71.7	250	232.5 233.4	89.6		279.1	
2	140./	17.9	100	93.4	22.0	150	140.1	23.0					-334	3.0	1300	200.1	10/.5
7:0	Dep	T	500	D	T	200	Dep	T	D.0	Dep	Las	D: 12	Dep	1	100	Dep	T

for 69 Deg.

2 01.6 3 02.8 4 03.7 5 04.6 6 05.6 7 06.8 9 08.9 10 09.1 11 10.1 12 11.1 13 15.1 14 13.1 15 13.1 16 14.1 17 15.1 18 16.1 19 17.2 20 18.2 21 22.2 22 23.2 24 22.2 25 23.2 26 24.2 27 25.2 28 26.2 29 26.3 30 37 38 35.3 37 38 35.3 37 38 35.3	9 00 .8 01 .7 01 .6 01 .6 02 .4 03 .3 03 .3 03 .2 04 .1 04 1 04	4 5 5 5 5 5 5 5 5 5 5 5 6 5 5 6 6 5 5 6 6 6 5 6	47.3 48.2 49.1 50,1 551.0 551.0 551.0 551.0 551.0 551.0 551.0	19,1 19.5 19.9 20.2 20.6 21,0 21.4 21.7	101 02 03 04 05 106 07 08	96.4 97.4 98.3 99.2	37.8 38,2 38.6 39.0 39.3 39.7	151 52 53	140.0 140.9 141.9	56.6 56.9 57.3 57.7 58.1	201 02 03 04 05	Lat 186.4 187.7 188.2 189.1 190.1	75·3 75·7 76.0 76.4 76.8	52	Lat   232.7   233.7   234.6   235.5   236,4	94.4 94.8 95.2 95.5
2 01.6 3 02.8 4 03.7 5 04.6 6 05.6 7 06.8 9 08.9 10 09.1 11 10.1 12 11.1 13 15.1 14 13.1 15 13.1 16 14.1 17 15.1 18 16.1 19 17.2 20 18.2 21 22.2 22 23.2 24 22.2 25 23.2 26 24.2 27 25.2 28 26.2 29 26.3 30 37 38 35.3 37 38 35.3 37 38 35.3	.9 00 .8 01. .7 01. .6 01. .6 02. .4 03. .3 03. .3 03. .2 04. .1 04. 04.	7 5: .1 5: .5 5. .9 5 .2 5: .6 5: .0 5: .7 6: .7 6: 5 6:	48.2 49.1 50,1 551.0 551.0 552.9 553.8 54.7 55.6	19.5 19.9 20.2 20.6 21,0 21.4 21.7 22.1	02 03 04 05 106 07 08	94.6 95.5 96.4 97.4 98.3 99.2	38,2 38.6 39.0 39.3 39.7	52 53 54 55	140.9 141.9 142.8 143.7	56.9 57.3 57.7 58.1	02 03 04 05	187.7 188.2 189.1 190.1	75,7 76.0 76.4 76.8	52 53 54	233.7 234.6 235.5	94.4 94.8 95.2
3 02.3 4 03.5 5 04.6 6 05.6 7 06.8 9 08.9 10 09.1 11 10.1 12 11.1 13 12.1 14 13.6 15 13.1 15 13.1 16.1 19 17.2 20 18.2 21 19.2 22 23.2 24 22.2 28 26.2 29 26.3 31 28.3 32 29.3 33 32.3 34 31.3 35 36 37 34.3 38 35.3 37 34.3 38 35.3	.8 01. .7 01. .6 01. .6 02. .5 02. .4 03. .3 03. .3 03. .1 04. .1 04.	.1 5: 5 5 5 9 5 .2 5! .6 5: .0 5: 4 5: .7 6: .1 6 6:	50,1 50,1 51.9 7 52.9 8 53.8 9 54.7 9 55.6	19.9 20.2 20.6 21,0 21.4 21.7 22.1	03 04 05 106 07 08	95.5 96.4 97.4 98.3 99.2	38.6 39.0 39.3 39.7	53 54 55	141.9 142.8 143.7	57·3 57·7 58.1	03 04 05	188.2 189.1 190.1	76.0 76.4 76.8	53 54	234.6 235.5	94.8
4 03: 5 04: 6 05: 7 06: 8 07: 9 08: 10 09: 11 10: 12 11. 13 12. 14 13: 15 13: 16 14: 17 15: 18 16. 19 17. 20 18. 21 19. 22 23. 24 22. 25 23. 26 24. 27 25. 28 26. 30 27. 31 28. 32 29. 33 33. 34 31. 35 36 33. 37 34. 38 35.	.7 01. .6 01. .6 02. .5 02. .4 03. .3 03. .3 03. .1 04. .1 04.	.5 5. .9 5 .6 5 .6 5 .0 5 .7 6 .1 6	50,1 51.0 51.9 52.9 53.8 54.7 55.6	20.2 20.6 21,0 21.4 21.7 22.1	04 05 106 07 08	96.4 97.4 98.3 99.2	39.0 39.3 39.7	54 55	142.8	57.7 58.1	04	189.1	76.4 76.8	54	235-5	95.2
5 04.6 6 05.6 7 06.3 8 07.4 9 08.1 10 09.1 11 10.1 12 11.1 13 12.1 14 13.1 15 13.1 15 13.1 16.1 19 17.1 20 18.2 21 19.2 22 20.2 23 21.2 24 22.2 25 26 24.2 27 25.2 28 26.3 30 37 34 38 35 36 33 37 34 38 35 35 36 33 37 34 38 35 35 36 37 38 35 36 35 36 37 38 36 37 38 37 38 38 38 38 38 38 38 38 38 38 38 38 38	.6 01. .6 02. .5 02. .4 03. .3 03. .3 03. .1 04. .1 04.	.9 5 .2 5 .6 5 .0 5 .0 5 .7 6 .1 6	51.0 51.9 52.9 53.8 54.7 55.6	20.6 21,0 21.4 21.7 22.1	05 106 07 08	97·4 98·3 99·2	39·3 39·7	55	143.7	58.1	05	190.1	768			
6 05.6 7 06.8 9 08.10 11 10.11 12 11.11 13 12.11 14 13.15 15 13.11 17 15.18 16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 17.15 18.16.19 19.17 20.18 21.19 22.20 23.21 24.22 25.28 26.30 27.31 28.33 31.35 33.31 35.33 36.33 37.34 38.35 37.34 38.35 37.38 38.35 37.38 38.35	.6 02. .5 02. .4 03. .3 03. .3 03. .2 04. .1 04. 1 04.	.2 51 .6 55 .0 55 .7 66 .7 66	51.9 52.9 53.8 54.7 55.6	21,0 21.4 21.7 22.1	106 07 08	98.3	39.7			-	_		-	55	236,4	95.5
6 05.0 7 06.1 8 07.2 9 08.1 10 09.1 11 10.1 12 11.1 13 12.1 14 13.1 15 13.1 16 14.1 17 15.1 18 16.1 19 17.2 20 18.2 21 19.2 22 23.2 24 22.2 28 26.2 29 26.3 30 27.3 31 28.3 32 36 33.3 33 34 31.3 35 32.3 36 37 34.3 38 35.3	.5 02. .4 03. .3 03. .2 04. .1 04. .1 04.	.6 5 .0 5 .4 5 .7 6 .1 6	52.9 53.8 54.7 55.6 56.6	21.4 21.7 22.1	07	99.2		156	TAA.6	-0 -	1					_
8 07.4 9 08.1 10 09.1 11 10.1 12 11.1 13 12.1 14 13.1 15 13.1 16 14.1 17 15.1 18 16.1 19 17.1 20 18.2 21 19.2 22 20.2 23 21.2 24 22.2 25 23.2 26 24.2 27 25.2 28 26.3 29 26.3 30 27.3 31 28.3 32 29.3 33 30.3 34 31.3 35 32.3 36 33.3 37 34.3 38 35.3 38 35.3 37 34.3 38 35.3	.4 03. .3 03. .2 04. .1 04. .1 04.	.0 5 4 5 .7 6 .1 6	53.8 54.7 55.6 56.6	21.7	08		40.1		-44.0	50.4	206	191.0		256	237.4	95 9
9 08. 10 09. 11 10.: 12 11. 13 12. 14 13. 15 13. 16 14. 17 15. 18 16. 19 17. 20 18. 21 19. 22 20. 23 21. 24 22. 25 23. 26 24. 27 25. 28 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	3 03 3 03. 2 04. 1 04. 1 04.	4 5 .7 6 .1 6	54.7 55.6 56.6	22. I				57	145.6	58.8	07	191.9	77.5	57	238.3	96.
10 09. 11 10. 12 11. 13 12. 14 13. 15 13. 16 14. 17 15. 18 16. 19 17. 20 18. 21 19. 22 20. 23 21. 24 22. 25 23. 26 24. 27 25. 28 26. 24 22. 28 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	.3 03. .2 04. .1 04. .1 04.	.1 6	55.6			the second second	40.5	58	146 5		08	192.9	77.9	58	239.2	96.
11 10.: 12 11. 13 12. 14 13.: 15 13.: 16 14.: 17 15: 18 16. 19 17. 20 18. 21 19. 22 20. 23 21. 24 22. 25 23. 26 24. 27 25. 28 26. 29 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	.1 04	.1 6	56.6	22 1	09	101.1		59	147 4		09	193.8		59	240.1	97.0
12   11. 13   12. 14   13. 15   13. 16   14. 17   15. 18   16. 19   17. 20   18. 21   19. 22   20. 23   21. 24   22. 25   23. 26   24. 27   25. 28   26. 29   26. 30   27. 31   28. 32   29. 33   32. 34   31. 35   32. 36   33. 37   34. 38   35. 38   35. 39   35. 30   35. 31   36. 32   36. 33   36. 34   35. 35   36. 36   37. 37   38. 38   35. 38   35. 38   35. 38   35. 39   35. 30   35. 31   35. 32   35. 33   35. 34   35. 35   35. 36   35. 37   36. 38   35. 38   3	.1 04	.5 6			10	102.0		60	148.4	_	10	194.7		60	241.1	97.
13 12.1 14 13.1 15 13.1 16 14.1 17 15.1 18 16.1 19 17.2 20 18.2 21 19.2 22 23.2 24 22.2 25 23.2 26 24.2 27 25.2 28 26.2 29 26.3 30 27.3 31 28.3 32 32.3 33 33.3 34 35.3 35 36 33.3 37 34.3 38 35.3	.0 05	-5 6		22.9	III	102.9	41.6	161	149.3	60.3	2 J I	195.6	790	261	242.0	97.
14 13.1 15 13.1 16 14.1 17 15.1 18 16.1 19 17.2 20 18.2 21 19.2 22 20.2 23 21.2 24 22.2 25 23.2 26 24.2 27 25.2 28 26.2 29 26.3 30 27.3 31 28.3 32 39.3 33 30.3 34 31.3 35 36 33.3 37 34.3 38 35.3	.005	0 6	57.5	23.2		103.8				60.7	12	196,6		62	242,9	98,
15 13.1 16 14.1 17 15.1 18 16.1 19 17.2 20 18.2 21 19.2 22 20.2 23 21.2 24 22.2 25 23.2 26 24.2 27 25.2 28 26.3 30 27.3 31 28.3 32 32.3 33 33.3 34 31.3 35 32.3 36 33.3 37 34.3 38 35.3			58.4			104.8		63		61.1		197.5		63	243.9	98.
16 14.: 17 15.: 18 16.: 19 17.: 20 18.: 21 19.: 22 20.: 23 21.: 24 22.: 25 23.: 26 24.: 27 25.: 28 26.: 29 26.: 31 28: 32 29.: 33 32.: 33 33.: 35 36 33.: 37 34.: 38 35.: 38 36.: 38 37 38.: 38 36.: 38 37 38.: 38 38 38 38.: 38 38 38 38.: 38 38 38 38.: 38 38 38 38 38.: 38 38 38 38 38 38 38 38 38 38 38 38 38 3	010		1 59,3		14	105.7	42.7		152.1	6. 9	14	198.4		64	244 8	98
17 15. 18 16. 19 17. 20 18. 21 19. 22 20. 23 21. 24 22. 25 23. 26 24. 27 25. 28 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 37 34. 38 35.	1.9 05		60.3		15	106.6		65	153.0		15	199 3	-	65	245.7	99
18 16. 19 17. 20 18. 21 19. 22 20. 23 21. 25 23. 26 24. 27 25. 28 26. 29 26. 30 27. 31 28. 32 39. 33 31. 35 32. 36 37 34. 38 35.	8 06		6 61.2	24.7	116	107.6		166	153.9	62,2	216	200.3	80.9	266	246.6	
19 17. 20 18. 21 19. 22 20. 23 21. 25 23. 26 24. 27 25. 28 26. 29 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	.8 06		62.1		17			67	154.8	62 0	17	201.2		67	247.6	
20 18. 21 19. 22 20. 23 21. 24 22. 25 23. 26 24. 27 25. 28 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	.7 06			25.5	18	109.4		68	155.8	62.9	18	202.1		68	248.5	
21 19. 22 20. 23 21. 24 22. 25 23. 26 24. 27 25. 28 26. 29 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	.607		9 64,0		19	110.3			156.7		1 1 1 1 1	203.1		69	249 4	
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23 21. 24 22. 25 23. 26 24. 27 25. 28 26. 29 26. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	1.5 07			26.6	121	112.2		171	158.6	64.1	22 I	294.9		271	251.3	
24 22. 25 23. 26 24. 27 25. 28 26. 29 26. 31 28. 32 29. 33 33. 34 31. 35 32. 36 33. 37 34. 38 35.	0.4 08	.2 7	2 66,8		22	113.1		72	159.5	64.4		205.8		72	252.2	
25 23. 26 24. 27 25. 28 26. 29 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	. 3 08			27.3		114.0			160.4	04.8	1	206,7		73	253,1	
26 24. 27 25. 28 26. 29 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	1.3 09			27.7	24	115.0		74	161,3		24	207.7	83.9	74	254.1	
27 25. 28 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	3.2 09		_	28.1	25	116.9		75	162.3	_	25			75	255.0	_
28 26. 29 26. 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	1.1 09			28.5	126	116 8		176	163.2		226	209.5	84.7	276	255.9	103.
29 26, 30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	5.0 10			28.8	27		47.6	77	164.1		27	210 5	85.0	77	256.8	
30 27. 31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	0.0			3 29.2	28		47.9	78	165.0		28	211.4	85 4	78	257,8	
31 28. 32 29. 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	5.9 10			2 29.6	29	119.0	48.3	79 80	166.0		30	212.3		79	259.6	
32 29 33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	7.9 11			30.0	30		48,7	-		-	-			-		-
33 30. 34 31. 35 32. 36 33. 37 34. 38 35.	3.7 11			30.3	131	121.5		181	167.8		231	214 2	86.5	82	260.5	105
34 31. 35 32. 36 33. 37 34. 38 35.	9.7 12	.0   8	2 76.0	30.7	32		49.4	82	168.8	68 6	32	215.1		83	261.5	
35 32. 36 33. 37 34. 38 35.	0.6 12	-4	3 77.9	31.1	33			83	169.7	68.0		217.0		84	262.4	
36 33 37 34 38 35	1.5 12		777.	31.5	34			85	171.5		34	217.9	88.0	85	264.3	
37 34- 38 35.	2.5 13			-	35			-		-	35			_		-
38 35.	3 4 13	3.3		7 32.2	136		50.9	186	172.5		236	218.8		286	265.2 266.1	107
	4.3 13			7 32.6	37		51.3	87			37	219.7		88	267.0	107
39 30.	5.2 14	4,2	0 81.	6 33.0			52.1	89	174.3	70.8		221.6		89	268.0	107
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42 38.	7.1 15	5.7   9	2 85.	3 34.5	42		53.2		178.0	72.2	42	224.4		92	270.7	
43 39.	7.1 15 8.0 15 8.9 15	5 11 4	487	2 34,8		132.0	53.9			72.7	44	226.2	01.4	93	271.7	
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	7.1 15 8.0 15 8.9 15 9.9 16 0.8 16 1.7 16 2.7 17 3.6 17 4,5 18	6.5 9 6.9 9 7.2 9 7.6 9	6 89. 7 89. 8 90.	9 36.3	47	136.	55.1	97	182.7	73.8	47	229.9	92.5	97	275.4	111
Dift De	7.1 15 8.0 15 8.9 15 9.9 16 0.8 16 1.7 16 2.7 17 3.6 17	7.2 9 7.6 9 8.0 9	6 89. 7 89. 8 90. 9 91.	9 36.3	47 48 49	136.	55.1	97 98 99	182.7	73.8	47 48 49	229.0	92.5 92.9 93.3	97	275.4	111

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1	00,9	00,8	51	46,9	20.3	02		39.5	52	139,0	50.4		185.9		52	231.0		ı
2	7 7 35	01,2	53		20.7	93		39,9	53	140.8	59.8		186,9		53	232.9	98.8	
3	03.7	1	54	700	21.1	04		40.6	54	141,8	60.2	04	187.8	79.7	54	233.8		
5	04.6	02 0	55	50.6	21.5	05		41.0	55	142.7	50.6	-	188.7	-	55	234.7	99.6	
6	05.5	02.3	56	51.5	21.9	106	97.6		156	143.6	60.9		189.6		256	235.6	100.0	
1 7	06.4	02.7	-57	52.5	-	07		41.8	57	144.5	61.3		190.5		57	236,6		1
8		03.1	58		22.7	08		42.2	1 -	145.4			191.5		58	237.5		1
9		03,5	59		23.1	10	100.3		59	146.4	10	10	2 2	82.0	60		101.2.	1
10		03.9	61		23,8	111	-		161	148.2	-	211		82,4	261		102.0	-
112		04.3	62	57.1	1 - 1	12	102.2		62	149.1			195.1	82.8	62	The contract	102.4	١
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11	13.8	05,9	65	-		15	105.9	-	65	151.9	_	15	197 9		65	243.9	103.5	
116		06.3	66	1	1 3 1	116	106.8	45.3	166	152.8	64.9	216		84.4	67	244.9		1
17		06.6	67	1	26.2	17	107.7	1	67	153.7	65,2	17	199.7	86.2	68	245.8		1
18		5 07.4	68		26.6	18	108.6	46.1	68	155.6	65.6	10	201.6	85.6	69		104.7	1
10		407.8	70		27.3	20		46.9	70	156.5	66.4	20	202.5		70		105.5	1
2		3 08,2	71		27 7	121	111.4	-	171	157.4	66 0	221	203.4		271		105.9	1
2	20,	3 08.6	72	100		22	1	47.7		158.	67.2	22	204.4	86.7	72		106.3	1
2		2 09.0	1.1	10	2 28.5	23	113.2	48.1	73	159.2	67.6	23	205.3	87.1	73	251.3	106.7	١
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1 4	0 36	.8 15.6	9	0 82.	8 35.2	40		9 54 7	90	174.	9 74.2	4	220.	93.8	90	200.0	113.3	1
14	1 37	7 16.0	9	1 83.	8 35.6	141		8 55.1	191	175.	8 74.6	24	221.	8 94,2	231	267.	113.7	1
	2 38	7 16.4	1 9	2 84.	7 35.9	42	130,	7 55.5		176.	7 75.0	1 4	232.	94,5	92		114,1	
		.6 16.8		3 85.	6 36.	43	131.	6 55.9	93	177.	7 75.4	1 4	3 223. 4 224.	6 95.3	93		6 114.9	
		.5 17.1		5 87	5 36.7	44	132.	6 56.3 5 56.7	94	170.	5 76.2	1 4	5 225	5 95.7	95		5 115	
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	6 42	3 18.4	9		4 37.5	47	125.	3 57.4	97	180.	3 77.0	4	7 227.		5 97	273.	4 116.0	5
14	8 44	2 18.8	9	8 90.	2 38.3	48	136.	2 57.8	98	182.	3 77.4	4	8 228.	3 96 9	9 98	274.	3 116	4
	9 45	1 19.1	9	9 91.	1 38.7	49	137.	2 58.2	1 99	183.	2 77,7	1 4	9 229.			275.	2 116.	8
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2		00,8	52	47.5	21.1	02		41.5	52	138.9	51.8		184.5	84.2	52		102.5
3		01,2	53	48 4	21.6	03		41.9	53	139.8	62.2		1854	82 6			102,9
4		01.6	54		22.0	04	1 7 7 1	42.3	54	140.7			186,4	8:0			103 3
5	04.0	02.0	55	-	22.4	05	_	42.7	55		63.0	0		83,4	55	-	103.7
6	05.5		56	1 -	22.8	106		43.1	156	142.5			188.2	83.8	256		104,1
7	06.4	100	57	1-	23.2	08		43 5	57		64.3		190.0	84.2			104.5
8	1-0	03.3	58		23.6			43.9			64.7	11 -	0.001	1 .	59		105,3
10		04,1	60					5 44-7	60		2 65.1		191.8	1 0 1	60		105.7
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11		04.9	62	100	6 25.2		1	3 45.6	110		0 65.9		2 193.7	1 0 - 1	62	1	106.6
13		9 05.3	63		6 25.6		103.	2 46.0	63	148.	9 66.3	1	3 194.6		63	240.3	107.0
14		8 05.7	64	13		11 .		1 46 4			8 66.7		4 195.5	1 - 1	64	1	107 4
15	13.	7 06.1	65	59.	4 26.4		105.	1 46.8			7 67.1	- 1 1	5 196.4	-	65	242 1	107.8
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17		5 06.9	67			11 6		9 47.			6 67.9		7 198.		67		0.801
12		4 07.3		63.	1 27.7	11		7 48,	11 .	153.	5 68.		9 200.		69		0.001
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2		8 10 2	7	5 68	.5 30.	5 2	5 114	2 50.	8 7	159	9 71.	2 2	5 205.	5 91,5	7.5	251.	2 111.8
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	7 33	.8 15	0 8	7 79	,5 35	4 3		5,1 55		7 170	8 76	.1	37 216			0	2 116 7
	18 34	.7 15.		8 80	4 35	8 3	8 12	5.1 56	1 8	8 171	7 76	.5	38 217	4 96.8		263	.1 117.1
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	8 43	.8 19.			5 39	9 4	8 13	5,2 60	2 9	8 180	0.0 80	,5	43 226	.5 100.	9 9	8 272	.2 121.2
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1	00,9		51	46,2	21.6	101	91.5	42.7	151	136.9		201	182.2	84.9	251	227.5	106.1
2	01.8		52		22.0	01	92,4		52	137,8			183.1	85.4	52	228.4	
3	02.7		53	100,000	22.4	03	93.3			138.7		04	184.0	85.8	53	229.3	MENT OF STREET
4	03.6	32.1	54		23.2	05	PACONA COMPANIE	44.0	54	139.6		05	185.8	86.6	54	230.2	
5	04.5	-			_	-	95.2	_	_	_		206	186,7		-		_
6	05.4	A	56	12.00	23.7	106	97.0	44 8	57	141,4		07	187.6	87.1	57	232.0	
7	07.3	93.0	58	10	24.5	08	97.9		58	143.2			188.5	87.9	58	232.9	Market Committee of the
9	08.2	03,8	59	1	24.9	09		46.1	59	144.1		09	189.4	88.3	59	234.7	10 to 10 to 10
10	5 5 5	04,2	60	54.4		10	99.7	46.5	60	145.0	67.6	10	190.3	88.7	60	235.€	
11	10.0	04.6	61	55.3	25.8	111	100.6	46.6	161	145.9	68.0	211	191.2	89,2	261	236,5	110.2
12	10.9	05.0	62	56.2		12	101.5		62	146.8		12	192.1	89.6	62	237.5	110,7
13	11.8	05.5	63			13	102.4		63	147.7		13	193.0	90.0	63	238.4	112,1
14	12.7		64		27.0	14	103.3	48.2	64	148.6		14	193.9	90,4	64	239.3	111.6
15	13.6		65	58.9	-	15	104.2	48,0	65	149.5	69 7	15	194.9	90.9	65	240.2	112.0
16	14.5		66	59.8		116	105.1		166	150.4		216	195.8	91.3	266	241 1	112.4
17		07.2	68		28.3	17	106,0		67	151.4			196.7	91,7	68	242,0	1
18		07.6	69		28.7	19	105.9		69	152.3	100		198.5	92.1	69	242.9	113.3
19		08.5	70		29.6		108.8		70	154.1			199.4	93.0	70	244.7	114.1
-	200	08.9	71	64.3			-	-	171	-			200.3	93.4	271	2446	
21		09.3	72		30.4		110.6		72	155.0		W	201.2	93.8	72	246.5	114,5
23		09.7	73		30.8		111.5	1	73	156.8		1	202.1	94,2	73	247.4	115.4
24		10.1	74	67.1	1 200	41	112,4	A 18 mm	74	157.7		24	203.0	94-7	74	248.3	115.8
25	22.7	10.6	75	_	31.7	25	113.3	52.8	7.5	158.6	74.0	25	203.9	95.1	75	249.2	116.2
26	23.6	11.0	76				114.2	53.2	176	159.5	74.4	226	204.8	95.5	276	250.1	1166
27		11.4	77		32.5		115.1	53.7	77	160.4	74.8		205.7	95.9	77	251.0	
28		E1.8	78	70.7			116.0		78	161.3		1	200 6	90.4	78	252.0	1000
29		12.3	80		33.4		116.9		19	162.2			207.5	96.8	79	252.9	
30	-	12.7	81	7.0	33.8				181			_		-	281		-
31	28.7		82	1/3	44 5 25 3 1	1000	119.6		82	164.0	100	3	209.4	97.6	82	254.7	W. 1 W. 1
32	1	13.5	83		34.7	41 5 .	120.5		83	165.9		33	100000	98.5	33	256.5	Dec 10 10
34		14.4	84		35.5	41	121 4	Ent I	84	166.8	1	34	Audio	98.9	84	257.4	120.0
35		14,8	85		100 600		122.4	57.1	85	167.7		35	213.0	99.3	85	258.3	120.4
36	32.6	15 2	86	77:9		136	123.3	57.5	186	168.6	78.6	236	213.9	99.7	286	259.2	120.9
37	10	15.6	87		36.8	37	124.2	100 100 100	87	169,5	79.0	37	2148	100.2	87	260,1	121.3
38	34.4	16.1	88	100	37.2	38	125,1	58.3	88	170.4	79 4		215.7			261.0	
39	35.3	16.5			37.6		126.0	58.7	89	171.3				101.0		261.0	
40	_	16.9	30		38.0			59,2	90	172.2	_			101.4	_	262.8	-
41		17.3	91	82.5	38,5	141	127.8		191	173,1	80,7			101.8		263.7	123.0
42	38,1	17.7	92	83.4	38.9	42	128.7		93	174.0	81,1			102.3		264.6	
43	20.0	1816	93	85.	39.7	44	130,5	60.0	94	175.8	82.0	44		103.1	94	266.5	124.2
45	40.8	19.0	95		40.1		131.4	61.3	95	176.7	82.4	45		103,5	95	267.4	
46	-	19.4			40.6	7	132.3				82.8			104.0	196	-	125.1
47		19.9	97	87 0	41.0	47	177.2	62.1	97	178.9	83.2	47	223.9	104.4	97	260.2	125,5
48	43.5	20,3	98	88.8	41.4	48	134.1	62.5	98	179.4	83.7	48	224.8	104 8	98	270.1	
49	44.4	20,7	99	89 7	41.8	49	135,0	63.0	99	180.4	84.1	49	225 7	105.2	99	271.0	126.4
		21.1	100	90.6	42.3	1:0	135.9	63.4	200	181 3	84.5			105 7			
		Lai	-	1 10 100			Dep	-									The same of the sa

for 65 Deg.

Diff Lat   Dep   Diff
2 01.8 00.9 5 5 46,7 22.8 02 91.744.7 52 136.6 66.6 02 181.6 88.6 52 236.5 110.0 03 182.8 89.4 54 03.6 01.8 54 48.5 23.7 04 93.5 45.6 54 138.4 67.5 04 183.4 89.4 54 23.7 111.5 04.5 04.5 02.2 55.4 99.4 14.1 05 94.4 46.6 55 139.3 68.0 05 184.3 89.9 55 239.2 111.3 05.7 06.3 93.1 57 51.2 25.0 07 95.2 46.5 15 140.2 68.4 12.1 168.2 07.3 15 15.2 54.0 8 97.1 47.3 58 142.0 69.3 10.1 185.2 90.3 256 23.0 112.2 112.3 10.0 09.0 04.4 60 53.9 26.3 10.9 98.0 47.8 59 142.0 69.3 10.8 18.5 29.2 112.3 10.0 09.0 04.4 60 53.9 26.3 10.9 98.0 47.8 59 142.9 69.7 12.1 12.0 09.0 04.4 60 53.9 26.3 10.9 98.0 47.8 59 142.9 69.7 12.1 12.0 09.0 04.4 60 53.9 26.3 10.0 98.0 48.3 10.9 98.0 48.3 10.1 10.0 09.0 04.4 60 53.9 26.3 10.0 10.0 09.0 04.4 60 53.9 26.3 10.0 09.0 04.4 60 53.9 26.3 10.0 09.0 04.4 60 53.0 09.0 09.0 04.4 60 53.0 09.0 09.0 04.4 60 53.0 09.0 09.0 04.4 60 53.0 09.0 09.0 09.0 09.0 09.0 09.0 09.0 0
3 0.2.7 0.1.3   53 47.6   23.2   03   23.6   45.2   53   137.5   67.1   03   183.5   89.0   53   227.4   120.5   5 0.4.5   0.2   2   55   49.4   49.1   05   94.4   40.6   55   139.3   63.0   05   184.3   89.9   55   23.2   111.2   6 0.5.4   0.2   6   56   50   24.6   106   95.3   46.5   156   140.2   68.4   106   185.2   90.3   256   230.1   112.2   8 0.7.2   0.3.5   58   52.1   25.4   08   97.1   47.3   58   140.6   95.3   68.4   206   185.2   90.3   256   230.1   112.2   9 0.8.1   0.3.9   0.5   53.9   16.3   10   98   94.5   10   98.0   187.8   91.6   10   91.7   10   99.0
4 03.6 01.8 5 54 48.5   23.7 04 93.5   45.6   54   138.4   67.5   04.183.4   89.4   54   288.3   111.5   50.4   50.5   29.4   46.6   55   29.4   46.6   56   27.5   29.4   46.6   56   27.5   29.4   46.6   26.8   20.5   29.5   29.2   211.2   20.6   20.7   20.6   20.7   20.6   20.7
5 04-5 02 2 55 49-4   4-1   05 94-4   46-6   55   139-3   68-0   05   184-3   89-9   55   239-2   111-3   60   64-5   05-4   02-6   03-3   15   56   03-4   05   185-2   09-3   25   230-1   112-3   03-1   0
6 05.4 02.6 56 50 3 24.6 106 95.3 46 5 150 140.2 68.4 106 185.2 90.3 256 230.1 112.2 106.3 39.1 57 51.2 25.0 07 96.2 46.5 57 141.1 68.6 07 186.1 90.7 57 31.6 112.7 90.8 07.2 07.5 58 53.1 25.4 08 97.1 47.3 58 142.0 69.3 00 187.6 91.2 58 131.9 113.1 0.9 0.0 44.8 60 53.9 46.3 10 98.9 48.2 60 143.8 70.1 10 188.7 92.1 60 233.7 114.6 11 0.9 9.0 48 61 54.3 26.7 111 99.8 48.7 161 144.7 70.6 111 189.6 92.5 62 55.7 27.2 12 100.7 49.1 62 145.6 71.0 12 190.5 92.9 62 235.5 114.1 11.7 05.7 63 56.6 27.6 13 10.1 49.5 63 146.5 71.5 13.1 0.0 6.6 55.9 48.2 51.5 103.4 50.4 65 143.8 70.1 14 192.3 93.8 64 237.3 115.1 11.7 05.7 67 60.2 19.4 17 105.2 51.3 67 150.1 73.2 17 195.0 95.1 67 60.2 19.4 17 105.2 51.3 68 151.0 73.7 18 195.9 95.6 67 60.2 19.4 17 105.2 51.3 68 151.0 73.7 18 195.9 95.6 67 60.2 19.4 17 105.2 51.3 68 151.0 73.7 11 19 19 10 10 3.3 69 62.0 30.2 19 107.0 52.2 51.3 68 151.0 73.7 11 19 196.8 96.0 70.0 12.2 12.2 12.2 12.2 12.2 12.2 12.2 1
7 06.3   3-1   57   51.2   5.0   07   96.2   46.5   57   141.1   68.8   07   186.1   90.7   57   231.c   112.7   90.8   10.9   90.8   10.9   95   53   52.5   90   99   98.4   47.8   58   142.0   69.3   90   187.c   91.2   131.1   10.9   90.4   60   53.9   16.3   10   98.9   48.2   60   143.8   70.1   10   188.7   92.1   60   233.7   114.1   11.1   10.8   05.3   62   55.7   27.2   11   100.7   49.1   61   144.7   70.6   11   189.c   92.5   26   233.5   114.1   11.1   11.7   05.7   63   56.6   27.6   13   100.7   49.1   61   144.7   70.6   11   190.5   92.9   62   235.5   114.9   11.1   11.1   11.1   11.1   10.5   50.0   64   147.4   71.9   14   192.3   93.8   64   237.3   115.1   11.1   11.1   11.1   10.5   50.0   64   147.4   71.9   14   192.3   93.8   64   237.3   115.1   11.1   11.1   10.5   13.3   10.1   13.3   10.1   13.3   10.1   13.3   10.1   13.3   10.1   13.3   10.1   13.3   13
8 07.2 03.5 58 52.1 25.4 08 97.1 47.3 58 142.0 60,3 00 187.6 91.2 58 231.9 113.1 0.9 9 0.4 4 60 53.9 16.3 10 98 94.8 26.7 111 99.8 48,7 161 144.7 70.6 23.2 110.8 05.3 62 55.7 27.2 12 100.7 49.1 60 144.7 70.6 214.6 60.1 64 57.5 28.1 14 102.5 50.0 64 147.4 71.9 14 192.3 93.8 64 23.7 115.1 15 13.5 06.6 65 58.4 28.5 15 103.4 50.4 65 148.3 72.3 15 193.2 94.3 65 238.2 116.2 115.3 06.6 65 58.4 28.5 15 103.4 50.4 65 148.3 72.3 15 193.2 94.3 65 23.2 116.2 117.1 15 3 07.5 66 59 3 28.9 116 104.3 50.9 166 149.2 72.8 118 16.2 07.9 68 61.1 12.8 18 106.1 54.7 68 151.0 73.7 18 195.9 95.6 68 24.0 17.1 17 108.3 69 62.0 30.2 19 107.0 52.2 69 151.9 74.1 19 196.8 95.0 69 241.8 117.9 20.1 18.9 09.2 71 63.8 31.1 121 108.8 53.2 20.7 10.1 73 55.6 32.0 20 107.9 52.6 70 152.8 74.5 22 199.5 97.3 72 244.5 119.2 22 19.8 09.6 72 64.7 31.6 22 109.7 53.5 72 154.6 75.4 22 199.5 97.8 73 244.5 119.2 24.3 11.8 76 68.3 33.3 126 113.2 55.2 72 152.5 77.5 22 20.2 2.9 8.6 75 24.0 117.2 12.2 24.3 11.8 76 68.3 33.3 126 113.2 55.2 72 152.5 77.5 22 20.2 2.9 8.6 75 24.2 118.6 22.2 118.6 25.2 11.0 75 67.4 32.9 25 113.4 54.8 77 155.7 77 159.1 77.0 24.0 107.0 24.2 118.6 25.2 12.3 22.5 111.0 75 67.4 32.9 25 113.4 54.8 77 155.7 77 159.1 77.0 24.0 107.0 24.2 118.6 25.2 12.3 27.0 13.2 80 71.9 35.1 30 116.1 57.0 80 161.8 78.9 30.0 71.9 35.1 30 116.1 57.0 80 161.8 78.9 30.0 71.9 35.1 30 116.1 57.0 80 161.8 78.9 30.0 71.9 35.1 30 116.1 57.0 80 161.8 78.9 30.0 67.9 35.5 13.1 117.9 56.4 33 11.9 55.8 31 119.5 58.3 31 119
9 08.10 3,9 59 53 c 25.9 09 98.0 47.8 59 143.9 69 7 09 187.8 91,6 59 232.8 133.1 09 90 04,4 8 61 54.8 26.7 111 99.8 48,7 161 144.7 70.6 112 10.8 05.3 62 55.7 27.2 12 100.7 49.1 62 145.6 71.0 12 190.5 92 9 62 233.7 114.0 11.1 11.7 05.7 63 56.6 27.6 13 101.0 49.5 63 146 5 71.5 13.1 190.5 92 9 63 23.8 113.1 11.7 05.7 63 56.6 27.6 13 101.0 49.5 63 146 5 71.5 13.1 190.5 92.9 463 23.6 113.1 15.1 13.5 06.6 65 58.4 28.5 15 103.4 50.4 65 148.3 72.3 15 193.2 94.3 65 238.2 116.1 16 14 4 07.0 66 59 3 28.9 116 104.3 50.9 166 149.2 73.8 216 194.1 94.7 166 239.1 110.1 19.8 18 106.2 07.9 68 61.1 29.8 18 105.1 51.3 67 150.1 73.2 17 195.0 95.1 67 240.0 117.1 18.9 09.2 70 62.9 30.7 20 107.9 52.6 70 152.8 74.5 22 199.5 96.6 96.0 92.1 19.1 107.0 52.2 19.4 17 105.2 51.3 69 151.9 74.1 19.1 19.6 96.0 69 241.8 117.2 118.9 09.2 71 63.8 31.1 121 108.8 53.0 17.1 153.7 75.0 121.1 19.8 09.6 72 64.7 31.6 22 109.7 52.6 70 152.8 74.5 22 199.5 97.3 72 244.5 119.2 22 12.3 20.7 10.1 73.5 5.6 32.4 24 111.5 54.4 74 156.4 70.3 24.0 13.1 1.8 7.7 69.2 33.4 27 14.1 15.5 4.8 74 74 156.4 70.3 24.0 13.2 28 25.2 11.0 75 67.4 32.9 25 112.4 54.8 75 157.3 76.7 25.2 20.2 29.6 77.9 13.2 28.7 11.8 27.9 13.6 27 19.5 56.1 33.1 11.7 55.4 77 155.1 77.5 22.1 19.8 00.0 75 67.4 32.9 25 112.4 54.8 75 157.3 76.7 25.2 20.2 29.6 75.3 24.1 14.1 55.7 77 155.1 77.1 19.1 17.0 17.6 17.6 17.6 17.6 17.5 17.6 17.6 17.5 17.6 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17.5
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11 09 9 04 8 61 54.8 26.7 111 99.8 48,7 161 144.7 70.6 211 189.6 92.5 261 234.6 114,1 12.0 8 05.3 62 55.7 27.2 17 100.7 49.1 62 145.6 71.0 12 190.5 92 9 62 235.5 114.6 14 12.6 06.1 64 57.5 28.1 14 10.5 50.0 64 147.4 71.9 14 192.3 93.8 64 237.3 115.5 13.5 06.6 65 58.4 28.5 15 103.4 50.4 65 148.3 72.3 15 193.2 94.3 65 238.2 116.2 07.9 68 61.1 29.8 18 106.1 51.7, 68 151.0 73.7 17 195.0 95.1 67 240.0 117.1 19.17 108.3 69 62.0 30.2 19 107.0 52.2 5.3 67 150.1 73.2 17 195.0 95.1 67 240.0 117.1 19.17 108.3 69 62.0 30.2 19 107.0 52.2 6 151.9 74.1 19 196.8 96.0 69 241.8 117.9 22.1 18.9 09.2 77 65.2 32.0 107.9 52.6 70 152.8 74.5 20 197.7 96.4 70 242.7 118.4 12.2 198.0 96.9 171 243.6 118.3 22.2 19.8 09.6 72 64.7 31.6 22 109.7 53.5 72 154.6 75.4 22 199.5 97.3 72 244.5 119.2 24.3 11.8 22.2 110.6 53.5 72 67 152.8 74.5 22 199.5 97.3 72 244.5 119.2 24.3 11.8 22.2 11.0 10.5 74 66.5 32.4 24 111.5 54.4 74 155.7 75.8 23 200.4 97.8 73 244.5 119.2 24.3 11.8 22.2 11.3 79 71.0 34.6 29 115.9 56.6 79 152.8 77.5 25 202.2 98.6 75 247.2 120.1 27 243.3 11.8 28 25.2 12.3 20.1 32.2 80 71.9 35.1 30 116.1 57.0 80 116.8 78.9 30 20.6 7 100.8 83 74.9 112.3 28 115.5 56.6 18.8 78.9 30 20.6 7 100.8 83 74.9 112.3 28 115.9 56.6 18.8 78.9 30 20.6 7 100.8 83 25.1 12.3 29.7 14.5 83 74.5 36.8 31 117.7 57.4 38 31.5 12.3 39.7 14.5 83 74.5 36.8 34 120.4 55.9 83 164.5 50.9 83 164.5 50.9 83 164.5 50.9 83 164.5 50.9 83 164.5 50.9 83 124.9 50.9 83 164.5 50.9 8
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13 11.7 05.7 63 56.6 27.6 13 101.6 49.5 63 146 57.1 5 13 191.4 93.4 63 236,4 115.1 12.6 06.1 64 57.5 28.1 14 102.5 50.0 64 147.4 71.9 14 192.3 93.8 64 237.3 115.1 13.5 06.6 65 58.4 28.5 15 103.4 50.4 65 148.3 72.3 15 193.2 94.3 65 238.2 116.2 11.5 3 07.5 67 60.2 19.4 17 105.2 51.3 67 150.1 73.2 11.6 10.4 3 50.9 166 194.1 94.7 166 239.1 116.2 07.9 68 61.1 19.8 18 106.1 51.7 68 151.0 73.7 18 195.9 95.6 68 240.9 117.1 08.9 69 62.0 30.2 19 107.0 52.2 69 151.9 74.1 19196.8 96.0 69 241.8 117.2 20 18 0.08.7 70 62.9 30.7 20 107.9 52.6 70 152.8 74.5 21 198.6 96.0 69 241.8 117.3 21 18.9 09.2 71 63.8 31.1 121 108.8 53.0 171 153.7 75.0 22 1198.6 96.0 69 241.8 117.3 22 19.8 09.6 72 64.7 31.6 22 109.7 53.5 72 154.6 75.4 22 199.5 97.3 72 244.5 119.2 22 19.8 09.6 72 64.7 31.6 22 109.7 53.5 72 154.6 75.4 22 199.5 97.3 72 244.5 119.2 22 22.5 11.0 75 67.4 32.9 25 112.4 54.8 75 157.3 76.7 25 20.2 2.9 8.6 75 247.2 120.6 23.4 11.4 76 68.3 33.3 126 113.2 55.2 17.6 158.2 77.6 27 20.2 98.6 75 247.2 120.6 23.4 11.4 76 68.3 33.3 126 113.2 55.2 17.6 158.2 77.6 27 20.2 98.6 75 247.2 120.6 23.4 11.4 76 68.3 33.3 126 113.2 55.2 17.6 158.2 77.6 27 20.0 99.5 77 249.0 111.2 24.3 11.8 77 69.2 33.8 27 114.1 55.7 77 159.1 77.6 27 20.2 98.6 75 247.2 120.0 32.5 12.3 78 70.1 34.2 28 115.0 56.1 78 160.0 78.0 29.5 80.0 4 97.8 22.5 12.3 78 70.1 34.2 28 115.0 56.1 78 160.0 78.0 29.5 80.0 4 97.8 22.5 12.3 78 70.1 34.2 28 115.0 56.1 78 160.0 78.0 29.5 80.0 4 97.8 22.5 12.3 30.2 27 13.5 85.5 36.8 34 120.4 58.7 98.8 164.5 80.7 33.2 27.0 13.2 80 71.9 35.1 30.1 16.1 57.0 80 160.9 78.5 30.2 25.8 10.0 78.2 20.0 99.5 77 249.0 121.2 32.0 32.0 32.0 32.0 32.0 32.0 32.0 32
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19 17 1 08,3 69 62.0 30.2 19 107.0 52.2 69 151.9 74.1 19 196.8 96.0 69 241.8 117.5 118.9 08.7 70 62.9 30.7 20 107.9 52.6 70 152.8 74.5 20 197.7 96.4 70 242.7 118.4 117.5 118.9 09.2 71 63.8 31.1 121 108.8 53.0 17.1 153.7 75.0 121 198.6 96.9 271 243.6 118.9 118.9 118.9 09.6 72 64.7 31.6 22 109.7 53.5 72 154.6 75.4 22 199.5 97.3 72 244.5 119.2 119.8 119.2 119.8 119.2 119.8 119.2 119.8 119.2 119.2 119.8 119.2
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22       19.8 09.6       72       64.7 31.6       22       109.7 53.5       72       154.6 75.4       22       199.5       97.3       72       244.5 119.5         23       20,7 10.1       73       55.6 32.0       23       110.6 53.5       73       155.5 75.8       23       200.4 97.8       73       245.4 119.5         24       21.6 10.5       74       66.5 32.4       24       111.5 54.4       74       156.4 76.3       24 201.3       98.2       74       246.3 120.1         25       22.5 11.0       75       67.4 32.9       25       112.4 54.8       75       157.3 76.7       25       202.2 98.6       75       247.2 120.1         26       23.4 11.4       76       68.3 33.3       126       113.2 55.2       176       158.2 77.2       226 203.1 99.1       276 248.1 121.6         27       24,3 11.8       77       69.2 33.8       27       114.1 55.7       77       159.1 77.6       27 204.0 99.5       77 249.0 121.4         28       25.2 12.3       78       70.1 34.2       28       115.9 56.6       79       160.9 78.5       29 205.8 100.0       78 249 9121.4         29       26.1 12.7       79       71.0 34.6       29       115.9 56
23 20,7 10.1 73 55.6 32.0 23 110.6 53.5 73.8 23 200.4 97.8 73 245.4 119.7 24 21.6 10.5 74 66.5 32.4 24 111.5 54.4 74 156.4 76.3 24 201.3 98.2 74 246.3 120.1 25 22.5 11.0 75 67.4 32.9 25 112,4 54.8 75 157.3 76.7 25 202.2 98.6 75 247.2 120.1 27 24,3 11.8 77 69.2 33.8 27 114.1 55.7 77 159.1 77.6 27 204.0 99.5 77 249.0 121.2 28 25.2 12.3 78 70.1 34.2 28 115.0 56.1 78 160.0 78.0 28 204.9 100.0 78 249.9 121.1 29 26.1 12.7 79 71.0 34.6 29 115.9 56.6 79 160.9 78.5 29 205.8 100.4 79 250 8 122.3 28.8 14.0 82 73.7 15.9 35.1 30 116.8 57.0 80 161.8 78.9 30 206.7 100.8 8.2 251.7 122.3 12.8 14.0 82 73.7 15.9 32 118.6 57.9 82 163.6 79.8 32 208.5 101.7 82 253.5 123.3 32 28.8 14.0 82 73.7 15.9 32 118.6 57.9 82 163.6 79.8 32 208.5 101.7 82 253.5 123.3 32 29.7 14,5 83 74.6 36.4 33 119.5 58.3 83 164.5 80.2 33 20.6 7 100.8 8.2 253.5 123.3 33 29.7 14,5 83 74.6 36.4 33 119.5 58.3 83 164.5 80.2 33 20.6 7 100.8 82 253.5 123.3 33 29.7 14,5 83 74.6 36.4 33 119.5 58.3 83 164.5 80.2 33 20.6 7 100.8 84 255.3 124.3 35 31.5 15.3 85 76.4 37.3 35 121.3 59.2 85 166.3 81,1 35 211.2 103.0 85 256.2 124.3 125.3 36.3 15.1 5.3 85 76.4 37.3 35 121.3 59.2 85 166.3 81,1 35 211.2 103.0 85 256.2 124.3 125.3 36.0 17.5 90 80.9 39.5 40 125.8 66.9 89 169.9 82.9 39 214.8 104.8 89 259.8 126.9 30.5 17.5 90 80.9 39.5 40 125.8 66.4 90 170.8 83.3 40 215.7 105.2 90 260.7 127.
24       21.6       10.5       74       66.5       32.4       24       111.5       54.4       74       156.4       76.3       24       201.3       98.2       74       246.3       120.1         26       23.4       11.4       76       68.3       33.3       126       113.2       55.2       176       158.2       77.2       226       203.1       99.1       276       248.1       121.0         27       24,3       11.8       77       69.2       33.8       27       114.1       55.7       77       159.1       77.6       27       204.0       99.5       77       249.0       121.4         28       25.2       12.3       78       70.1       34.2       28       115.0       56.6       79       160.0       78.0       28       204.9       100.0       78       249.0       121.4         29       26.1       12.7       79       71.0       34.6       29       115.0       56.6       79       160.0       78.5       204.9       100.0       78       249.0       121.4         30       27.0       13.6       31.7       35.1       31.17.7       57.4       181       162.7 </td
25       22.5       11.0       75       67.4       32.9       25       112,4       54.8       75       157.3       76.7       25       202.2       98.6       75       247.2       120.1         26       23.4       11.4       76       68.3       33.3       126       113.2       255.2       176       158.2       77.2       226       203.1       99.1       276       248.1       121.0         27       24,3       11.8       77       69.2       33.8       27       114.1       55.7       77       159.1       77,6       27.0       204.0       99.5       77       249.0       121.0         28       25.2       12.3       78       70.1       34.6       29       115.9       56.6       79       160.9       78.5       29.205.8       100.4       79.250.8       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       121.0       249.9       1
26       23.4       11.4       76       68.3       33.3       126       113.2       55.2       176       158.2       77.2       226       203.1       99.1       276       248.1       121.6         27       24,3       11.8       77       69.2       33.8       70.1       34.2       28       115.0       56.1       78       160.0       78.0       28       204.0       99.5       77       249.0       121.2         29       26.1       12.7       79       71.0       34.6       29       115.9       56.6       79       160.9       78.5       29       205.8       100.0       79       250.8       122.3         30       27.0       13.6       81       72.8       35.5       131       117.7       57.4       181       162.7       79.4       231       207.6       101.3       281       252.6       122.3         31       27.9       13.6       81       72.8       35.5       131       117.7       57.4       181       162.7       79.4       231       207.6       101.3       281       252.6       123.3         32       28.8       14.0       82       73.7       15.9
27       24,3       11.8       77       69.2       33.8       27       114.1       55.7       77       159.1       77,6       27       204.0       99.5       77       249.0       121.4         28       25.2       12.3       78       70.1       34.2       28       115.0       56.1       78       160.0       78.0       28       204.0       99.5       77       249.0       121.4         29       26.1       12.7       79       71.0       34.6       29       115.9       56.6       79       160.9       78.5       29       205.8       100.4       79       250.8       122.2         30       27.0       13.2       80       71.9       35.1       30       116.1       57.0       80       161.8       78.9       30       206.7       100.8       8.3       251.7       122.1         31       27.0       13.6       81.7       72.8       35.5       131       117.7       57.4       181       162.7       79.4       231       207.6       101.3       281       252.6       123.3         32       28.8       14.0       82       73.7       15.9       32       118.6
28 25.2 12.3 78 70.1 34.2 28 115.0 56.1 78 160.0 78.0 28 204.9 100.0 78 249 9 121.0 29 26.1 12.7 79 71.0 34.6 29 115.9 56.6 79 160.9 78.5 29 205.8 100.4 79 250 8 122.0 30 27.0 13.2 80 71.9 35.1 30 116.1 57.0 80 161.8 78.9 30 206 7 100.8 8.0 251.7 122.1 31 27 9 13.6 82 73.7 15 9 32 118.6 57.9 82 163.6 79.8 32 208.5 101.7 82 253.5 123.1 32.9.7 14,5 83 74.6 36.4 33 119.5 58.3 83 164.5 80.2 33 209.4 102.1 83 254.4 124, 34 30.6 14 9 84 75.5 36.8 34 120 4 58.7 84 165.4 80,7 34 210.3 102.6 84 255.3 124.3 35 31.5 15 3 85 76.4 37.3 35 121.3 59.0 85 166.3 81,1 35 211.2 103.0 85 256.2 124.1 36.3 37 33.3 16.2 87 78.2 38.1 37 123.1 60.1 87 168.1 82.0 37 213.0 103.9 87 258.0 125.3 38 34.2 16.7 88 79.1 38.6 38 124.0 50.5 88 169.0 82.4 38 213.0 103.9 87 258.0 125.3 39 35.1 17.1 89 80.0 39.0 39 124.9 60.9 89 169.9 82.9 39 214.8 104.8 89 259.8 126.4 40 36.0 17.5 90 80.9 39.5 40 125.8 61.4 90 170.8 83.3 40 215.7 105.2 90 260.7 127.5
29       26.1       12.7       79       71.0       34.6       29       115.9       56.6       79       160.9       78.5       29       205.8       100.4       79       250.8       122.8         30       27.0       13.2       80       71.9       35.1       30       116.1       57.0       80       161.8       78.9       30       206.7       100.8       83       251.7       122.8         31       27.0       13.6       81       72.8       35.5       131       117.7       57.4       181       162.7       79       4       231       207.6       101.3       281       252.6       123.8         32       28.8       14.0       82       73.7       15.9       32       118.6       57.9       82       163.6       79.8       32       208.5       101.7       82       253.5       123.9         33       29.7       14.5       83       74.6       36.4       33       119.5       58.3       83       164.5       80.2       33       209.4       102.1       83       254.4       124.9         34       30.6       14.9       84       75.5       36.8       34       <
30       27.0       13.2       80       71.9       35.1       30       116.1       57.0       80       161.8       78.9       30       206.7       100.8       \$3       251.7       122.8         31       27.9       13.6       81       72.8       35.5       131       117.7       57.4       181       162.7       79.4       231       207.6       101.3       281       252.6       123         32       28.8       14.0       82       73.7       15.9       32       118.6       57.9       82       163.6       79.8       32       208.5       101.7       82       253.5       123.6         33       29.7       14.5       83       74.6       36.4       33       119.5       58.3       83       164.5       80.2       33       209.4       102.1       83       254.4       124.9         34       30.6       14.9       84       75.5       36.8       34       120.4       58.7       84       165.4       80.7       34       210.3       102.6       84       255.3       124.9         35       31.5       15.3       85       76.4       37.3       37.7       136
31 27 9 13.6
32       28.8       14.0       82       73.7       35       9       32       118.6       57.9       82       163.6       79.8       32       208.5       101.7       82       253.5       123.1         33       29.7       14,5       83       74.6       36.4       33       119.5       58.3       83       164.5       80.2       33       209.4       102.1       83       254.4       124,4         34       30.6       14.9       84       75.5       36.8       34       120.4       58.7       84       165.4       80.7       34       210.3       102.6       84       255.3       124.4         35       31.5       15.3       85       76.4       37.3       35       121.359.2       85       166.3       81.1       35       211.2       103.0       85       256.2       124.4         36       32.4       15.8       86       77.3       37.7       136       122.2       59.6       186       167.2       81.5       236       212.1       103.0       85       256.2       124.4         37       33.3       16.2       87       78.2       38.1       37       123.1
33     29.7     14,5     83     74.6     36.4     33     119.5     58.3     83     164.5     80.2     33     209.4     102.1     83     254.4     124,5       34     30.6     14.9     84     75.5     36.8     34     120.4     58.7     84     165.4     80,7     34     210.3     102.6     84     255.3     124.       35     31.5     15.3     85     76.4     37.3     35     121.3     59.2     85     166.3     81.1     35     211.2     103.0     85     256.2     124.       36     32.4     15.8     86     77.3     37.7     136     122.2     59.6     186     167.2     81.5     236     212.1     103.0     85     256.2     124.       37     33.3     16.2     87     78.2     38.1     37     123.1     60.1     87     168.1     82.0     37     213.0     103.5     87     258.0     125.3       38     34.2     16.7     88     79.1     38.6     38     124.0     50.5     88     169.0     82.4     38     213.0     103.9     87     258.0     125.3       39     35.1     <
34       30.6       14.9       84       75.5       36.8       34       120.4       58.7       84       165.4       80,7       34.2       10.3       102.6       84       255.3       124.3         35       31.5       15.3       85.7       76.4       37.3       35.1       121.3       59.2       85.66.3       81.1       35.2       11.2       103.0       85.2       256.2       124.4         36       32.4       15.8       86       77.3       37.7       136.1       122.2       59.6       186.1       167.2       81.5       236.2       12.1       103.5       286.2       257.1       125.3         37       33.3       16.2       87.78.2       38.1       37.123.1       60.1       87.168.1       82.0       37.213.0       103.9       87.258.0       125.3         38       34.2       16.7       88.7       79.1       38.6       38.124.0       50.5       88.169.0       82.4       38.213.0       103.9       87.258.0       125.3         39       35.1       17.1       89.80.0       39.0       39.124.9       60.9       89.169.9       82.9       39.214.8       104.8       89.259.8       126.2
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4	S. 75 1.18	15.4	84		38,1	34		60.8	84	163.0	83.5	34		106 2		253 0	
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2		19.1		82.0	41.8	42	126,	5 64.5	92	171.	1 37.2	42		109,9		260.	
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16		12,2			35.7		111.3		176	155.4	82.6	226		106.1	276	243.7	129
27	23.8	12.7	77		36.2		112.1		77	156.	83.1	27	A 165 4	106.6		244.6	
28	1	13.1			36.6		113.0			157.2				107.0		245.5	
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10	26.5	14.1	80	70.0	37.6		114.8	-	80	-	. /		203.1			247.2	-
31	27.4		81	71.5		131	115.7	61.5	181		85.0			108.5	281		131
12	28.3	15.0	82	72.4	38.5	32	116.6							108.9	82	249.0	132
33	29.1		83		39.0		117.4		11 -	161.6				109.4	83	249.9	132
34		16.0	84	1.	39.4	11	118.3		84		06.4	34		109,9		250.8	
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37		17.4	1 87	76.8	40.8	37	121.0		87	165.1				111,3	87	253 4	134
38	33.6	17.8	88	77.7	41.3	30	121.9		88	166.0	00.3	30		111.7	0.	254.	135
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10		18.8			42.3		123.6		90	-	-			112.7		256.1	
+1	36.5	19.2	91	80.4	42.7	141	124.5	00.2	191	168.	89.7	241		113,1	29	257.9	136
12		19.7	92	81.2	43.2	42	125.4	00.7	92	169.	5 90,1	42		113.6	92	257.	137
13	38.0	20.2	93		43.7		126,	6-6	93	170.4				114.1		258.	
14	38.9	20.7	94	83.0	44.1		127.2	68				44		114.6		259.	133
15		21,1			44 6		128.0	08.1	95					115.0		260.	
16		21.6			45.1	146	128.0	68.5	196			246	217.2	115.5	29	261.	1 39
17	41.	22.1			45.5	47	129.8	69.0	97	174.0	92.5	47	218.1	115.9		262.	3 139
48		22.5		86.9	46.0		130.7	09,5	98	174.8	93.0			115.4		263.	1 36
49		23.0			46.5		131.6	170.0	99	175.7	93.4	49	219.9	116.9		264.	140
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2	01.7	0.10			26.0	02	88.3	51.0		131.6		02	174.9	0.101	52	218.2	126.0
3	02.6	31 5			26.5	03		51.5	53	132.5		03	2	101.5	53	219.1	126,5
4	03.5	72 0	7		27.C	04	120 12 12 12 13	520	54	133.4	77.0	04		102.0	54	17.18.19.20	127.0
_5	04 3	72.5	55		27.5	05	90.9	-	55	134.2	77.5	05	177.5	102.5	55	220,8	
6	05.2	03.0	56		28.0	106	91.8	53.0	_	135.1	78 0	206		1030	256	221.7	1280
7	06.1	03 5	-57		28.5	07		53.5	57	136 0		07		103.5	57	222.6	128.5
8	06 9				290	08	93.5		100	136.8	79.0	08		104.0		223.4	129 0
10	0	04 5	59	-	29.5	09	94 4		1 33	137,7	79·5 80.0	10		104.5	59	224.3	129,5
-		35.c	-	-	-	10	95.3		_	-	_	-	_	105,0	-	-	1300
111	09.5	05.5	61	52.8	100	111	96.1			139.4	80.5	211		105.5	62		130.5
12		06.0			31.0	12	97.0		62	140.3	81.0	12		106.0	63	226.9	
13	12.1	06,5	64	55 4	31.5	13	97 9 98.7	57,0	64	142.0	82.0	14	185,3	107.0	64	228.6	131.5
15	2 2 3	07.5	65	56.3	32.0	15	99 €	57.5	65	142,9	82.5	15		107.5	65	229 5	132 5
16	-	08.0	66	-	-	116	100.5		166	143.8	83.0	216	187.1	108.0	266	-	-
17		08.5	67	57.2	100	17	101.3	58,5	67	144.6	83.5	17		108.5	67	230 4	133 0
18		09.0			33.5	18	102.2		1 00	145.5	84.0	18	0 0	109.0	68		134.0
19		09.5	69	59,8	34.5	1	103 1	,,		146 4	84.5	19	189 7	109.5	69		134.5
20		10.0	70	50.6		20	1039		70	147 2	850	20	190.5	110.0	70	233,8	135 c
21	-0	10.5	71	61.5	_	121	104.8	-	171	148.1	85.5	221	191 4	110 5	271	234.7	135 5
22		11,0	72	62.4	36.0	22		610	72	149.0	86 0	22	192.3	1110	72		136.0
23		11.5	73	63 2	36.5	23	106.5		73	149.8	86.5	23	193.1	111 5	73		136.5
24	20.8	12.0	74		37.c	24	107 4	62.0	74	150.7	87.0	24	194.0	112.0	74	237.3	137 0
25	21.7	12.5	75	55.0	37.5	25	108.3	62.5	75	151.6	87.5	25	194.9	112.5	75	238.2	137.5
26	22.5	13.0	76	65.8	38.0	126	109.1	63,0	176	152.4	88.0	226	195 7	113.0	276	239.0	1380
27	23.4		77	66,7	38.5	27	110.0	63.5	77	153.3	88.5	27	196,6	113.5	77	239 9	138.5
28		14,0	78	67.5	39.0	28	1108		78	154 1	890	28	197 4	114.0	78	240.7	139 0
	25.1			68,4	39.5	29	111.7	64,5	73	155.0	89.5	29		114.5	79	241 6	139.5
30		15.0	80	09.3	40.0	30	112.6		80	155.9	90.0	30	199 2	115.0	80	242,5	140.0
31	26.8	15.5	81	70.1	113	131	113.4		181	156.7	90.5	531	200.0		281	243.3	140 5
32		16.0	82		41,0	32		66.0	82	157.6	91.0	32		116.0	82	244 2	141 0
33		16.5	82	71.9	1. 3	33	-	66.5	83	158.5	91.5	33		116.5	83	245.1	141.5
34	29.4	17.0	84	73.6	1	34	116.9	67,0	1 0	159.3	92.0	34		117.5	85	245 9 246 8	142.0
35	30.3	17.5	-		-	35					_	35	203.5		-		
35	31,2	18.0	86	74.5	43.0	136	117.8		186	161,1	93.0	236	204.4	118.0	286	247.7	143.0
37		18.5	28	76.3	43.5 44.0	37	119.5	60.0	88	162.8	93.5	37	206,1		88	249 4	144.0
39	32.8	19.0	80	77.1	44.5	30	120,4	69.5		163 7		39	207.0	119.5		250.3	
40	34.6	20.0	90	77.9	45.0	40	121.2		90	164.5	950	10	207.8	1200	90	251.1	145.0
41	-		01	78 8	45.5	141	122,1	-	101	165.4		-		120.5		252.0	
42	36.4	20.5	02	70.7	45.5	42	1230		92	166.3	96.0	42	209 6	121.0		252.9	146.0
43		21.5	93	80.5	46.5	43	123.8	71.5	93	167 1	96.5			121.5	93	253,7	146.5
44	38.1	22.C	94	81.4	47.0	44	124.7	72.0	94	168.c	97 0	44	211.3	122,0	94	254.6	
45		22 5	95	82,3	47.5	45	125 6		95	168.9	97.5			122 5		255.5	
45	-	23.0			48.0	146	126.4			169 7	98,0	246	2130	123.0	296	256.3	11,000,000,000
47		23.5	97	84 c	48.5	47	127.3	73.5	97	170.6	98.5	47	213.9	123.5	97	257,2	148 3
48		24.0		84 9	49,0	48	128.2	74.0	98	171.5	99.0	48	214 8	124.0	98	258,1	149.0
49	42.4	24.5	99	85.7	49.5	49	129 0	74,5	99	172.3	99.5	49	215.6	124.5		258.9	149.5
50		24.0	100	86.6	50.0	150	129 9	75.0		173.2				125.0	100		150.0
Diff	Den	Lat	Dit	Dep	Lar	Ditt	Dep	La	Dift	Der	La	Ditt	De	L	Diff	Dep	Lat
-	-	-	-		•				-			11411	100	1	120		TO NO. OF

for 60 Deg.

-	L	10-	uD.	1.1	Der	I:D:a	1100	IDen	VD.A		10						3
_	Lat	-	-	-	Dep	-		Dep	-			Diff		Dep	Dift	Lat	Dep
1		00,5	11 -		26.3	02		52.0	11			201		103 5	251	215.1	129.3
2	02.6		11 -	1	27.3	03		53.0		130.3		02	173,1				129.8
3	03.4	1	11 30	1	27.8	04	89,1	53.6	11	132.0		03		104.5	53	216.8	3 3
. 5	04 3	02.6	55	47.1	28.3	05	90.0	54.1	55	132.8	79.8	05	175.7		55	218 5	130.8
6						106	90.8	54.6	156	133.7	80.3	206	176.5	_	256	219.4	-
7		03.6	11 - 2	48,8		07	91.7	55.1	57	134.5	80.6	07	177 4	106.6	57	220.2	1 3
8		04.1	58		30.4	08	92.6	-6 -	58	135.4		08		107.1	58	221.1	132.9
10	1.0 /	05.2	11 2 -	51.4		10	93 4 94 3	56.7	59	136.3	81.9	10	1	107.6	59	222.0	133.4
11	200	-	11 2	52.3	-	111	95.1	57.2	161	138.0		-	-	_	60	222 8	133 9
12	1 1		11 /	53.1	31 9	12	96.0	57.7	62	138.8	83 4	12	180 8	108.7	62	223.7	134.4
13	11.1		63	54 0	32.4	13	96.8	58.2	63	139.7		13		109.7	1	224 5	134 9
14	1	07.2	11 0	10.	33.0	14	97.7		64	140.5	84.5	14		110.2	64	226.2	33 1
15	12 9	-	11	-	33.5	15	98.6		65	141.4		15	184.3		65	227.1	136.5
16	13.7		66		34.0	116		59.7	166	142.3	85.5	216	185.1	111.2		228.0	137.0
17		03,8			34,5 35.c	17	100.3	2 6	68	143.1	86.0	17	186.0		100		137.5
19		39 8	11 -	59.1		19	102.0	4 .	69	144.8	0	10	186.8		68	229.7	138.0
20	17.1	10000	70	000	30. L	20	102,8	61.8	70	145,7	87.6	20	188.5	113.3		230.5	138.5
21	18.0	10.8	71	60 8	36,6	121	103.7	62 3	171	146.5	88,1	221	189.4	_	-	232.2	-
22	18.9		72		37.1	22		62.2	72	147.4	88.6	22	190.3			233.1	139.6
23	19.7		73		37.6	23	3 1	63.3	73	148.3	89 1	23	191.1	114.8		234.0	
24	21.4	12.4	74	53 4 64.3		24	106.3		74	149.1	89.6	24	192.0	115.4		234 8	141.1
26	22.3	-	76	65.1		126	108.0	_		150.0	_	25	192.8			235.7	141.6
27	23.1		77	66.0		1 5 8	108.8			150.8	90.6	226	193.7	116.4		236,5	142.1
28	1	14.4	78	66.8			109.7			152.5	91.7	28	195.4			237.4	142.7
29	24 9	14,9	79	1 1	40.7	29	110.6		79	153.4	92,2	29	196.3			239.1	143,2
30	25.7	15,5	-	68,6	41.2	30		67.0		154.3	92 7	30	197.1	118.5	9-1	240.0	144.2
31	26,6		81		41.7		1	67.5	181	155,1	93.2	231	198.0	119.0	181	240.8	144.7
32	18.3	16,5		70.3	5 6 7		113.1	68.c	82	156 0 156.8	93.7		1988		0 1	241.7	145.2
34	29.1	17.5	84	,	43.3		114.8			157,7	94.8	33	199.7	120.0	0 . 1	242.5	145.7
35	30.0	180	85	72.8	43.8			69.5		158.5	95 3	35		121.0	3 1	243.4	146,8
36	30.9	18.5	86		44.3	136	116.6	70 C	26	159.4	95.8	-		121.5	186	2451	147.3
37		19,1	87	746	44 8		117.4		87	160 3	96.3	37		122.1	a 1	246 c	147,8
38		196	88	75.4	45.3	38	118.3	71.1		161.1	96 8	38	204.0	122.6	88	246.8	148.3
39	33.4	20.1	90	76.3	46.4	39	119 1	72.1	89	152.0		39	204.8	123.1			148,8
40	35.1	20 6	2	78.0	16.0		120.8		-		97.9		205.7			248.5	
		21.6					121.7	22.1	02	164.5		42	206.5	124.1	291	249.4	149 9
43	26.9	22.1	93	79.7	47,9	43	122.6				99.4	43	208.3	125.1	02	250 2	150.4
44	37.7	22.6	94	80.6	48,4	44	123.4	74.2	94	166.3	99,9	44	209.1	125.6	94	252.0	151.4
45	38.6	23,2		81.4		_	124.3				100.4	45	210.0	126.2	95	2528	151 9
40	39.4	23.7	96	82.3	49.4	146	125.1	75.2	196	168.0	100.9	246	210.8	126.7	296	253.7	152.4
		24.2	97	84.0	50.0	47	120.0	75.71	97	168,8	101.5	47	211.7	127.2	97	254 5	1530
	41.1 42.c	25.2	50	84.8	51.0	40	127.7	76.2	90	170.5	102.0	48	212.5 213.4	127.7	98	255.4	153.5
50	42.9	258	100	85.7	51.5	150	128.6	77.3	200	171.4	103 0	250	214 2	128 9		250.2	154.0 154.5
NiR	Dep	Lat	Dift	De	Lat	Diff	Dep	Lai	Dift	Dei	Lat		Dep		Dift		-
-	P									20,	Lat	Dilli	Dep 1	La.	ושות	Deb	Lat

DA	Lat	Dep	Diff	Lar	Dep	Dift	Lat	Dep	Dia	Lat	Dep	DiA	Lat.	Dep.	Dift	Lat	Dep
1	00.8	00,5	51	43.2	27.0	101	85.6	53.5	151	128 0	80.0	201	170.4	106.5	251	212.8	133
2	01.7	1	52	44.1	27.6	02	86.5		52	128.9	80.6	02	171.3	107.1	1	213.7	23
3	02.5	01.6	53	44.9	28,1	03		54.6	53	129.7	81.1	03	172.1	107.6	1000	214.5	
4	03.4	02.1	54	45.8	28.6	04	88 2	55.1	- 54	130.6	81.6	04		108,1	54	215.4	134
5	04.2	02.7	55	46.6	29.2	05	89,0	55.7	55	131.4	82.2	05	173.8	108 7	55	216.2	135
6	05.1	03 2	56	47.5	29.7	106	89.9	56.2	156	132.3	82.7	206	174.7	109.2	256	217.1	135
7	05.9	03-7	57	48,3	30.2	07	90.7	56.7	57	133.1	83.2	07	175.5	109.7	57	217.9	136
8			58	49,2	30.7	08	91.6	57.2	58	134.0	83.7	08	176.4	110.2	58	218.8	136
9		04.8	59	50.0		09	92.4	57.8	59	134.8	84.3	09	177.2	20 - 1 - 0	59	219.6	137
10	08.5	05.3	60	50.9	31.8	10	93.3	58.3	_	135.7	84.8	10	175 1	111.3	60	220.5	137
11	09.3	05.8	61	51.7	32.3	111	94 1	58.8		136.5	85,3	211	178 9	production of the same	261	221.3	138
12	10,2	06.4	62	52.6	32.9	12	95.0	59.4		137.4	85.9	12	179.8	112.4	62	222.2	138
13	11.0	06.9	63	53.4	33 4	13	95.8	59.9		138.2	86.4	13		112.9		223.0	139
14	11.9	07.4	64	54 3	33 9	14	96.7	00.4	64	139.1	86.9	14	181.5		64	2239	1 39
15	12.7	08 0	05	55,1	34,5	15	97.5	01.0	.05	139.9	87 5	15	182.3	114.0	05	224 7	140
16	13.6	08,5	66	56.0		116	98.4	61.5		140.8	88,0	216	183.2	114.5	266	225 6	141
17	14.4	09,0	67	56.8	35.5	17	99.2	62.C	1	141.6	88.5	17	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	115.00	67	226 4	141
18	15.3		68	57.7	1 0	15.15	100.1	62.5	68		89 0	18	184.9	- 6		227.3	142
19	1	10,1	69	10 0	30,0		100,9	63.1	69	143 3	89.6	19	185.	116 1		228.1	142
20	17.0	10.6	70	59 4	37.1	20		63.6	79	144.2	90.1	20	186.6	116.t	70	229.0	143
2 1	17.8	103 113 11	71	60.2	37.6		102.6	64,1	171	145.0	90.6	221	187.4	117.1	271	229.8	143
22	18.7	11.7	72		38.2		103.5	047	72	45,9	91,2	22	188.3	117.7	72	230.7	144
23	19.5	12.2	73	61.9	E			5.2	73	146.7	93.7	23	189.1		73	231.5	144
24	20.4	12.7	74	62.8	F-1	24	105.2	65.7	74	147.0	92,2	24	190.0		74	232.4	14.5
25	21.2	13.3	75	03 6	39.8	25	106 0	00.3	75	148.4	92.8	25	190.8	119 3	1.75	233.2	14
26	22.0	1 3.8	76	64.4	40.3	126	106 8	66.8	176	149.2	93.3	226	191.6	A COLOR	276	23:0	146
27	22.9		77	65.3		1	107.7	27.3	77	150.1	93.8	47	192.5	100	77	2349	146
28	23.7	14,8	78	66.1	41.3	28		69 4	78	150.9	94.3	28	193.3	120.8	78	235.7	147
29	24.0	15,4	1 0	67.0	41.9	29	109 4	68.4	79	151,8	94.9	29	194.2	1	100	238,0	
30	25.4		-	67.8	41.4	30	110.2	68,9	80	152 6	95.4	3c	1950	121 9	80	237-4	148
31	26,3	16,4	81	68,7	42.9	131	111.1	69,4	181	153 5	95.9	231	1959	1224		238.3	148
32		17.0	82	69.5	44	32	1119	700		154.3	96.5	32	190.7	123.0		239 1	149
33	28.C		83	70.4	44 0	33	112.8	70.5	0	155,2	97,0	33	197 6		1 0 .	240.0	
34	28.8	18.6	84	71.2	44 5	34	113.0	71.6	0	156 0	97.5	34	198 4	124.0	84	240.8	150
35	29.7	10.0	85	72,1	+5	35	114.5	_	-		-	35	199.3	124 0	3	241.7	151
36	30.5	1	86	72.9	45.0	136	115 3	72.1	186	157,7	98.6	236	200.1	125.1	286	242.5	151
37	31.4		87	73.8	46.1	37	110.2	72 0	1 00	158 6	99 1	37	201.0	125.0	07	243.4	1 52
38		20.1	88	74.6	47 2	30	117.0	72.2	80	159.4	100 2		201.8	126.7	80	244.2	152
		20.7	09	76.3	47.2	39	118.7	74.2	00	161.1	100 7		203 5			245 1	153
40		21.2	1 30	70.3	10	-										245.9	
11		21.7	91	77.2	40,2	141	119 6	74 7	191	172.0	101.2	241	204.4	7.7		246.8	
42		22.3	92	78.9	40.0	42	120.4						205.2	128.8	92	247.6	154
		22.8	93	79.7	40.8	43	122.1	76.2	93	164.5	102.8		206 9			248.5	
	28.2	23,3		80.6	50.4	45	123.0	76.0	05	165.4			207.8			249.3	
45			95							-		-	_	The same	-	250.2	
46		24.4	96	81.4	50.9	140	123.8	77.0	190	160.2	1039		208.6		290	251.c	150
		24,9	97	82.3	51.4	47	124.7	78 4	97	167.1	104 4		210.3	130 9		251.0	
	41.6	25.4	90	84.0	52.5	40	176	70.0	90	168 8	105 5			131.0		253 6	
52	42.4	26	100	84.8	52.0	750	127.2	79.6	200	160 6	106,0	200	212.0	122 5		254 4	150
10	-		0:0	D	33	10.0	Dep	100	13.0	D	Los		Dep				
111	Den'	1.3 1	UIII	Del	Lat	Dill	Det	La	ווע	De	Pari	וווען	Deb !	Lai	Dift	Deb ,	L

·I	Difference of	Latitude	and Departu	re for 3	3 Deg.	3
5	the second secon				The state of the	

1	1			100			19	100		12/5		-					33
Dit	Lat	Det	Dill	Lar	Dep	Ditt	Lat	Dep	Ditt	Lat	Dep	Dift	Lat.	Dep	Dut	Lat	Dep
1	00.8	00,5	51	42.8		101	84.7			126.6	82.2	201	168.6	109.5	251	210.5	136.7
2	01.7		52	43.6		02		55.5		127.5	82.8	02		110.0	52	211.3	
3	02.5	1000		44.4	Acres 15	03		56.1			83.3	03		110.6	001		137.8
4	03.4	1000	0.72	45.3	10 7 6 7	04	88 1	56.6	54	129.1	83.9	04		111.1			138.3
_5	04.2	-	55	-	30 0	05		31	55	130 0	84.4	05	171.9	_	-	213.8	138.9
6	05.0		56	47.8		106		57·7 58.3	156	130.8	85,0	206	172.8			214.7	139 4
7 8	05.9		57		31.6	08		58.8	57	131.7	85.5	08	173,6	112.7		215.5	
9	07.5	2000	59	49,5	-	09		59.4	59	133.3	86.6	09	Man e	113.8		217.2	140.5
10	08.4		60	50.3	7.	10		59.9	60	134.2	87.1	10		114.4	2-1	18.0	
-11	09.2	06.0	61	51.2	33 2	111	93.1	60.5	161	135.0	87.7	211	176 9	114.9	261	218.9	142.1
12	10,1		62	52.0		12	93.9	61.c	62	135.9	88,2	12		115.5	1 1	119.7	142.7
13	10.9	07.1	63	52.8	34,3	13	94 8	61.5	63	136.7	88.8	13	178.6	116.0	63 2	220.6	143,2
14		07.6	64	53.7		14	95.0	62.1	64	137.5	89 3	14		116.5	64 2	221.4	
15	12.6	_	65	54 5	354	15	-	62.6	65	1 38.4	89.9	15		117.1		222.2	144.3
16	13.4		66	55,3		116	97.3	63.2	166	139.2	90.4	216		117.6	. 1	223.1	144.9
17	14.3		68	56.2	37.0	17	98.1	64,3	68	140.0	90.9	17	182.8	118.2			145.4
19	15.1		69		37.6	19	99.8	64.8	69	141.7	92,0		183.7		- 1		146.0
20	16.8		70	58.7	38.1	20	100.6		70	142.6	92.6	20		119.8			147.0
21	17.6	-	71	59.5		121	101.5	-	171	143.4	93.1	221	_	120.4			
22	18.4			60.4	3 3 3	22	102.3		72	144.2	93.7	22	186.2	120.9			147,6
23		12.5	73	61.2		23	103.1	67.c	73	145.1	94.2	23	187.0	121.4			148,7
24	20.1		74	62.1		24	104.0		74	145,9	94.8	24	187.8	122.0		29.8	
25	21.0	13.6	75	62.9	40.8	25	104.8		75	146.8	95.3	25		122.5	75 2	30.6	149.8
26	21.8	14.2	76	63.7	41.4	126	105.7	68,6	176	147.6	95.8	226	189.5		276 2	31.5	150.3
27	1	14,7	77		41.9		106.5		77	148.4	96.4	27		123.6		32.3	150.9
28	23.5		78	65.4		28	107.3	1.00		149.3	96.9	28		124 2		33.1	
30	24.3	2	80		43.6	30	109.2	- a	79	150.1	98.0	30	192.0		79 2	34.8	151.9
31	26.0	-	81	67.9	-		109.9	-	-	151,8	98.6	231		125.8	0 1		
32	26,8		82	68,8		131	110.7			152.6	99.1	32	194.6	126.2	0 1		153.6
33		18.0	83	69.6	2	33	111.5			153.5	99,7	33	195.4			37.3	154.1
34	28.5	18.5	84	70.4	45.7	34	112.4		84	154.3	100.2		196.2		84 2	38.2	154.7
35	29.4	19,1	85	71.3	-	35	113.2	73.5	85	155,1	100.8	35	197.1	_	85 2	39.0	155.2
36	30.2		86	1, -, -	46.8	136	114.0			1560		236	197.9	128.5	286 2		155.8
37	31.0		87	73.0	47.4	37	114.9			156.8		37	198.7	129.1	87 2	40.7	156.3
38	31.9		100	73.8	47,9	38	115.7	75.2	88	157,7		38	199.6		88 2	41.5	156.8
39	32.7	21.8	00	74.0	48.5 49.0	39 40	116.6	76.2	00	150.5	102.9	40		130.2	00 2	42.4	157.4
40												-					157.9
42		22.3	91	70.3	49.6 50.1	42	118.2	77.3	191	161.0	104.6	42	202.1	131.2	02	44.0	158.5
43	36.1	23.4	93	78.0	50.6	43	110.0	77.0	03	161.8	105.1	43	203.8	132.3	93	44.9	159.6
44	36.9	24.0	94	78.8	51.2	44	120.8	78.4	94	152.7	105.7	44		132.9		246.5	160.1
45	37.7		95	79.7	51.7	45	121.6		95	163.5	106.2	45		133.4		247.4	160.7
45	38.6	25.1	96	80.5	52.3	146	122.4	79.5	196	164.4	106,7	246	206.3	134 0	296	248.2	161.2
47	39.4	25.6	97	81.3	52.8	47	123.3	80.1	97	165.2	107.3	47	207.1	134.5	97 3	240.1	161.7
48	40.3	26.1	98	82.2	53.4	48	124.1	80.6	98	166.0	107.8	4.8	208.0	135.1	98	240.0	162.2
50	41.1			8.3,0	53.9	49	125.0	81.1	99	166.9	108.4	49	208.8	135,6	99	250.7	162.8
0:0	41.9	27.2	100	03.9	54.5	150	125.8	01.7	200	107.7	100.9	2.00	209.7	130.2	300	251.6	103.4
Lin	Deb	La'	Dill	Dei	Lat	Ditt	Dep	IT31	MINIT	) Det	Lat	Din	Dep	Lar	Dist.	Пер	Lat
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11 (	Lat	Dep	Diff	Lat	Dep	Dift	La:	Dep	Dift	Lat	Dep	Dift	Lat.	Dep	Dift	Lat	Dep
1	00.8	00,6	51	42.3	28.5	101	83 7	56.5	151	125.2	84.4	201	166.6	112.4	251		140
2	01.7	01.1	52	43.1	29.1	02	84.6		52	126.0	85,0	02		113.0	52	208.9	140.
3	02.5	01.7	53	43.9		03	85.4		53	126.2	85.6	03		113.5	53	209.7	141.
4	03.3	02.2	54	44.8		04	87.0	58.2	54	127.7	86.1	04	169.1	114.1	54	210.6	142.
5	04.1	02.8	55	45.6	30.8	05		-	55	128.5	86.7	05	169 9	114.0	55	2114	142.
6		03 4	56	46.4	31.3	10:		59.3	156	129.3	87.2	206		115.2	256	212.2	143,
7	05.8	23.9	57	47 3		07		59.8	57	130.2	87.8	07	171.6		57	213.1	143.
8		24.5	58	48.1		08		60.4	58	131.0	88,4	08		116.3	58	213.9	144.
9		05.0	59	10	33.6	09	90.4	61.5	59	131.8	89 5	10	173,3	1	59	214.7	144
10	08.3	05.6	60	19,7		10		-	-			-		-		215.5	14.5
11	09.1	06.2	61	50.6		111	92.0	62.1	62	133.5	90.6	211	174 9	1 00	11	216.4	146
12		06.7	62	51.4		12			63	134.3	91,1	13	175.7	110.0	62	1	146
13		07.3	63	52.2	35.8	13	93.7	10	64	135.1		14	177.4		64		147
14	11.0	1 0	65	53.1	1 - 6 -	15		64,3	65	136.8		15	178.2		11	1	147
15	-	-	11	33.3	-	-	96.2	-	166	137.6	7.7	216	179.1	-	-	_	-
16	13:3	1	66	54 7	36.9	116	97,0		67	138.4		17		121.3	11 .		
17	14.9	1 3.3	68	55,5	37.5	17	97.8	66.0	68	139.3		18		121.0	11		
18		10.6	11	57.2	38.6	19		66.5	69	140.1	1	11		122.			1-43
20	1 . 2 .	11.2	1 70	1 0		20	99.5		70	140 9		11	182.4				1 3
21	17 4	1117	71	-	-	121	100.3	67 7	171	141.8	95.6	221	183.5	123.6	271	224.7	
22	1 1	12.3	11	10		22	101.	68.2	11 '	142.6				124.1			1 3
23	1.	12.9	11		1 0		102.0	68,8	11	143 4	-6 -	23			11		
24	1-		11 7		41.4	24	102.			144.2	97,3	24				227.1	1 0
25	20.	14.0	75	62.2	41.9	25	103.6	69,9	75	145.1	_	-	186.	5 125.8	75	228.0	
26	21.6	14,	76	63.	12.4	126	104	70 5	176	145,5	98.4	226	187.	4 126.	275	228.8	154
27	22.4	1	11	1 3		27	105	71.0	11 4 1			27					
28	23.	15.	78	64.	7 43.6	28	1 .	,	78			11	-	0 - '	11		155
29	24.0	16.2		1	5 44.2				11 6			1			- 11 - 2 -		
30	24.	9 16,8	80	66.	3 44	30			80		-	-	-	-	-   -		156
31	25	7 17.	11 0	- / -				337		1 .	1 6	111			11 0	3 .	157
32	26,	-		68	0 45.9							11 3		-		33	1-31
33		1	10		8 46.4	. 11 22	1		11 -						11 0		1 3
34		)	110			11		74.9	11 0		1	1		0	1 0		
35	-	-	-	-		-	-	-	-	-	-	-	-	-	-		-
36			11 0	1/	3 48.		1 1		1 186	1 3 1			1	1 3		1-31	1 3.
37	30.	11	11 0	0 1	1 48.	37	113.	4 77.3			9 105.	37	197.	5 132. 3 133.		2 9	160
38	31.	3 21.	8	73.	8 49.	38	115.	2 77.	80	156.	7 105.	39	198.	1 133,	6 8	239.	5 16
40		2 22.			6 50.		116.	78.	90	157,	5 106.	40	199.	0 134.	2 90	240.	1 16
41		-		_	_			78.8	TOI	T . 8.	106.	241	190.	8 124	8 20	1 241.	
42		8 23,			3 51.4			7 79.4	1 92	159.	2 107.	4 42	2 200.	6 135.	3 0	2 242.	1 16
4:	35.	6 24.	9		1 52.0			5 80.0	93	160.	0 107.	9 4:	201.	4 135,	9 9	3 242.	9 16
44		5 24,		4 77.	9 52.	6 44		4 80.	94	160.	8 108.	5 44	202.	3 136.	4 9	4 243.	7 16
4	37.	3 25.		5 78.	8 53.	1 45		2 81.			7 109.	4	203	1 137.	0 9	5 244.	6 16
45	38.	1 25.	-11		6 53.			0 81.6	-	-	5 109.	6 24	203.	9 137.			-
47	139.	0 26.	9	7 80.	4 54.	2 47	121.	9 82.2	2 97	163.	3 110.	2 4	7 204.	8 138.	1 9	7 246.	2 16
4	130.	8 26.	811 9	8 81.	2 54.	8 48	122.	7 82.	98	164.	1 110.	7 4	205.	6 138.	7 9	8 247.	0 16
45	40.	6 27.	1 9	9 82.	1 55.	4 49	123.	5 83.	3 99	165.	O III.	3 4	9 206.	4 139.	2 9	9 247.	9/16
5	41.	5 28.0	01	C 82,	9 55.	9 150	124.	4 83.	9 200	165.	8 111.	8 250	207.	3 139.	8  30	0 248.	7/16
-			- 41-				De		11	A 1 W		II TO	010	1 -	110:	4	L

	4-14	14.1	4	10, 10	171		•					-					
Diff	Lat	Der	Dift	Lat	Dep	Dift	Lat	De	Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep
1	00.8	00.6	51	41.8	29.2	101		57.9	151	123 7	86.6	201	164.6	115,3		205.6	
		01.1	52		29.8	02		58.5	52	124.5	87.2	02		115.8		206.4	
3	02.5	01,7	53		30.4	03		59 1	53	125.3	87.7	03		116.4			
4	03 3	1 7	11	44.2		04		59.6	54	126.1	88.3	05	167.1	117.0			
5	04.1	02 9	55	450	-	05	-	60.2	55		-	-	-		-	208.8	
6		03.4	.56	45.9		106	86.8			127.8	89.5	206	168.7	113.1		209.6	
7		04.0	57	46.7		07		61,4	57	128.6	90 0	08	169.5	118.7		210.5	
8		04.6	58	48.3	33.3	09		62,5	59	130.2	91.2	09	171.2	119,9		211.3	
10	1	05,7	60	49.1		10		63.1	60	131.0	918	10	172.0	120.4		212.9	
11	-	06.3	61	50.0	-	111	90.9		161		92.3	211	172.8	121,0		213 8	Street streets
12		06.9	62		35.6	12	91.7			132.7	92.9	12		121.6		214.6	
13		07.5	63		36.1	13		64.8		1335	93.5	13	174.4	122.2		215.4	
14		08.0	64		36.7	14	93.4	65.4	64	134.3	94.1	14	175.3	122.7		216.2	
15		08.6	65	53.2	37.3	15	94.2	66.0	65	135.1	94.6	15	176 1	123.3	65	217.0	152,0
16	13.1	09.2	66	54.1	37.9	116	950	66.5	166	136.0	95.2	216	176.9	123.9	266	217.8	152.6
17	1 -	09.7	67		38,4	17		67.1	67	136.8	95.8	17	177.7	124.4	67	218.7	153.1
18	14.7	10.3	68	55,7	39.0	18		67.7	68	137.6		18		125.0		219.5	
19	1 2	10.9	69		39.6	19		68.2	69	138 4	96.9	19	179.4	125 6		220.3	
20	16.4	11.5	70	57.3	_	20	98.3		70	139.2	97.5	20	130.2	126:2	-	221.1	
21	17.2		71	1 -	40.7	121		69,4	171	140.0		221	1810	126.7	1	221.9	
22		12.6	72		41.3	22		70.0	72	140.9	98.6	22	181,8	127.3	72		1560
23		13.2	73	1	41.9	23	100.7		73	141.7	99.8		133 5		74	223.6	1 - 1
24	20.5	13.8	74 75	4 3 1	43.0	25	101.6	1.	75					129.0	75		157.1
-	-	-	1		_	126			-		100.9		-		-	-	
26	21.3		76		43.6	27	103.2	. 0	77	144.1		11	185.1	130.2	77	226.c	158.9
27	22.1	15.5	78	1 -	44 7	28	104.8		78	145.8		28		130.8	78		159 4
29	23.8		11	4	45.3	29	105.6		79	146.6	1	29	187.5		79		160.0
30	24.6		11 0-	1	45.9	30	106.5		80	247.4	103.2	30	188.4		80	229.3	160.6
31	25.4	-	81	-	46.5	131	107,3	75.1	181	148.2	103 8	231	189.2	132,5	281	230 1	161.2
32	26.2	1 0		1 -	47.0	32	108.1	75.7	82	149.1	104.4		190.0		82	231.0	161.7
33	27.0	18.9	83	68.0	47.6	33	108.9		83		105.0	33		133 6		231.8	
34	27.8	19.5			48.2	34	109.7		84					134 2			162.9
35	28.7	20.1	85	69.6	48.7	35	110.6		85	-		-		134 8		233.4	
36			11 -	1000	49.3	136	111.4	78.0	186			11		1	286	1 3 1	1640
37	30.3	21,2	87	1, 0	49.9	37	112.2	78.6	87					135.5	87	235.6	164.6
38	31.1	21.8	88		50.5	38	113.0	79.1	88	154.6	107.8	30	194.9	136.5	80	235 9	165.2
39		22.4	89	72.9	51.6	40	114 6	80.2	89		100.4	40	196.6	137.1	00		165.7
40	-	23.0			-					-	_	-	-		-	-	166.9
41	100	23.5		74.5	52.2	141	116.	80.9	191		109.5			138.8			167 5
42		24.7	92	75.3	53.3	42	117.1	82.0	92		110.7			139.4	91	240.0	168 0
44		25.2			53.9	44	117.9	82.6	94		111.3		199.8	139.9	94		168.6
45		25.8			54.5		118.8	83.2	95	159	111.8			140.5			169.2
46		7 26.4			55.1		-		196	-	112.4		-	141 1		w leading	169.8
47		5 27.0			4 55.6	47	120.4	184.3		161.	113.0	47	202.3	141.7			170,3
48		3 27.		80.	3 56.2	48	121.2	84.9	98	162.2	113.6	48	203.1	1 142.2	98	8 244.	1 170.9
49		1 28.	1 99	81.	1 56.8	49	122.0	85.5	1 99	163.0	114 1	49	203.	142.8	99	9 244.	9 171.5
50		0 28.	7 100	81.	9 57.4	150	122.	86.0		_		_	_	7 143.4			7 172.1
Di	it De	PLat	Di	De	Lat	Dif	Dep	La	Dif	Den	Lat	Di	Dep	Lat	Di	Den	I.at
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Difi	Lat	Dep	Dift	Lat	Dep	Dift	Lat	De	Dift	Lat	Dep	Ditt	Lat	Dep	Dift	Lat	Dep
1	00.8	00.6	51	41.3	30.0	101	81.7	59.4	151	122.2	88.8	201	162.6	118.1	251	203.1	147.5
		01.2	52	42.1	30.6	02		60.0	52	123.0	89.3		163.4		52	203.9	148.1
3	-2.4	01,8	53	42.9	-	03		60.5	1	123.8	899		164.2	0.000	53	204.7	148.7
4	03 2			43.7	1 2	04		61,1	54	124.6	90.5		165.0		54		149.3
5	04.0	02.9	55	44.5	32.3	25		61.7	55	125 4	91.1	05	165.8			206.3	149,9
6	04.9		56	45.3	32.9	106			156	126.2	91.7		156.7			207.1	
7	1 3 1	04.1	57	46.1	-	07		62,9	57	127.0	92.3	07	167.5	121.7	57	207.9	151.1
8	-	04.7	58	46 9		09		64.1	58	127.8	93.5	1	169.1			208.7	
9	98.1	05.3	59 60	48.5	34.7	10	Py 15	64.7	59	129 4	94.0		169.9	PROPERTY AND ADDRESS.	59	210.3	
-	-		61		-	111		65.2	-	130.2	94.6	211			261		-
11	09.7	07.1	62	50.2	100	12		65.8		131.1	95.2		170.7		62	211.1	155.4
13	10,5		63	51 0		13		66.4		131.9	95.8		172.3				154.6
14		08.2	64	51.8		14		67.0		132.7	96.4		173.1	0	64	2136	
15	12.1	08.8c	65	52.6		15		67.6	65	133.5	97.0	15	173.9	126.4	65	214.4	
16	12.9		66	53.4	0.0	116		68.2	-	134.3	97.6	216	174.7	127.0		215.2	-
17	13,8		67		39.4	17	94.7	68.8	67	135.1	98.2	1.00	175.6			216.0	
18	14.6		68	55:0	40.0	18		69.4	68	135.9	98.7		176 4	128.1	68	216.8	157.5
19	15.4	11.2	69	55,8	40.6	19		69,9	69	136.7	99.3	19	177.2	128.7	69	217.6	
20	16.2	11.8	70	56.6	41.1	20	97.1	70.5	70	137.5	99 9	20	178.0	129.3	70	218.4	158.7
21	17.0	12,3	71	57.4	41.7	121	97.9	71.1	171	138 3	100 5	221	178.8	129.9	271	219.2	159.3
22	17.8	12 9	72	58.2	42.3	22	98.7	71.7	72	139.1	101.1	22	179.6	130.5		220.0	
23	18.6	13.5	73	59.1	42.9	23	99.5	72,3	73	140.0		23	180.4		73	220.9	160.5
24	19.4	14 1		59.9		24	100.3		74	140.8		24	181,2		74		
25	20.2	14.7	75	60.7	44 1	25	101.1	73.5	75	141.6	102,9	25	182.0	132,3	75	222.5	161.6
26		15.3	76	61.5	44 7	126	101.9	74.1	176	142.4	103.5	226	182.8		276	223.3	162.2
27	21.8		77		45.3	27	102.7		77	143.2				133.4	77		162.8
28	22.7	16.5	1	63.1	1	28	103.6		78		104.0	11	184.5			224.9	
29	23.5	17.6	79 80		46.4	30	104.4	1. 2	80		105.2		185.3	134.0	79	225.7	
30	44.3	_	-	-	47.0		-	-	-		-	-		135.2	-		
31	25.1	18.2	81		47.6	131	106.8		181	146.4		11 3	186.9	3.3	82	227.3	
32	1 3 0		83		48.2	32	107,6		83		107.0		187.7			228.9	165.8
33 34	27.5	19.4 20 C	84	1 - 5	49.4	34	108.4		84		108.2		189.3		84	229.8	
35	28.3	206	85		50.0		109.2		85	149.7		35	190.1	138.1	85	230.6	
36	29.1	31,2	86		50.6	136	110.0	-	186	150.5	109.3		190.9	-	286	-	168.1
37	29.1		87	-	51.1	37	110.8		87		109.9		191.7	139.3	87		1
38		22.3	00		51.7	- 0	111.6	0			110.5			139.9	00	233.0	
39		22.6	89	72.0	52.3	39	112.5	81.7	89	152.9	111.1	39		140.5	89	233,8	169.9
40		23.5	90	72.8	52.9	40	113.3	82.3	90		111.7		194.2	141.1	90	234.6	170,
41	33.2	24.1	91	73.6	53.5		114.1			154.5	112.3	241	195.0	141.7		235.4	_
42	34.0	24.7	92		54.1	42	114.9	183.5	92	155.3	112.9	42	195.8	142.2	92	236.2	
43	34.8	25.3	93	75.2	54 7	43	115.7	84.1	93	156.1	113.4	43	196.6	142.8	93	237.0	
44	35,6	25.9	94	76.0	55.3	44	116.5	84.6	94	156.9	114.0		197.4	143.4	94	237.8	172,
45 46	36.4	26.5	95	76.9	55.8	45	117.3		95		114.6		_	144.0		238.7	173.4
46	37.2	27.C	96	77.7	56.4	146	118.1				115.2		199.0	144.6		239.5	174.0
47	38.0	27.6	97	78.5	157.0	47	118.9	86.4	97					145,2	97	240.3	174.6
48	38.8	28.2	98	79.3	57.6	48	119 7	87.0	98					145.8		241.1	
49		28.8		80.1	58 2	49	120,5	87.6	99	101.0	117.0	49	201.4	146.4		241.9	
50	-	29.4	100		58.8									146.9		242.7	
Dil	Dep	Lat	Dia	Dep	Lat	Dift	Dep	( La.	Dift	Dep	Lat	Dift	Dep	Lat	Diff	Dep	I Lat

The	11 00	Dep	Dia	(F at	Den	A.CIV	Lat	Dep	ID.A	Lat	Dep	Dift	Lat	Dep	(Dift	Lat	Dep
-		-		-		101		60.8	151			-		121.0	251	200.4	_
1		00 6	51	40.7		02		61.4		121,4	100000000000000000000000000000000000000	.02	161.3		52		151.6
2	23.32	31.8		42,3		03	82.3	62.0		122.2	92.1	03	162.1	122.2	53	202,0	152.2
1	1	32.4		43.1		04		62.6	54	1130	92.7	04		122.8	54	202.8	
5		03.0	55	13.9	33.7	05		63,2	55	123.8	93.3	05	163.7	123.4	55	203.6	153.5
6	04.8	03.6	56	44.7	33.7	106	84.7	63.8	156	124.6	93.9	41.00	164.5	124.0	256	204.4	
7		04.2	57	45.5		07	85.5	64,4	57	125 4	94.5	07	165.3		57	205.2	
8		04.8	-	46.3		08	2	650	3-	126.2	95.1		166,1 166,9		58	206.0	155.3
9		05.4	59	47.1	35.5	09		66.2	59 60	127.8	96.3		167.7	126.4	60	207,6	
10	-		-	47 9	-	-	88 6	66.8	161	128.6	96.9	211	168.5	127.0	261	208,0	157.1
11	17.77.7	05,6	61	48.7	36.7	111		67,4	62	129 4	97.5	7.5	169.3		62	209 2	
13		07.8	63			13	90.2		1	130.2	98.1		170.1		63	210.0	
14		08.4	64		38.5	14	91.0	68.6	64	131.c	98.7	14	170.9		_64	210.8	
15		09.0	65		39 1	15	91.8	69 2	65	131.8	99.3	15	171.7	129.4	65	211.6	159.5
16	12.8	09 6	66	52.7	39.7	116	92.1	69.8	166	132.6	99.9	216	172.5	130.0	266	212.4	
17		10.2	67	53-5	40.3	17		70.4	67	133.4			173.3	Control of the Control	67	213,2	
18		10.8		54.3		18		71.0	68	134.2		18	174.1		68	214.0	161.9
19	1	11,4		55.1		20	95.c 95.8	71.6		135.8	102.2	19	174.9	132.4	70	215.6	0.000
20	-	12.0	70	-		-			-		102.9	221	176.5	133.0	271		163.1
21		12 6	71		42.7	121		72.8	72	137,4			177.3		72	217.2	
22		13.2		57.5		23		74.0		138.2			178.1		73	218.0	2 1
24		14,4	74	-4.		24		74,6	74	139.0		24	178.9		74	218.8	
25	1 .	15.0	75	1		25		75.2	75	139.8	105.3	25	179.7	1354	75	219.6	165.5
26	20.8	_	76	60.7	45.7	126	100.6	75.8		140.6		226		136.0	276	220,4	
27	21.6	16.2	77		46,3	27	101.4	76.4		141.4		27	181.3		77		166,7
28	22.4	16.9		62.3		28	102.2			142.2		1	182.1		78		167.3
29		17.5		63.1		29	103.0	77.0	1 0	142.9			182.9		79	222.8	
30		18.1	80	-	_	30	103.8		_	143.7					281	-	_
31	24.8		81	1	48.7	131	104.6		181	144.5		231 32	184.5 185,3		82	224.4	169.1
32		19.3		66,3	49.3	32	105.4		100000	146.1	110.1	33	186.1		83		170.3
33	26.4	20.5		67.1		34	107.0		84	146,9		34	186.9	0	84	226.8	
35		21.1		67.9		35	107.8	81.2	85	147.7	111.3	35	187.7	141.4	85	227.6	1715
36				68,7		136	108.6		186	148.5	111.9	236	188.5	142.0	286	228.4	172.1
37		22.3	87	69.5	52.4	37	100.4	82.4	87	149.3	112.5	37		142.6	87		172.7
38	30.	22.9	88	70.3	53,0	38	110.2	83.0	88	1 3	113,1		190 1		88		173.3
39	31,1	23.5	1 89	71.1	53.6	39	111.0	83.6	89	150.9	113.7		190.9	143.8		230.8	173.9
40	31.9	24.1			54.2		111.8				114.3	_		144.4			174,5
41	32.7	24.7	91	72.7	54.8	141	112.6	84.9	191	152.5	114.9		192.5	145,0		232.4	
42		25.3	92	73.5	55.4	1 42	113.4	86.1	92	153.3	115.5	42	194.1	145.6	93	234.0	175.7
43	34.	25.9	93	74.3	56.6	44	114.2	86.7	93	154.0	116.7		194.9	146.8	94	234.8	176.9
45	357	20,5			57.2		115.8	87,3	95	155.7	117.3	45	195.7	147.4	95	235.6	177.5
45	35.	7 27.7			57.8		116	87.0	106		117.9	246	196,5	148.0	296	236,4	178.1
47	30.	5 28.3	9	777	58.4	47	117.4	88.5	97	157-3	1118.0	47	197.3	148.6	1 97	237.2	178.7
47	38.	3 28.9	9	8 78.	59.0	48	118.2	189.1	1 98	1158.	1 1 1 9.2	40	198.1	149.2	98	238.0	179.3
40		1 29.5		9 79	1 59.6	49	119.0	89,7	99	158.9	119.8	49	198.9	149.8	99	238.8	179 9
56	139.	9 30.1	10	0 79.	9 60.2	150					120.4	250	199				180.5
Di	De	Lat	Di	ft De	La	Dif	t Dep	La	Di	A Dep	La	Dit	Dep	Lat	Diff	Dep	Lat

# 38 Difference of Latitude and Departure for 38 Deg.

וווע	Lat	Derl	Dift	Lat	Dep	DA	Lat	Dep	Diff	Lat	Dep-	Dift	Lat	Dep	Dift	Lat	Dep
1	00.8	00 6	51	40.2	31.4	101	79.0	62.2	151	119.0	93.0	201	158.4	123 8	251	197.8	
2	01.6		-	7.	32.0	02	80,4	02.8		119.8	93.6	03	159.2	124.4	52		155.2
	02.4	01.8	53	41.8	32.6	03	-	63,4		120.5	94.2	1	159 9	-	53	199.3	
4	03.2	02.5	54		33.2	04	100	64.0		121,3	94.8	1	160.7	17 19 10	54	200.1	
5	03.9	03.1	55	43.3	33 9	05	82.7	64,6	55	122.1	95.4	05	161.5		55	_	157.0
6	04:7	03.7	56	44.1	34.5	105		65.3		122.9	960		162.3	126.8	256	201 7	157.6
7		04.3			35.1	07		65.9		123.7	96.7			127.4	57	202,5	
8		04.9			35.7	08		66.5	- 1	124.5	97.3	1	163 9	-			158.9
9		05.5			36.3	09		67.1	2.	125.3	97.9	10	164.7		59	204.1	1 2
10	07.9	06 2	-	-	36.9	10		67,7	-		-		165.5		_	204.9	-
11	08.7		61		37.6	111		68.3	161	126.9	99.1	2 3 1	166.2		62	205.6	
12	09.5	07.4			38.2	12		69.0 69.6		127.6	99.7	12		130.5	63		161.9
13	10.2	08.0			38.8	13		70.2			101,0		168.6	-	64		162.5
14		08.6	6	1	39 4	100		70.8			101.6			132.4	65		163.2
15	-	-	66	-	-	115		71 +	166		102.2	-		133.0	-	-	163.8
10		09.9	11	52 5	40.6	17		72.0			102.8			133.6			164.4
17	13.4	10.5			41,9			72.7	63	1 1 1 1 1	103.4	11 0		134.2			165.0
18		11,7	11		42.5		93 8		69		104.1	19		134.8		211.0	1 -1 6
19		12.3			43.1	11		73.9	70	133.9	104.7	20		135.5	70	212.7	166,2
-	16.	-		-	9 43-7		-	74,5	171	134.7	105.3	22 I	174.1	-	271	213,	166,9
21	1				7 44.3			75.1	72		105 9	1		136.7		214.	
23	1.0	1 14.2			5 44,9			75.7	73		106.5			137.3	11	215.	
24		14,8			3 45.6			76.3	74		107.1			137.9			168.7
25				5 59,	1 46,2	25	98	77.0	75	137.	107 7	25	177.	138.9	75	216.	
26		5 16.0	7	6 59	9 46.	126		3 77.6		138.	7 108 4	226		139.			
27	1		7	7 60.	7 47.4	27	100.	73.2	77		5 109.0			139,8	77	218.	
28		1 17.2			5 48.0			78,8	11		2 109.6	11		140,4			171.2
29		9 17.9			2 48.		1	6 79.4			0 110.	. 11	1 .	141.0			8 171.8
30	23.	6 18.	5   8	_	049.	_		4 30.0		-	8 110.	-		141	-	-	6 172.4
31		4 19.		1	8 49.			2 80.7			6 111.	.11 -		142.			
32		2 19.			6 50.		1	81.3		1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11 -		8 142.			
33		0 20.			4 51.		1.00	8 8 1. g			0 113,			6 143			8 174.9
34		8 20	11 0		0 52.			4 33.						2 144.	1 0		1
3.5	-	6 21.	_	-	_			-	-	1000000	-	_	-				-
36					8 53,			9 84.4			5 114.			9 145,			1 176.
37		2 22.	1 0	8 60	5 5 <b>3</b> . 3 5 <b>4</b> .	37		785.0	85	148	1 115			5 146.	211	The state of the s	9 177.
3		9 23.	8	0 70	1 54.	8 30	100	5 85.	80	148	9 116.	5 39	188.	3 147	211	1	7 177.
39		5 24.	6 9		9 55.		110	3 86.	2 90	149	7 117.	0 40	189.	1 147.			4 178.
4	3-		11		.7 56.			1 36		_	5 117.	- 1		9 148.			_
4:		3 25		2 72	.5 56.	6 4:		9 87,	4 0	151	3 118.	2 4	190	7 149.	0 9	2 230	1 179.
4	2 2 2	.9 26,	5 0	3 73	.3 57.	3 4	1112	7 88.	0 9	152	.1 118.	8 4	19t.	5 149.	6 9	3 230	0 180.
4	4 44	.7 27.	1 9	4 74	.1 57.		1113	5 83.	7 9	1 152	9 119	4 4	4 192.	2 150.	2 9	4 231	6 181
4	5 35	,5 27.		5 74	9 58.		5 114	2 89.	3 9	5 153	6 120	1 4		0 150.		5 232	4 181.
4 4	6 26	.2 28	3 0	6 75	.6 59	1 14	6 115	0 89,	9 19	6 154	4 120	7 24	6 193	8 151.	5 29	6 233	2 182.
4	7 37	.0 28.	91 0	7 76	4 59	7 4	7 1115	8 90.	5 9	7 155	.2 121	3 4	7 194	6 152	1 9	7 234	0 182.
4	8 27	.8 29.	6 6	8 77	.2 60	3 4	8 116	691.	1 9	8 156	.0 121	9 4	8 195	4 152	7 9	3 234	8 183.
4	9 38	.6 30.	2 9	99 78	.061	0 4	9 117	491	71 9	9 156	8 122	5 4	9 190	2 153	3 9	9 225	6 184.
	€ 39	.4 30	8 10	00 78	8.8 61	6 15	0 118	.2 92.	4 20	0 157	.6 123	.1 25	0 197	153 L	.9 30	0 236	,4 184.
1.3																AlDei	Lat

119	1. 12/			7											-	3 40	"
Ditt	-		Dift	Lat	Dep	Dia	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep
1	00,8	00,6	51	39 6	32.1	101	78.5	63.6	151	117.3	95,0	201	156.2	126.5	251	195.1	158.0
2		01,3		40.4	32.7	02	79.3		.52	118.1	95.7	10 1 1 m	157.0		52	195,8	158.6
. 3	-	01.9	12 12	41,2	7.00	93	80,0		53	118.9	96.3	1	157.8			196.6	
4	200	02:5		42.0	34.0	04		65.4	54	119.7	96,9	04	158.5			197.4	
_5	03.9	3	55	42.7	34.6	05		_	55	120.5	97.5	05	159.3	129 C		-	160.5
6		03,2	56	43.5	35	106	82.4	1	156	121.2	98.2	1200		129 6		198.9	
7 8	05.4	04,4	57	44.3	36.5	08	83,1	68.0	57	122.8	98,8	08	160.9	130.3	57	199.7	- / /
	07.0	5.7	59	45.8	37.3	09	84.7	68.6	59	123.6	99.4	1	162.4	131.5		200.5	
10	1 -1	00.3	60	46.6	10.	10		69 2	60	124.3	100 7	10		132.2	1		163.6
11	-	05.9	61	47.4	38.4	111	86.3	-	161	125.1	101,3	211	164.0	132.8		202.8	
12	1	07.6	62	48 2	1			70.5	62	125.0		12		133.4	1 1	203.6	
13		03,2	63			13	87.8		63	1	102.6	13		34.0	1 / 1	204.4	
14	10.9	08.8	64	49.7		14	88.6		64	,	103.2	14	166 3	: 34.7	6.1	205.2	
15	11.7	09:4	65	50.5	40.9	15	89.4	72.4	65	128.2	103.8	15	167.1	135 3	65	205 9	166.8
16	12 4	101	66	51.3	41.5	116	901	73.0	166	129,0	104.5	216	167,9	135 9	266	206.7	167.4
17	13.2	10.7	67	52.1	42.2	17	90.0	1 .	67	129 8	105.1	17			1 1	207.5	
18	1 -	11.3	68		12.8	18	91 7	7413	68	130.6	105 7	18	169.4	137.2		208.3	168.7
19	14.8		69	53 6		11	92,5	11.00	69	131.3	106.4	19	135600			209,0	
20		12.6	70	54.4	44,1	20	93 3	75.5	70	132.1	107.0	26	171.0	1 38 4	70	209.8	169.9
21		13 2	71	55.2	1	11	94.0		171	132.9	107.6	221	173.7	139.1	271	210.6	170.5
22		13.8		1 -	1.00	11	94,8		11	133,7		22		139.7	72		171.2
23		14,5		100	1.25		95.6		11		108.9	23			73	212,1	
24	18.7	15.1	74	57.5		11	97.1	78.0		135.2	1,09,5	24			74	212 9	100
26	-		-		-		-	-	75	-		1		-			173,1
		16.4	11		47.8		97.9		176	1 36.8		226	1 . 5	1	276	214.5	173.7
27		17.6				11 0	99.	1		137,5		27	170.4	142.9	77	215.3	174.3
29	1	18.2			1 49.7			10	79	139.1	1		178.0	1 . 3 2	79	216.8	1
30		18.9				1		81,8		139.9	Control of the second	30	0		80	217.6	1.13
31		19.5	81	62.0	51.0	-	101.	8 82.4	181	140.7		231		-	281	218.4	
32		20,1	82			.11	102.			141,4		11 -	1 0	146.0	1 .	219.1	
33		20,8	83	64.	-	11	103.	10	83				0		83	219.9	1112
34	26.4	21.4	84		3 52.9	34	104.	10		143.0	115.8	34		1	84	220.7	178,7
35		22.0	85	66.1	1 53.5	35	104.	85.0	85	143.8	116.4	35	182.6	147.9	85	221.5	179:4
36	28.0		18	1	54.1	136		200	186	144.5	117.1	236	183.4	148.5	286	222.3	180.0
37	28.8	23.3	87			37	106,	5 86.2		145.3	117,7	37	184.2	149.1	87	223.0	180,6
38		23.9		68.4	1 55.4	38	107.	86.8	88	146.1	118.3	3 8	185.0			223.8	181,2
39		24.5		69.2			108.	0 87.5		146.	118.9	39	185,7			224.6	181.9
40		25 2		69.			-	88,1	-		119.6		186.5				182.5
41		25.8	91	70.7		141		6 88.7			120.2		187.3				183.1
42		26.4		71.			110.				120.8		188.1			226.9	183.8
43		27,1	93	72.3	50,5	43	111.			150.0	121.5	4	188.8	152.9		227.7	184.4
44		27 7	94	73.8	8 50.8	44		791.2		150.0	122.7	4	100 4	154.2	94		185.6
46								_			-						
47		28.9	90	74.6	160.4	146		5 91.9		152.	124.0		191.2	154.8	296	230.0	186.3
48	37.2	30.2	08	76.2	61.	48	115	2 92.	97		124.6		192 7			221	6 187.
49		30.8	90	76.0	62.						125.2		193.			232,	4 188.
50							116.				125.9	250	194.	157.	300	233.	1 188.5
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6 04.6 03.9	4	03.1	2.9		TOTAL CO	-				3.1	1.0							
7 05.404.5 57 43.71 36.6 0.7 82.068.8 57 120.3 100 9] 07 158.6 133.1 57 106.6 16.5 1 58 44.4 37.3 08 83.570.1 10 10.6 03 159.3 133.7 58 1976 165.5 10 07.706.4 60 45.0 38.6 10 84.70.7 66 123.6 10.1 10 10.6 03 159.2 159 10.1 134.4 11.0 10.0 10.0 10.0 135.0 160.0 160.0 135.0 160.0 160.0 135.0 160.0 160.0 135.0 160.0 160.0 135.0 160		-			_		-	_	-				_	-	-			-
8 06. 10c.1   51   54   45   37.9   08   8a.7   66   45   71.0   10.16   09   100.1   134.4   66   46.0   38.6   10   07.7   06.4   07.7   06.4   07.7   06.4   07.7   06.4   07.7   06.4   07.7   06.4   07.7   06.4   07.7   06.4   07.7   07.5   07.7   07.5   07.7   07.5   07.7   07.5   07.	4						T. E								1000		196.1	164.6
9 06.90 c.8 59 45.2 37.9 00 83,5 70.1 59 121.8 102.2 09160.1 134.4 59 109.2 166.5 10 08.4 07.1 61 46.7 39.2 11 8.5.0 71.3 161 133.3 103.5 1.1 161.6 135.6 162 139.2 167.1 12 09.2 07.7 62 47.5 39.9 12 85.8 72.6 62 124.1 104.1 12 162.4 116.3 16.2 15.0 169.9 135.6 162.1 12.0 08.4 63 48.3 40.5 13 85.8 72.6 62 124.1 104.1 12 162.4 116.3 16.5 162.1 161.6 135.6 162.1 162.		3 .1						-				1 51					190,9	165.2
10   07, 7  06, 4  60   46, 0  38, 6  10   84, 3  70.7  60   123.6  103.8    10   160.9  135.6    60   199.2  167.7  12   09.2  07.7  62   47.5  39.9  13   85, 8  71.6    62   134.1  104.1    11   163.9  137.6    63   20.7, 168.8    13   163.2  136.9    64   125.6  105.4    11   163.9  137.6    65   138.6    17   19.0  10.9  65, 49.8  41.8  15   88.9  74.6    64   125.6  105.4    11.6    17.0	14 (12)		11	-		12. 2							4					
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16	1000			65	49.8	41.8	15				1 2		11	164.7		65	203.0	
17	-	12.3	10.2			42.4	116	88.0	74.6	166	127.2	106.7	216	165.4	1	256	-	
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21   16.1   13.5   71   54.4   45.6   121   92.7   77.8   71   131.0   109   9   221   169   3   142.1   271   207.6   174.7   23   176   14.8   73   55.2   46.9   23   94.2   79.1   73   132.5   111.2   23   170.8   143.3   73   209.1   175   24   18.4   15.4   74   56.7   47.6   24   95.0   79.7   74   133.3   111.9   24   170.8   143.3   73   209.1   175   208.3   174.1   209.9   176   25   19.2   16.1   75   77.4   48.2   25   95.7   30.4   75   134.0   112.5   25   172.3   144.6   75   210.6   176   27   20.7   17.4   27   20.7   17.4   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2   27.2   27.8   27   27.2   27.8   27   27.2   27.8   27   27.2	20	15 3	12.9	70	53.	45.0	20	91.9	77.1	70	130.	2 109,3	20	168 5	141.4	70	206.8	173.6
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23       17.6       14.8       73       55.9       4.9       23       94.2       79.1       73       132.5       5111.2       23       17.0       18.4       15.4       74       76.7       47.4       95.0       79.7       74       33.3       111.9       24       171.6       144.0       74       20.9       19.9       16.7       75       57.4       48.2       25       95.7       80.4       75       134.0       112.5       25       172.3       144.6       75       22.0       17.4       77       59.0       49.5       27       97.3       81.6       77       135.6       113.8       27       173.9       145.9       77       212.2       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       276       211.4       176.2       217.2       217.2       173.2       173.2       17	22							93.	1 78.4	72	131.	7 110,6	22	170.0	142.7	72	208.	174.8
25	23					9 46.9	23			11	132.	5 111.2	23	170.8	143.3	73	209,	175.5
16       19.9       16.7       76       58.2       48.9       126       96.5       81.0       176       134.8       113,1       126       173.1       145.3       276       211.4       177.       27       20,7       17.4       77       59 0       49.5       27       97.3       81.6       77       135.6       113.8       27       173.9       145.9       77       212.2       178.         29       22.2       18.6       79       60.5       50.8       29       98.8       82.9       79       137.1       115.1       29       175.4       147.2       79       213.7       179.2       213.7 <td></td> <td></td> <td></td> <td></td> <td>1-</td> <td></td> <td></td> <td></td> <td>1.4</td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td></td> <td></td>					1-				1.4	-						1		
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30 23.0 19.3 80 61.3 51.4 30 99.6 83.6 80 137.9 115.7 30 176.2 147.9 8.2 214.5 180.3 123.7 19.9 81 62.0 52.1 131 100.3 84.2 181 138.6 116.4 231 176.9 148.5 281 215.2 180.3 180.3 180.3 180.3 180.5 181.3 180.3 180.5 181.3 180.3 180.5 181.3 180.5 181.3 180.5 181.3 180.5 181.3 180.5 181.3 180.5 181.3 181.3 181.5 180.5 181.3 181.5 180.5 181.3 181.5 180.5 181.5 180.5 181.5 181.5 180.5 181.5 181.5 180.5 181.5 181.5 181.5 180.5 181.5 18				11						-11							212.	9 178,7
31 23.7 19 9 81 62.0 52.1 131 100.3 84.2 181 138.6 116.4 231 176.9 148.5 281 215.2 180. 32 24.5 20.6 82 62.8 52.7 32 101.1 84.9 82 139 4 117.0 32 177.7 149.1 82 216.0 181. 33 25.3 21.2 83 63.6 53.4 33 101.9 85.5 83 140.2 117.6 33 178.5 149.8 83 216.8 181 34 26.0 21.9 84 64.3 54.0 34 102.6 86.1 84 140.9 118.3 34 179.2 150.4 84 217.5 182. 35 26.8 22.5 85 65.1 54.6 35 103.4 86 8 85 141.7 118 9 35 180.0 151.1 85 218.3 183. 36 27.6 23.1 86 65.9 55.3 136 104.2 87.4 186 142.5 119 6 236 180.8 151.7 286 219.1 183. 38 29.1 24.4 83 67.4 56.6 38 105.7 88.7 88 144.0 120.5 38 182.3 153.0 88 220.6 185. 39 29.9 25.1 89 68.2 57.2 39 106.5 89.4 89 144.8 121.5 39 183.1 153.6 89 221.4 185. 40 30.6 25.7 90 68.9 57.9 40 107.2 90.0 90 145.5 122.1 40 183.8 154.3 90 222.1 186. 41 31.4 26.4 91 69.7 58.5 141 108.0 90.6 191 146.3 122.5 24.1 184.6 154.9 90 222.1 186. 41 31.4 26.4 91 69.7 58.5 141 108.0 90.6 191 146.3 122.5 24.1 184.6 154.9 291 222.9 187. 42 32.2 27.0 92 70.5 59.1 42 108.8 91.3 92 147.1 123.4 42 185.4 155.6 92 223.7 186. 43 32.9 27.6 93 71.2 59.8 43 109.5 91.9 93 147.8 124.1 43 186.1 156.2 93 224.4 188. 44 33.7 28.3 94 72.0 60.4 44 110.3 92.6 94 148.6 124.7 44 186.9 156.9 94 225.2 189. 45 34.5 28.9 95 72.8 61.1 45 111.1 93.2 95 149.4 125.4 45 187.7 157.5 95 226.0 189. 46 35.2 29.6 96 73.5 61.7 146 111.8 93.9 16.0 126.0 47 189.2 158.8 97 227.5 190. 48 36.8 30.8 98 75.1 63.0 48 113.4 95.1 98 150.7 127.3 48 190.0 159.4 98 228.3 191. 49 37.5 31.5 99 75.8 63.6 49 114.1 95.8 99 152.4 127.9 49 190.7 160.1 99 229.0 192. 50 38.3 32.1 100.76.6 64.3 150.1 14.9 96.4 100.1 15.9 128.6 250 191.5 160.7 100.9 229.8 192.			1	11 0		-1-	11	1 -								110		
32       24,5       20,6       82       62.8       52.7       32       101.1       84.9       82       139.4       117.0       32       177.7       149.1       82       216.0       181,         33       25.3       21.9       84       64.3       54.0       34       102.6       86.1       84       140.9       118.3       34       179.2       150.4       84       217.5       182.         35       26.8       22.5       85       65.1       54.6       35       103.4       86.8       85       141.7       118.9       35       180.6       151.1       85       218.3       183.         36       27.6       23.1       86       65.9       55.3       136       104.2       87.4       186       142.5       119.6       236       180.6       151.1       85       218.3       183.         37       28.3       23.8       66.6       55.9       37       104.9       88.1       87       143.2       120.2       37       181.5       152.4       87       219.8       184.4         38       29.1       24.4       88       67.4       56.6       38       105.7       88.1	_	-	-	-	-	-	-		_	-	3/			-		1		
33       25.3       21,2       83       63.6       53.4       33       101.9       85.5       83       140.2       117.6       33       178.5       149.8       84       217.5       182.         35       26.8       22.5       85       65.1       54.6       35       103.4       86.8       85       141.7       118.9       35       180.0       151.1       85       218.3       183.         36       27.6       23.1       86       65.9       55.3       136       104.2       87.4       186       142.5       119.6       236       180.8       151.7       286       219.1       183.         37       28.3       23.8       87       66.6       55.9       37       104.9       88.1       87       143.2       120.2       37       181.5       152.4       87       219.8       184.         38       29.1       24.4       88       67.4       56.6       38       105.7       88.7       88       144.0       120.5       38       182.3       153.0       38       221.4       185.         39       29.25.1       89       68.2       57.2       39       106.5       89.4 <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>11</td> <td>1</td> <td></td> <td>11 -</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>11 -</td> <td>17</td> <td></td>	1						11	1		11 -						11 -	17	
34       26.0       21.9       84       64.3       54.0       34       102.6       86.1       84       140.9       118.3       34       179.2       150.4       84       217.5       182.         35       26.8       22.5       85       65.1       54.6       35       103.4       86       85       141.7       118.9       35       180.0       151.1       85       218.3       183.         36       27.6       23.1       86       65.9       55.3       136       104.2       87.4       186       142.5       119.6       236       180.8       151.7       286       219.1       183.         37       28.3       23.8       66.6       55.9       37       104.9       88.1       87       143.2       120.2       37       181.5       152.4       87       219.8       184.4         39       29.0       25.1       89       68.2       57.2       39       106.5       89.4       89       144.8       121.5       39       183.1       153.6       89       221.4       185.4         40       30.6       25.7       90       68.9       57.9       40       107.2       90.0						113		1									216.	81,3
35       26.8       22.5       85       65.1       54.6       35       103.4       86 8       85       141,7       118 9       35       180.0       151.1       85       218.3       183.         36       27.6       23.1       86       65.9       55.3       136       104.2       87.4       186       142.5       119 6       236       180.8       151.7       286       219.1       183.         37       28.3       23.8       87       66.6       55.9       37       104.9       88.1       87       144.0       120.2       38       182.3       153.0       88       219.1       183.         39       29.9       25.11       89       68.2       57.2       39       106.5       89.4       89       144.8       121.5       39       183.1       153.6       89       221.4       185.         40       30.6       25.7       90       68.9       57.9       40       107.2       90.0       90       145.5       122.1       40       183.8       154.3       90       222.1       186.         41       31.4       26.4       91       69.7       58.5       141       108.0		- 0		1 0			- 11					1 2	11 -	1		1 0		
36       27.6       23.1       86       65.9       55.3       136       104.2       87.4       186       142.5       119       6       236       180.8       151.7       286       219.1       183.         37       28.3       23.8       87       66.6       55.9       37       104.9       88.1       87       143.2       120.2       37       181.5       152.4       87       219.8       184.         38       29.1       24.4       88       67.4       56.6       38       105.7       88.7       88       144.0       120.5       38       182.3       153.0       88       220.6       185.         39       29.2       25.1       89       68.2       57.2       39       106.5       89.4       89       144.8       121.5       39       183.1       153.0       88       220.6       185.         40       30.6       25.7       90       68.9       57.9       40       107.2       90.0       90       145.5       122.1       40       183.8       154.3       90       222.1       186.         41       31.4       26.4       91       69.7       58,5       141		1	-1		65.	1 54.	- 1		4 86	8 85	141,	7 118	11 -	1 0			218.	3 183.2
37       28.3       23.8       87       66.6       55.9       37       104.9       88,1       87       143.2       120.2       37       181.5       152.4       87       219.8       184.3         38       29.1       24.4       88       67.4       56.6       38       105.7       88.7       88       144.0       120.5       38       182.3       153.0       88       220.6       185.         39       29.9       25.1       89       68.2       57.2       39       106.5       89.4       89       144.8       121.5       39       183.1       153.6       89       221.4       185.         40       30.6       25.7       90       68.9       57.9       40       107.2       90.0       90       145.5       122.1       40       183.8       154.3       90       222.1       186.         41       31.4       26.4       91       69.7       58.5       141       108.0       90.6       191       146.3       122.8       241       184.6       154.9       291       222.1       186.         42       32.2       27.0       92       70.5       59.1       42       108.8			22.1	8	6 65.	9 55.	1 1 36		-		142.	5 110	6 21	180.	8 151.7	286		
38       29.1       24.4       88       67.4       56.6       38       105.7       88.7       88       144.0       120.5       38       182.3       153.0       88       220.6       185.         39       29.9       25.1       89       68.2       57.2       39       106.5       89.4       89       144.8       121.5       39       183.1       153.6       89       221.4       185.         40       30.6       25.7       90       68.9       57.9       40       107.2       90.0       90       145.5       122.1       40       183.8       154.3       90       222.1       186.         41       31.4       26.4       91       69.7       58.5       141       108.0       90.6       191       146.3       122.8       241       184.6       154.9       291       222.9       187.         42       32.2       27.0       92       70.5       59.1       42       108.8       91.3       92       147.1       123.4       42       185.4       155.6       92       223.7       187.         43       32.9       27.6       93       71.2       59.8       43       109.5		1				- 33		104.	9 88,	1 87	143.	2 120.	2 3	181.	5 152.4	87	12.	8 184
39       29.9       25.1       89       68.2       57.2       39       106,5       89.4       89       144.8       121.5       39       183.1       153,6       89       221.4       185.         40       30.6       25.7       90       68.9       57.9       40       107.2       90.0       90       145.5       122.1       40       183.8       154.3       90       222.1       186.         41       31.4       26.4       91       69.7       58,5       141       108.0       90.6       191       146.3       122.8       241       184.6       154.9       291       222.1       186.         42       32.2       27.0       92       70.5       59.1       42       108.8       91.3       92       147.1       123.4       42       185.4       155.6       92       223.7       187.         43       32.9       27.6       93       71.2       59.8       43       109.5       91.9       93       147.8       124.1       43       186.1       156.2       93       224.4       188.4       196.9       156.9       94       225.2       189.       225.2       189.       44.8       18	38			8	8 67.	4 56.	5 38	105.	7 88.	7 88	144.	O 120.	3	182.	3 153.0	88	210.	6 185.1
40 30.6 25.7 90 68.9 57.9 40 107.2 90.0 90 145.5 122.1 40 183.8 154.3 90 222.1 186.  41 31.4 26.4 91 69.7 58,5 141 108.0 90.6 191 146.3 122.8 241 184.6 154.9 291 222.9 187.  42 32.2 27,0 92 70.5 59.1 42 108.8 91.3 92 147.1 123.4 42 185.4 155.6 92 223.7 187.  43 32.9 27.6 93 71.2 59.8 43 109.5 91.9 93 147.8 124.1 43 186.1 156.2 93 224.4 188.  44 33.7 28.3 94 72.0 60.4 44 110.3 92.6 94 148.6 124.7 44 186.9 156.9 94 225.2 189.  45 34.5 28.9 95 72.8 61.1 45 111.1 93.2 95 149.4 125.4 45 187.7 157.5 95 226.0 189.  46 35.2 29.6 96 73.5 61.7 146 111.8 93.9 196 150.1 126.0 246 188.4 158.1 296 226.7 190.  47 36.0 30.2 97 74.3 62.4 47 112.6 94.5 97 150.9 126.6 47 189.2 158.8 97 227.5 190.  48 36.8 30.8 98 75.1 63.0 48 113.4 95.1 98 151.7 127.3 48 190.0 159.4 98 228.3 191.  49 37.5 31.5 99 75.8 63.6 49 114.1 95.8 99 152.4 127.9 49 190.7 160.1 99 229.0 192.5 193.3 229.8 192.	39	29.	25.1	8	68.	2 57.	2 39	106,	5 89.	4 89	144.	8 121.	5 3	9 183.	1 153,6	89	221.	4 185.8
41 31.4 26.4 91 69.7 58,5 141 108.0 90.6 191 146.3 122.8 241 184.6 154.9 291 222.9 187. 42 32.2 27,0 92 70.5 59.1 42 108.8 91.3 92 147.1 123.4 42 185.4 155.6 92 223.7 187. 43 32.9 27.6 93 71.2 59.8 43 109.5 91.9 93 147.8 124.1 43 186.1 156.2 93 224.4 188. 44 33.7 28.3 94 72.0 60.4 44 110.3 92.6 94 148.6 124.7 44 186.9 156.9 94 225.2 189. 45 34.5 28.9 95 72.8 61.1 45 111.1 93.2 95 149.4 125.4 45 187.7 157.5 95 226.0 189. 46 35.2 29.6 96 73.5 61.7 146 111.8 93.9 196 150.1 126.0 246 188.4 158.1 296 226.7 190. 47 36.0 30.2 97 74.3 62.4 47 112.6 94.5 97 150.9 126.6 47 189.2 158.8 97 227.5 190. 48 36.8 30.8 98 75.1 63.0 48 113.4 95.1 98 151.7 127.3 48 190.0 159.4 98 228.3 191. 49 37.5 31.5 99 75.8 63.6 49 114.1 95.8 99 152.4 127.9 49 190.7 160.1 99 229.0 192.5 193.3 32.1 100 76.6 64.3 150 114.9 96.4 200 153.2 128.6 250 191.5 160.7 100 229.8 192.	40	30.	25.7	90	08.	9 57-	40	107.	2 90.	90	145.	5 122.				90	222.	
42       32.2       27,0       92       70.5       59.1       42       108.8       91.3       92       147.1       123.4       42       185.4       155.6       92       223.7       187.         43       32.9       27.6       93       71.2       59.8       43       109.5       91.9       93       147.8       124.1       43       186.1       156.2       93       224.4       188.         44       33.7       28.3       94       72.0       60.4       44       110.3       92.6       94       148.6       124.7       44       186.9       156.9       94       225.2       189.         45       34.5       28.9       95       72.8       61.1       45       111.1       93.2       95       149.4       125.4       45       187.7       157.5       95       226.0       189.         46       35.2       29.6       96       73.5       61.7       146       111.8       93.9       196.1       126.0       246       188.4       158.1       296       226.7       190.         47       36.0       30.2       97       74.3       62.4       47       112.6       94.5			26.4	9	1 69.	7 58,	141						24	184.	6 154 9	291	222.	9 187.1
44       33.7       28.3       94       72.0       60.4       44       110.3       92.6       94       148.6       124.7       44       186.9       156.9       94       225.2       189.         45       34.5       28.9       95       72.8       61.1       45       111.1       93.2       95       149.4       125.4       45       187.7       157.5       95       226.0       189.         46       35.2       29.6       96       73.5       61.7       146       111.8       93.9       196       150.1       126.0       246       188.4       158.1       296       226.0       189.         47       36.0       30.2       97       74.3       62.4       47       112.6       94.5       97       150.9       126.6       47       189.2       158.8       97       227.5       190.         48       36.8       30.8       98       75.1       63.0       48       113.4       95.1       98       151.7       127.3       48       190.0       159.4       98       228.3       191.         49       37.5       31.5       99       75.8       63.6       49       114.1		32.	2 27,0	92				108.	8 91.	3 92	147.	1 123.	4 4	185.	4 155.6	92	223.	7 187.7
45     34.5     28.9     95     72.8     61.1     45     111.1     93.2     95     149.4     125.4     45     187.7     157.5     95     226.0     189.       46     35.2     29.6     96     73.5     61.7     146     111.8     93.9     196     150.1     126.0     246     188.4     158.1     296     226.7     190.       47     36.0     30.2     97     74.3     62.4     47     112.6     94.5     97     150.9     126.6     47     189.2     158.8     97     227.5     190.       48     36.8     30.8     98     75.1     63.0     48     113.4     95.1     98     151.7     127.3     48     190.0     159.4     98     228.3     191.       49     37.5     31.5     99     75.8     63.6     49     114.1     95.8     99     152.4     127.9     49     190.7     160.1     99     229.6     192.5       50     38,3     32.1     100     76.6     64,3     150     114.9     96.4     200     153.2     128,6     250     191.5     160.7     300     229.8     192.5		32.	27.6	9:														
46 35.2 29.6 96 73.5 61.7 146 111.8 93.9 196 150.1 126.0 246 188.4 158.1 296 226 7 190 47 36.0 30.2 97 74.3 62.4 47 112.6 94.5 97 150.9 126.6 47 189.2 158.8 97 227.5 190. 48 36.8 30.8 98 75.1 63.0 48 113.4 95.1 98 151.7 127.3 48 190.0 159.4 98 228.3 191. 49 37.5 31.5 99 75.8 63.6 49 114.1 95.8 99 152.4 127.9 49 190.7 160.1 99 229.6 192. 50 38,3 32.1 100 76.6 64,3 150 114.9 96.4 200 153 2 128,6 250 191.5 160,7 300 229.8 192.			28.3	94	72,	0 60.4	44	110.					4	180,	9 150.	94		
47 36.0 30.2 97 74.3 62.4 47 112,6 94.5 97 150.9 120.0 47 189.2 158.8 97 227.5 190.  48 36.8 30.8 98 75.1 63.0 48 113.4 95.1 98 151.7 127.3 48 190.0 159.4 98 228.3 191.  49 37.5 31.5 99 75.8 63.6 49 114.1 95.8 99 152.4 127.9 49 190.7 160.1 99 229.0 192.  50 38,3 32.1 100 76.6 64,3 150 114.9 96.4 200 153 2 128,6 250 191.5 160,7 300 229.8 192.									-	-	_							_
48 36.8 30.8 98 75.1 63.0 48 113.4 95.1 98 151.7 127.3 48 190 0 159.4 98 228.3 191. 49 37.5 31.5 99 75.8 63.6 49 114.1 95.8 99 152.4 127.9 49 190.7 160.1 99 229.0 192. 50 38.3 32.1 100 76.6 64.3 150 114.9 96.4 200 153 2 128.6 250 191.5 160.7 300 229.8 192.			29.6	96	73.	5 61.7	146	111.	8 93	9 196							226	7 190.
49 37.5 31.5 99 75.8 63.6 49 114.1 95.8 99 152.4 127.9 49 190.7 160.1 99 229.0 192, 50 38,3 32.1 100 76.6 64,3 150 114.9 96.4 200 153 2 128,6 250 191.5 160,7 300 229.8 192																	227.	5 190.
50   38,3   32.1   100   76.6   64,3   150   114.9   96.4   200   153 2   128,6   250   191.5   160,7   100   229.8   192					75.	8 62 6	40	113.	195	8 90	151.	4 127					228.	3 191.6
Diff Den Las Dift Den Las		38.3	32.1	100	76.	6 64.2	150	114	95	4 200	152	2 128	6 250					8 702
[ ] [ ] [ ] [ ] [ ] [ ] [ ] [ ] [ ] [ ]			-	D:0	D	Total	D:#	Des	1	Di	Den	Ta	10		_	-		
	-			1.711	. D-1	L	Dill	Det	IDai	IDI	in Dep	La:	IIDI		p. Lat	1/21	n De	Lat

for 50 Deg.

# Difference of Latitude and Departure for 41 Deg. 41

Dett	II at l	Deul	Dia	II at	Dep	Die	Lat	Den	Di	I Tat	Dep	nDia	Lat	Dep	MDift.	Lat	Den
Din	_	-	-	-	-		_	and region in	-	-		-		-	-		
1	00.8		51		33.5	101		66.3	151	114.0	1 1	03	151.7	131.8		189 4	
2		01.3		39.2	- 41	02		67,6	52	114.7	100.4	03		133.2	52	190,2	
3	03.0			40.8		04		68 2	54	116.2		04	1	133.8	54	191.7	
4	03.8	200	55			05		68.9	55	117.0		05		134.5	55	193.5	
5		_	-	-		106	-	69.5	156	117.7		206	-	135.1	256	1932	-
6	04.5			43.0		07.	80.8	70.2	57		103.0	07		135.8	57	194.0	
7 8	06.0			43.8		08		70.8		119.2		08		136.4		194 7	
	06.8			44 5		09		71.5		120.0		09	157.7	1	59	195.5	
	07.5		1	45.3		10		72.2	60		1050	10		137.7	60	196.2	170 9
-	08.3			46.0	_	111	-	72.8	161	121.5	-	211	The state of	138.4	261	197.0	171.2
12	09.1			46.8		12		73.5	62	122.3		12	160.0		62	197.7	
	09.8			47.5		13	85.3		63	123.0		13	160.8		63	198.5	172.5
14	10.6			48.3		14	86.0	74,8		123.8	107.6	14	161.5	140;4	64	199.2	
15	11.3	09.8		49.1		15	86.8	75.4	65	124.5	108.2	15	162.3	141.0	65	200.0	173 8
16	12.1	10,5	66	49,8	43.3	116	87.5	76.1	166	125 3	108.9	216	163.0	141 7	266	200 8	174,5
17	12.8			50,6		17	88.3	76.7		126.0		17	163.8	142.3	67	201 5	
18	13.6	11.8		51.3		18	89 1	77.4		126.8		18		143.0	68	202,3	175.8
19	14.3	12.5	69	52.1	45.3	19	89.8		69	127.5		19	165.3		69	203.0	
20	15.1	13.1	70	52.8	45,9	20	90.6	78,7	70	128.3	111.5	20	166.0		70	203.8	177.1
21	15.8	13.8	71	53.6	46.6	121	91.3	79.4	171	129.1	112,2	221	166,8	145,0	271	204.5	177.8
22	16.6	14.4		54.3		22		80.0	, -	129 8	112.8	22	167.5		72	205 3	
23	17.4		73	55.1	47.9	23	92.8			130.6		23	168.5		73	206.0	
24		15.7		55.8		24	93.6			131.3		24	169.1	146.9	74	206.8	
25	18.9	16.4	7.5	56.6	49.2	25	-	82 0	_	132.1		25	169.8		75	207,5	_
26	19.6	17.1	76	57.4	49.9	126	95.1	82.6		132.8		226		148.2	276	208.3	
	20.4		77	58.1	50.5	27	95.8			133.6		27	171.3		77	209,1	
1	21.1			58.9		28		84.0		134.3		28	172.1		78	209 8	
29	21.9			59,6		29	97.4		79	135.1	117.4	30	173.6		79	211.3	
-	22.6	19.7		60.4	-	30	98.1		-			_		-	281		-
31	23.4		81	61.1	53.1	131	98.9			136.6		231	174.3		82	212 1 212.8	
	24.2		82	61.9	53,8	32	99.6			137,4		32	175 8		83	213.6	-
7.70	24.9	2. 3		63.4		33	101.1			138.9		34	176.6		84	214.3	
-	25.7 26.4			64.2		34	101.9			139.6		35	177.4		85	215,1	
_	-					_	102.6	_	-	140.4		_	178.1		286	215.8	-
	27.2			64,9 65.7		37	103.4			141.1			178.9			216,6	P
37	27.9 28.7	24.3		66,4			104.2		88	141.9	122.2	38	179.6	156.1	88	217.4	188.9
30	20.4	25.6		67.2	58.4	30	104.9	91.2	80	142.6	124.0	39	180.4	156.8	89	218.1	189.6
		26.2		67.9			105.7			143.4		40	181.1	157.4	90	218.9	
		-		68,7		_	106.4		_		125.3			158.1		219.6	190.0
		27.6		69.4			107.2				125.9		182.6			220,4	
43	32.5	28.2	93	70.2	61:0		107.9		93	145.7	126.6	43	183.4	159.4	93	221.1	192.2
44	33.2	28.9		70.9	61:7		108.7		94	146,4	127.3			160.0	94	221.9	192.8
45		29.5		71.7		45	109.4		95	147.2	127.9	45	184,9	160.7	95	222.6	193.5
46.		30.2		_			110.2		196	147.9	_			161.4		223.4	194.2
47	35.5	30.8	97	73.2	63.6		110.9			148.7	129.2	47	186.4	162.0	97	224.2	
48	10000	31.5	98	74.0	64.3		111.7				129.9			162.7	98	224.9	
49		32.1	99	74.7	64.9	49	112.5	97,7	99	150.2	130.5	49	187.9	163.3	99	225.7	
50		32.8		75,5	65.6		113.2	98.4	200	150.9	131,2	250		164,0	-	226.4	_
		Lat			Lat	-	In	1 -4	10:0	D	Lat	IID;	Dep	1 T	ID:A	Dan	Lat

for 49 Deg.

# 42 Difference of Latitude and Departure for 42 Deg.

De	11.21	De	Diff	Lat	Det	(D) (I)	Lat	Dep [	Diff	Lat	Den /	Dift	Lat	Dep	Dift	Lat	Den
-	-	-	-	-		-		67,6	-				-	_	251	186,5	-
2		01.3	51	37·9 38.6	34.1	02	75 ° 75 8	68.21	- 1	112.2			149.3	134.5	52	187.2	168.6
3		02.0		39.4		03	76.5	68.9		113 7	102.4		150 8		53	187.9	
4	03.0	2.7	54		36.1	04	77.3	69.6	54	114 4	103.0	04	151.5	136.5	54	188.7	
5	23.7	03.3	55	40.9	36.8	05	78.0	70.2		115.1	103.7	05	152.3	137.1	55.	189 4	170 6
6	04.5	04.0	56	+16		106	78.7	70.9	156	115.9	104.4	206	153.0	137.8	256	190,2	
7	05 2		57	42,3	38.1	07	79.5	71.6	2,	116.6		07	153.8		57	190.9	
8	1 :	35.4	58	0	38.8	08	80,2 81.c	72.3	1 - 1	2 1	106.4		154.5		58	191.7	173.3
9	00.7	06.0	59	44 6	39.5	10	81.7	73.6	221	118.9		10	156,0		60	193.1	173.9
11	08.2	-	61	45.3	40.8	111	82.5	74.3	_	119.6	_	211	156.7	_	261		174,6
12		08.0	11	46 1	41.5	12	83.2	74.9		120.3		12	157.5		62	6	175.3
13		08.7		46.8		13	839	75.6	63	121,1	SOME A SECURITY	13	158.2		63	195.4	175.9
14	1	09.4	64	47.5		14	84.7	76.3	64	121.8	109.7	14	159.0		64		176.6
15	11 1	10,0	-	18.3	43.5	15	85.4	76 9	65	122.6	1104	15		143 8	65		177.3
16		10.7	1 -		44.2	116	86.2	77.6	166	123.3	100 000	216	160.5	144.5	266	197.6	177.9
17	100	11.4			44,8	17	86.9 87.7	78.3	40	124.1	12 C 1 2	17	161.2		68		178.6
18		12.0	11 /		45.5		88.4	78,9	69	125.5		19		146.5	69		180.0
19		13.4	11		46.8	20	89 1	80.3	70	126.3	10 1 Tan 1	20		147.2	70	200.6	4
21	-	6 14.0	-	-		121	89.9		171	127.0	114.4	221	_	147.8	271	201.3	181.3
122		3 14,7	11		48.2		90.6		72		115.1	22		148.5	72		182.0
23	17.	1 15 4	73	54.2	48.8	23	91.4	82 3	73	128.5	115.7	23		149.2	73		182.6
24		8 16.1	11		49.5	24	92.1	83.0		129 3		24		149.9	74		183.3
25	-	6 16.7	7.5	-	-	-	92.9			130.0	117.1	25		150.5	75	_	184.0
26			. 11	1 .	1 -	126	93.6		176	130.7		226		151.2	276		184.6
27		1 18.1			51.5	27	94.3	85.6			118.4	27		151.9	77		185.3
28		5 19.4	11		52.9		95.1				119.1	29		152.5	79		186,6
30		3 20.1	11 0		53,5		96.6			133.7		11	1 2 2 2 4 10 4	153.9	80	208.0	187.3
31		20.	-	-	54.2	_	97.3	-			121.1	231		154.5	281		188.0
32		8 21.4			54.9		98.1				121.8			155,2	82	209.5	188.7
33		5 22.1	11 0	61.7	55.5	33	98.8				122.4			155.9	83		189.3
34	1 2	3 22.7			56.2		99.5				123.1			156.5	84		190.0
35		0 23.4		-	56.9		100.3	-	85		123.8			157.2	85	-	190.7
36		7 24.		1.3.		136	101.0		11		124.4	11.7	175.3	157.9	286 87		191.3
37	27.	5 24.	8	65	58.9	37	101.8				125.8	37	176.8	159.2			192.7
39		0 26.	1 80	66.	59.	30	103.		80	140.4	126.4	39	177.5	159.9	89		193.3
40		7 26,		66.	60.2	40	104.0				127.1	40	178.3	160.6	90	215.4	194.0
41	_	5 27.	-	_	6 60.0	-	104.7				127.8		179.0	161.2	291	216,2	194.7
42	2 31,	2 28.	1 9		3 61.	42	105.	95.0	92	142.6	128.4	42	179.8	161 9	93	216,	195.3
4:	3 31.	9 28.	8 9	3 69.	1 62.2	43	106.2	95.7	93	143.4	129.1	43	180.5	162.6	93		196.0
44		7 29.		4 69.	8 62	44					129.8			163.2	94		1 196.7
4.		4 30.	- 1		6 63.				-		130.						197.4
40		2 30.	8 9		3 64.		108.		196	145.	131,	240	182.7	164.6	296		198.0
47	34.	9 31.	4 9	8 72.	8 65.	6 47	109.	98.3	97	147	1 122.	48	184.2	165.9	98	221.	199.4
49	36	4 304	21 0	0 72.	5 66.	2 40	110.	7 99.7	1 99	147	8 133.	1 49	185,0	166.6	99	222.	200.0
1 5		139		0 74.	3 66	9 150	III	4 100.4	200	148.	6 133.	8 250	185.7	167.2	300	222.	200.7
				ft De	p La	Di	t Dep	Lat	Dif	Dep	La	Dil	Dep	Lat	Diff	Dep	Lat
-	1	1-4	11-		11-	11			11			4	•		11		

for 48 Deg.

# Difference of Latitude and Departure for 43 Digs. 43

	T	Des	arria	Lat	Dent	D.A.	Laul	Den I	Ditti	Lat	Den l	Det	Lat	Deo II	Dift,	Lat	De	-13
Dill	Lat	Deb	-	-		-	Lau	-	_		-	-			-	-	-	
1		00.7		37.3	34.8	101	73.9	68.9		110.4			147.0	- 11		183.E		
		01.4	11	38.0	35.5	02	74 6	69,5	3-1	111.2	103 0		148.5	2, 11		185.C		
3	N 27 . C	02.7	11 -3		36.8	03	75.3	70.9	53	112.6		-		139.1		185 €		
1 4	03 7		54	40.2		05	76.8	71.6		113.4	105 7			139.8		186.5		
5		-	56	41.0	-	106	77.5	72,3	156	114.1	-	-	150.7	140.5	-	187.2	-	-
6	04.4	. 0		41.7	0	07	78.3	73.0	57	114.8				141.2		187.9		
8		05.5		42.4	7	08	79.0	73.6	58	115.6				141.8	58	188.7	175	.9
9		06.2			40.2	09	797	74.3	59	116.3	108.4		152.9		59	189.4	176	.6
10	07.3	06.8	60	43.9	40.9	10	80.4	75.0	60	1170	109.1	10	153.6	143.2	60	190.1	177	.3
111	08.0		1	44.6	41.6	111	81.2	75.7	161	117.7	109.8	211	154.3	143.9		190.9		
12		08.2	62	45.3	1	12	81.9	.76.4	62	118.5	110.5	11		144.5		191.6		
13	09.	08.9		46.1		13	82.6	77.1	63	119.2			1558			192.3		
14		109.5		46.8		14	83.4	77.7	64		111.8		155.5			193.1		
15	11.0	10.2	-		44.3	15	84.1	784	65	120.7	112.5	-	157.2	-	-		-	-
16	11.	10.9			45.0	116	84.8	79.1	166	121.4	1132	11	158.0	147.3		194.5		
17	100	111.0		49.0		17	85.6	79.8		122.1	113.9			148.6		195.3		
18		12.			46.4	18	86,3 87.0	80.5	11-6-	122.9		1		149.3		196.7		
19	14.	6 13.6	- 11.		47.1	19	87.8	81.8		124.3	1	11		150.0		197.5		
20	-	-	-	-	48.4	-	88.5	82.5	-	125.1	1-	221	161.6	150.7		198.2	-	
21	16.	4 3 3 3	- 11		49.1	121	89.2	83.2			117.3			151,4		198.9	1	
22		8 15.			49.8		90.0	83.0	11	1	1 0			152,1		199.7		
24	1		1		50.5		90.7	84.			118.6	24	163.8		74	200.4		
25	1 0			100			91.4	85.2		128.0	119.	25	164.6	153.4	75	201.1	187	7.5
26		0 17.	7 7	5 55,	51.8	126	92.1	85.0	176	128.7	120.0	226	165.3	154.1		201.		
27		7 18.			3 52.5		92.9	86.	77		120.			154.8				-
28	20.	5 19.	1 7		53 2		93.6				121.	11	1 -	155.5	11	203,		
29		2 19.			8 53.9		94.3	88.0	11 -	-	12.2.			156.2		204.	0	
30	21.	9 20.	-		-	-	95.1	88.	-11-	-	122,	-11-	_			-	-	-
31				130	1	-	95.8		- 11 0	-	4 123.			157.5		205.	5 19	1.0
32					0 55.				11 0		1 124.			158.9		207.		
33		1000	-11 -	- 1 -	7 56.0		-0		11 0		6 125.		171.1		. 0			1
34		9 23	11		2 58.				11 0		3 126.			1	11 0 -			
35			-   -		9 58.	-	_	-	-	-	-	8 236	172.	160.9	286	209.		5.0
36		3 24	2	7 62	6 59.			1 .	1 0		8 127.		1	3 161.6	87	209.	9 19	5.7
37		.8 25		8 64	4 60.	38		94.	1 8	8 137.	5 128.	2 3	174.	1 162.3	88	210.	6 19	6.4
39	28	.5 26	6 8	9 65	1 60.	7 39			8 8	9 138.	2 128			8 163.0	89	211.	4 19	7.1
40		.3 27		0 65	8 61.	4 40	102.	95	5 9	0 139.	0 129		_	5 163.6	-	212.		
4		.0 28	.0 9		6 62.	1 14	1 103.	96.			7 130			3 164.		212.		
4	2 30	.7 28	.6 9	2 67	.3 62.	7 42	103.	9 96		2 140	4 130	.9 4	2 177.	0 165,0		2 213		
4	3 31	.4 29	.3 9		0 63.		104.	6 97	5 9	3 141.	1 131		3 177.	7 165.	7 9	3 214		
4		.2 30		4 68	.7 64.	1 4		3 98		4 141.	6 132	.0 4	5 170.	4 166.	1 9	4 215		
4	_	.9 30			.5 64.				_		6 133						_	
4	6 33	.6 31		6 70	.2 65.	5 14	6 106.		.5 19		3 133	.6 24		9 167.		7 217		
4		1.4 32	.1	7 79	.9 66.	2 4	7 107,	2 100	9	7 144	.1 134	0 4		4 169,		8 218		
4		5.8 3	7		.7 66	8 4		0 101	6 6		.5 135			1 169.		9 218		
5	0 3	6.6 3	1.1	99 72	.1 68	2 15	0 109		.3 20	146	.3 136			.8 170.	5 30	219		
		ep L	31 5	18 D	en La		A Dep			ift De		t Di	A De			it De		
1.	INI	chir	at IL	III D	ch Ta	. 110	it ibe	- 134	112			-					-	-

for 47 Deges.

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	En C		18			20.			-								
Dut	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep	Dia	Lat	Dep	Diff	Lat	Dep
1	00,7	00,7	51	36.7	35.4	101	92,6	70.2	151	108.6	104.9	201	144.6	139.6	251	180.5	174,
2	01.4	01,4	52		36.1	02	73.4	70.8	52	109.3	105.6	02	145.3	140.3	52	181.3	175.
3	02.2	02.1	53	38.1		03	74.1	71.5	53	110.1	106.3	03	146.0	141.0	53	182.c	175.
4	02.9	02.8	54	38.8		04	74.8	72.2	54	110.8	107.0	04	146.7	141.7	54	182.7	
5	03.6	03.5	55	39.6	38.2	05	75.5	72.9	55	111.5	107.7	05	147.5	142.4	55	183.4	177.
6	04.3	04,2	56	40.3	38.9	106	76.2	73.6	156	112.2	108.4	206	148.2	143.1	256	184.1	177.
7		04,9	57		39.6	07	77.0	74.3	57	112.9	109.1	07	148.9	143.8	57	184.9	
8		05.6	58	1 7 6	40.3	08	77.7	75.0	58	113.6	109,7	08	149.6	144,5	58	185.6	
9		06.3	59	42.4	41.0	09	78.4	75.7	59	114.4	110,4	09	150.3	145.2	59	186 3	179.
10	07.2	06.9	60	43.2	41.7	10	79.1	76.4	60	115.1	111.1	10	151.1	145.9	60	187.0	180,
11	07.0	07.6	61	42.0	42.4	111	79,8	77.1	161	115.8	111,8	211	151.8	146.6	261	187.7	181
12		08,3	62	1	43.1	12	80,6		62	116.5		12		147.3	62	188.	
13		09.0	63		0	13	81.3		63		113.2	13	-	147.9	63	189.2	
14		09.7	64	46.0		14	82.0		64	118.0	113,9	14	153.9	0 2	64	189 9	
15	10.8	10.4	65	46.8	45.1	115	82,7		65	118.7	114.6	15	154.6		65	1900	
16	11.5	11.1	66	47.	- 0	116	83.4	-		119.4	115,3	216	155.4		266	191.3	184
17	12.2	1 0	11	1			84.2		67	120.1	1 2			150.7	67	192.1	
18	1000	12.5	1 00		47.2		84.0				116.7			151.4	68	192.8	
19	13.		11 0			11	85.6		69	1 4	117,4	11	-	152.1	69	193.5	
20	14.4	-	11		1.00	11	86.				118.1	20	1 0		70	1942	
-	-	-	11	-	-	-	-	-		-	118.8	1221	-	_	1		-
21	15.8		11	2000			87.8				The Park State of the Control of the	11		153,5	72	194 9	100
22	16.		11				1.00				119.5	11	33.	154.2	11	1	
23	1		11			11 -	89.2		11		10000	11	161.1		11	196.4	4 -
24	17.		11 -		1		89.5		74		121.6	11		155.6	75	197.1	
25	_					-		-		-	-	-	-	-	1 -6	_	1-
26		7 18.1				11	1			1	30			1-21	11	198.5	
27	1	4 18.8					1			-		1	100	157,7	77	199.2	
28	1000	1 19.4	1			11 -	1. 7 -				123.6	11 2 2 2 2		158.4	78	200.0	
29		9 20,1		75							8 124.	11		1 22	79	200.7	
30	21.	6 20,8		-13/	-	-	_			-		11-	-		1	201.4	1-24
31	22.	3 21.	111	13		,	1 6 7 7	91.0							181		
32		0 22.2			0 57.0	11			82						82	202.8	195
33	23.	7 22.	8:	59.		19 / 10			1 0		1	11 33	1 40	161.8	11 0	203.6	196
34			11 0	100	.12							11 -		162.5		204.	1
35	25.	2 24.	1	-	1 59.0	35	-		85	133.	1 128,	35	109.0	163.2	85	205.0	198
36		9 25.0			2 32-1				186	133,	8 129.2	2 36		163.9		205.	
37	26.	6 25.	8	62.	6 60.4	37	98.	95.2	87	134.	5 129.	37	170.	164.6	87	206.4	1199
38		3 26.		63.	3 61.			95.9	88	135.	2 130.	38		165.3	88	207.2	2 200
39		1 275			0 61,		100.	96.		135.	9 131.	39	171.9	166.0	89	207,	200
40	28.	8 27.1	30	64.	7 62.	40	100.	97.2	90	130.	7 132,0	40	172.0	166.7	90	208.	201
41		5 28.	9	65.	5 63.2	141	101.	97.9	191	137,	4 132.	241	173-4	167.4	291	209.	3 202
42		2 29		66.	2 63.9	42	102.	98.6	92	138.	1 133.4	42	174-1	168.1	92	210.0	
43		9 29.	9:	66.	9 64.6	43	102.	99.	93	138.	8 134.	43	174.8	168.8	93	210.	8 203
44	31.	6 30.6	94	67.	6 65.3	44	103.6	100.0	94	139.	5 134.	44	175.	169.5	94		
45	32.	131.		68.	3 66.0	45	104.	100.7	95	140.	3 135,4	45	176.2	170.2	95	212,	
46		32.0	100	60.	1 66.7	146	105.0	101.4	196	141.	0 136.	-		170.9			-
47		32.6	97	60.5	8 67.4	47	105.7	102.1	97	141.	7 136.8	47		171.6			
48	34	33.3	98	70.	5 68.1	48	106,	102.8	98	142.	1 37.5	48	178.	17213	98		
49		34.0	99	71.2	68.8	49	107.2	103.6	99	143.	138.2	49	179.1	173.0	99		
50	36.0	33 7	100	71.0	69.5	150	107.0	104.2	200	143.0	138.0	250		173.6		215.	
Dif		La	0:0	D	Lat	Dia	Den	Ter	Die	Den	Lat	Die		Lat	Dil		-
211	40	177	11	Del	Lat	111	. Deli	Lat	ווכון	ch	Lat	1	- 20	J. Lat	Di	t De	1 -

		3.7													-	,	כד
DI	Lan	Dep	Dif	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat.	Dep	Dift	Lat	Dep
1	00.7	00,7	51	36.1	36.1	101	71.4	71.4	151	106.8	106.8	201	142.1	142.1	251	177.5	177.5
2	01.4	01.4	52		36.8	02	72.1	72.1	52	107,5	107.5	02	142.8	142.8	52	178.2	178,2
3	02.1		53	37.5	37.5	03	72.8	72.8	53	0.000	108.2	03	143.5	143.5	53	178.9	178.9
4	02.8	10.0		38.2	38.9	04	73.5	73.5		109.6	108.9	04	144.2	144.2		179.6	26
-51	03.5	03.5	55		-	_	74.2	74.2	55	-	_	05	144.9	144 9	55	180.3	188.3
7 31		04.2	56	39.6	39.6	106	74.9	74 9	156	110.3	110.3	206	145.7	145.7	256	181 0	181.5
21	04.9	05.7	57 58	41.0	40.3	07	75.7	75.7	57	111.0	111.0	08	146.4	147.1	57	181.7	181.7
2	2		59	41,7	41.7	09	77.1	77.1	59	112.4	112.4	09		147.8	59	183.1	182.4
10	07.1	07.1	60	42.4	42.4	10	77.8	77.8	60	113.1	113.1	10	148.5	148.5	60	183.8	183.8
11	07.8	07.8	61	43.1	43.1	111	78.5	78.5	161	113.8	113.8	211	149.2	149.2	261	184 5	184.5
12	08.5	08.5	62	43.8		12	79.2	79.2	62	114.5	114 5	12	149.9	149.9	11	185.3	185.2
13	09 2	09,2	-	44.5	44.5	13	79.9	79.9	63	115.3	115 3	13	150.6	150.6	63	185,0	186.0
14	09.9		64	45.3	45.3	14	80.6	80.6	64	116,0		14		151.3	64	186.7	186.7
15	10,6	-	-	40.0		15	81.3	81.3	05	116.7	116.7	15	152.0	152.0	65	187.4	187.4
16	11.3	11.3	66	46.7		116	82.0	82.0	166	117.4		216	1 52.7	152.7	266	188.1	188.1
17		12.0	68	47.4	47.4	17	82.7	82.7	67	118.1	118.1	17	153.4	153.4	67	188.8	
18	13.4	12.7	69	48,8		10	84.1	83.4	68	119.5	118.8	18	154.1	154.1	11 -	189.5	
19	14.1	14.1	70	49,5	49.5	20	348	84,8	70	120.2	120.2	19	154.8		11 -	190.2	
21	14.8	14,8	71	50 2	50.2	121	85.6	85.6	-	120.9			-33	33		190.9	
22	15.6		72	50.9	-	22	86.3	86 3	72	121,6		221	156.3	156.3	11	191.6	191.6
23	16.3	-	73	51.6	51.6	23	87.0		73	122.3		23	-	157.7	73	192.3	192.3
24	17.0	17.0	74	52.3	52.3	24	87.7	87.7	74	211	1230	24	158.4		74	193.7	193.7
25	17.7	17.7	75	53.0	53.0	25	88,4	88.4	75	123,7	123.7	25	159.1	159.1	75	194 4	194.4
26	18.4	18 4	76	53.7	53.7	126	89,1	89.1	176	124.4	124.4	226	159.8	159.8	276	195 2	195.2
27		19,1	77		54.4	27	89.8	89,8	77	125.2	125,2	27	160.5	160.5	77	195.9	195.9
28	19.8	1 TO 12 CO.	78	55,2	55.2	28	90.5	90.5	78	125.9			-	161.2		196.6	
30		20.5	79	55.9	55.9	29	91.2	91.2	79	120.0	100000	29		161.9	11 0	197.3	
-	-	-	81	-	-	30	91.9	91.9	80	127.3		30	162.6	_	-	-	198.0
31	2	21.9	82	57.3	57∙3 58.€	131	92.6	92.6	181	128.0				163 3	281	198.7	198.7
33	10.00	1.00	83	58.7	58.7	32	93.3	93,3	82	129.4		32	-	164.0	11	199.4	
34	24.0		84	59.4	59.4	34	94.7	94.7	84	130.1	130.1	34	165.5			200.8	200.8
35	24.7	24,7	85	60.1	12.	35	95.5	95.5	85	130.8		35	166.2	1 44	85	201.5	201.5
36	25.5	25.5	86	60.8	60.8	<b>136</b>	96.2	96.2	186	131.5	131.5	236	166.9	166,0	286	202.2	20212
37	26,2			61.5		37	96.9	96.9	87	132.2	132,2	37	167.6	167.6	87	202.9	202.0
		26.9	88	62.2	62.2		97,6	97.9	88	132.9	132.9	38	168.3	168.3	88	203.6	203.6
		27.6	89	62.9	62.9	39	98.3	98.3	89	133.6	133.6	39	169.0	169.0	89	204.3	204 3
-		28.3	-		63 6		99.0	1 2 1 1 1			134.3	1	169.7			205.1	
41	29.0		91	64.3	64,3	141	99.7	99.7	191	135.1	135.1						
	30.4		02	67.0	65.8		100.4	100.4	92	135.8	135.8	42	171.1	171.1		206.5	
44	21.1	31.1	94	66.	66.5	43	101.1	1.101			137.2		171.8			207.2	
	31.8	31.8		67.2				102.5			137.9		172.5		94	207.9	208.6
	32.5	_	-		67,9			103.2			138.6						
		33.2	97	68.6	68.6	47	102.0	101.0	97	130.0	130.2	246	173.9	173.9	07	209.3	250.5
48	33.9	33.9	98	69.3	69.3	48	104.6	103.9	98	140,0	140.0	48	175.4	175.4	98	210.7	210.7
49	34.6	34,6	99	70.0	70.0	49	105.4	105.4	99	140.7	140.7	49	170.1	176.1	99	211.4	211.4
			100	70.7	70.7	150	106.1	106.1	100	141.4	141,4	250	176.8	176.8	300	212.1	212.
==		f.ar	-														

Number for the Readier finding the Courses in the foregoing Tables of Difference of Latitude and Departure.

Dift.	and I	Diff. of		1		and.	Depar	ture		of La	at. and	Dep.
Num	Deg.	Num	Deg.		Num	Deg.	Num	Deg.	Num	Deg.	Num!	Deg.
1000	1	17	89		17	1	1000		2	1	5882	89
909	2	35	88	1000	35	2	999	88	3	2	2855	88
908	3	52	87	196	52	3	998	87	5	3	1908	87
997	4	70	86		170	4	997	86	1 7	4	1432	86
996		87	85		87		996	85	9	5	1145	85
995	5	105	84		105	5	995	84	10	6	950	84
993	7	122	83		122	7	993	83	12	7	816	83
990	8	139	82	1. 1. 4	139	8	990	82	14	8	711	82
988	9	156	81		156	9	988	81	16	. 9	632	81
985	10	173	80	3	173	10	985	80	18	10	568	80
982	11	191	79	1	191	11	982	79	19	11	515	79
978	12	208	78		208	12	978	78	21	12	470	78
974	13	225	77		225	13	974	77	23	13	433	77
970	14	242	76		242	14	970	76	25	14	401	76
966	15	259	75		259	15	966	75	27	15	373	75
961	16	276	74		276	16	961	74	29	16	349	74
956	17	292	73	100 m	292	17	956	73	30	17	328	73
951	18	309	72		309	18	951	72	32	18	308	72
945	19	326	71		326	19	945	71	34	19	290	71
940	20	342	70	41	342	20	94°	70	36	20	275	70
934	21	358	69	der.	358	21	934	69	1 38	21	260	69
927	22	375	68		375	22	927	68	40	22	248	68
921	23	391	67		391	23	921	67	42	23	236	67
914	24	407	66		407	24	914	66	45	24	225	66
906	25	423	65		423	25	906		47	25	214	65
899	26	438	64	4	438	26	899	64	49	26	205	64
891	27	454	63		454	27	891	63	51	27	196	63
883	28	470	62	1	470	28	883	62	53	28	188	62
875	29	485	61		485	29	875	61	55	29	180	61
866	30	500	60		500	30	866		58	30	173	60
857	31	515	59		515	31	857	59	60	31	166	59
848	32	530	58		530	32	848	58	62	32	160	
839 829	33	545	57		545	33	839	57	65 67	33	154	57
829	34	559	56	1	559	34	829	50	07	34	148	
819	35	574	55		574 588	35	819	55 1	70	35	143	55
809	36	588	54	12 1	588	36	809	54	73	36	138	54
799 788	37	602	53		602	37	799	53	75 78	37	133	53
788	38	616	52		616	38			78	38		52
777	39	629	51		629	39	777	51	81	39	123	51
	40	643	50	3 4	643	40	766	50	84	40		
755 743 731 719	41	656	49		656 669	41	755	49	87	41	1115	49
743	42	669	48	618	669	42	743	48	90	42	111	
731	43	682	47		682	43	731	47	93	43		
719	44	695	40	33.53	695	44	719		96	44	103	
707	45	707	45	5	707	45	707	45	100	45	1 100	45

The Use of the Tables of Difference of LATITUDE and DEPARTURE, in Working any of the Cases of PLAIN-SAILING.

will be found at the Top of the Tables; but if it is more than 4 Points, or 45 Degrees, will be found at the Bottom of the Tables; and on every Side there are Six Columns for the Distances, mark'd Dist. which contain 50 Miles in each Column, the First beginning at 1, and ending at 50; the Second beginning at 51, and ending at 100, and so on to 300 Miles Distance; and to each of these Columns of Distance there belongs two other Columns, shewing the Difference of Latitude and Departure to any of them Distances, mark'd Lat. and Dep. in which you are to observe, that if your Course be found at the Top of the Tables, then you are to take the Difference of Latitude and Departure as they are mark'd at Top; but if your Course be found at Bottom, then you must take them as they are mark'd at Bottom.

Note, In any Case where the Course is given in Points, half Points, or Quarters, you must make use of the following Tables of Difference of Latitude and Departure, which are calculated for Points, &c. but where the Course is given in Degrees, or where it is not given at all, you must make use of the foregoing Tables of Difference of Latitude

and Departure.

### Plain Sailing, Case the First.

Course and Distance being given, to find the Difference of Latitude and Departure.

### RULE.

Find your Course as before directed, and look in some of the Distance Columns belonging to that Course, for your Distance, the Difference of Latitude and Departure answering to that Distance, will be the Difference of Latitude and Departure required.

Example

#### EXAMPLE I.

A Ship sails NNE. 136 Miles, I demand her Difference of Latitude and Departure.

Having found my Course, which is 2 Points in the Table for Points, I find my Distance 136 in the third Column for Distances, and right against that, I find 125.7 Tenths for my Difference of

Latitude, and 52.0 Tenths for my Departure.

Note, In all Cases whatsoever, if the given Side or Sides be in Miles, then the Sides found by the Table, will also be in Miles; but if the given Side or Sides be Leagues, then the Sides found will also be Leagues.

Plain-Sailing, Cafe the Second.

Course and Difference of Latitude being given, to find the Distance and Departure.

#### RULE.

Find your Course as before, then look in some of the Difference of Latitude Columns belonging to that Course, for your Difference of Latitude, the Distance and Departure answering to that Difference of Latitude, will be the Distance and Departure required.

#### EXAMPLE.

A Ship sails S. 48 Degrees 00 Minutes E. till her Difference of Latitude he 164 Leagues, I demand her Distance and Departure?

Having found my Course 48 Degrees at the Bottom of the Tables, I look in some of the Columns mark'd Latitude at Bottom, for the nearest I can find to my Difference of Latitude, which is 163.9, and answering to that, I find for my Distance 245 Leagues, and for my Departure 182.0 Leagues.

Plain-Sailing, Cafe the Third.

Course and Departure being given, to find the Distance and Difference of Latitude.

### RULE.

Find your Course as before, then look in some of the Departure Columns belonging to that Course, for your Departure, the Distance and and Difference of Latitude answering to that Departure, will be the Distance and Difference of Latitude required.

### EXAMPLE.

A Ship sails SW. by S. till her Departure be 165 Miles: I demand her Distance and Difference of Latitude.

Having found the Course, which is 3 Points at the Top of the Table for Points, I look in some of the Columns mark'd Dep. at Top, for the nearest I can find to my Departure, which is 165.0, and answering to that I find my Distance 297 Miles, and for my Difference of Latitude 246.9 Miles.

Note, In any Case where the given Side is too big to be found in the Tables, then divide it by 2, 3, 4, or any other Number that will make it small enough to be found, and then the required Sides, when found, must be multiplied by the same Number; but the Course must never be multiplied nor divided.

### Plain Sailing, Cafe the Fourth.

Distance and Difference of Latitude being given, to find the Course and Departure.

### RULE.

Put two Cyphers to the Difference of Latitude, and divide it by the Distance (without taking any Notice of the Comma that stands between the Miles and Tenths) and note the Quotient: Then look in the Table of Numbers (at the end of the Tables of Difference of Latitude and Departure) in the Columns belonging to Distance and Difference of Latitude, for the nearest Number to that Quotient, the Degrees answering to that Number will be the Course. Then to find the Departure, proceed as in Case the first. But here you are to obferve, that in all Cases where the Course is to be found by the Table of Numbers, the Difference of Latitude and Departure are supposed always to be in Miles and Tenths, as for Example, 112,4 Tenths, 907,2 Tenths, &c. fo that if at any Time either of them should be given in Miles without Tenths, as 117, 124, &c. You are then to put a Cypher to them to supply the Place of Tenths, and call them 117,0 Tenths, 124,0 Tenths, &c. and then put two Cyphers more according to your other Rules, to find the Number for the Course.

H

### EXAMPLE.

A Ship sails between the North and West, till her Distance is 276 Miles, and her Disserence of Latitude 211.4 Miles, I demand her Course and Departure.

Having put two Cyphers to the Difference of Latitude, which makes it 211400, I divide it by the Diftance 276, and find the Quotient be 766 nearly, then I look in the Table of Numbers (under Dift. and Diff. of Lat.) for the nearest to it which is 766, against which I find 40 Degrees for my Course, and with that Course and my given Distance, I find my Departure to be 177.4 Miles, (by Case the first.)

### Plain Sailing, Case the Fifth.

Distance and Departure being given, to find the Course and Difference of Latitude.

### RULE.

Put two Cyphers to the Departure, then divide it by Distance, and look in the Table of Numbers, in the Columns belonging to Distance and Departure, for the nearest Number to the Quotient; the Degrees answering to that Number will be the Course, and then the Difference of Latitude may be found, (by Case the First.)

### EXAMPLE.

A Ship sails between the South and East, till her Distance is 546 Miles, and her Departure 412 Miles, I demand her Course and the Difference of Latitude.

Having put a Cypher to my Departure to supply the Place of Tenths, which makes it 412.0 and then two more Cyphers according to the Rule for this Case, which makes it 412000, I divide it by the Distance 546, and find the Quotient to be 754, against the nearest to which, viz. 755 in the Table of Numbers under Dist. and Dep. I find 49 Degrees for my Course; and with that Course and my Distance (divided by 2, because it is too big to be found in the Tables) I find a Difference of Latitude 179,1 (by Case the First) which multiplied by 2, because the Distance was divided by 2, gives 358,2 for my whole Difference of Latitude.

Plain

### Plain Sailing, Case the Sixth.

Difference of Latitude and Departure being given, to find the Course and Distance.

### RULE.

Put two Cyphers to the Departure, and divide it by the Difference of Latitude, then look in the Table of Numbers, in the Columns belonging to Difference of Latitude and Departure, for the nearest Number to the Quotient, the Degrees answering to that Number will be the Course. Then to find the Distance proceed as in Case the 2d, or 3d.

### EXAMPLE.

A Ship sails between the North and West, till her Difference of Latitude is 184 Miles, and her Departure 115 Miles, I demand her Course and Distance.

Having supplied the Place of Tenths in both these Sides, which makes them 184.0, and 115.0, I then put two Cyphers to the Departure which makes it 115000, and divide it by the Difference of Latitude 1840, and find the Quotient to be 62; against which in the Table of Numbers, under Difference of Latitude and Departure, I find 32 Degrees for my Course, and with that Course, and my Difference of Latitude, (by Case the Second) or with that Course, and my Departure (by Case the Third) I find my Distance to be 217 Miles.

Note, By these foregoing Rules for Plain Sailing, you may work any Case in Traverse, Mercator, Parallel and Middle Latitude, only by supposing the Names of the Sides and Angles in Mercator, Parallel and Middle Latitude, to be changed into the Sides and Angles they represent in Plain Sailing.

### TRAVERSE.

The several Courses and Distances a Ship sails being given, to find what direct Course and Distance she has made good, and her Distence of Latude and Departure.

### RULE.

Make a Table as on the following Side, and fet down in it your feveral Courses and Distances, then by the Rule, for Case the First of Plain Sailing, find the Difference of Latitude and Departure to each H 2

of the Courses and Distances, and set them down in the Table, opposite to the Courses they belong to, taking Notice that the Dissernce of Latitude must always be set in the North Column, if the Course be Northerly, and in the South Column if the Course be Southerly; and the Departure must always be put in the East Column, if the Course be Easterly, and in the West Column, if it be Westerly.

Then add up all your Columns of North, South, East and West separately, and set down their respective Sums at the Bottom of each Column, and if you have but one Column of Northing or Southing, and but one of Easting or Westing, then their Sums will be the Difference of Latitude and Departure of the same Name with the Column they stand under; that is, the Difference of Latitude will be Northerly, if it stands under the North Column; and the Departure

Easterly, if it stands under the East Column, &c.

But if you have Numbers in all the Columns of North, South, East, and West, then take the Sums of the North and South Columns, and subtract the lesser from the greater, the Remainder will be the Difference of Latitude, of the same Name with the greater of them: Also do the same with the Sums of the East and West Columns for the Departure; then with that Difference of Latitude and Departure, find the Course and Distance, as in Case the Sixth, of Plain Sailing.

### EXAMPLE.

A Ship sails the following Courses, viz. SSW. 54 Miles, W. by S. 39, NW. by N. 40, NE. by E. 69, and NNW. 60 Miles; I demand her direct Course, Distance, Difference of Latitude and Departure.

		Diff. o	f Lat.	Dep	arture
Couries	Dift.	North	South	East,	Wett:
SSW	54	W. T. L.	49.5		20.7
W by S	39		7.6	1.0	38.2
NW by N	40	33.3			22.2
NE by E	69	38.3		57.4	
NNW	60	- 55.4			23.0
		127.0 57.5	57.5	57-4	57.4
Diff. Lat	N.ly		DepW	verly.	-

Note, 'Tis by this Method that the Difference of Latitude and Departure are found in working any Days Work at Sea; and from the Difference of Latitude and Departure so found, we find the Course, Distance and Latitude by Dead - Reckoning, Meridian Distance and Longitude made; all which will be further explained in the Rules for keeping a Journal.

Course N. 34 00 W. Distance 84 Miles.

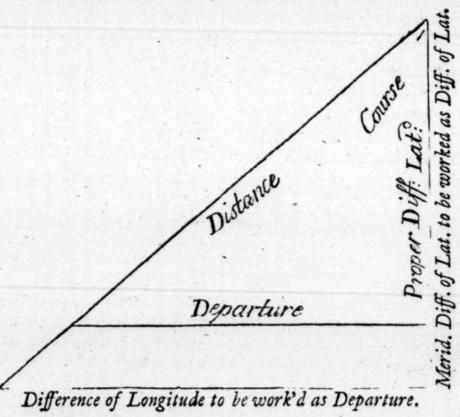
# To Work any Right-angled Triangle, by the foregoing Rules for PLAIN SAILING.

In all Right-angled Triangles that are to be worked by the Tables, you are to suppose four Things, viz. Course, Distance, Difference of Latitude and Departure, two of which must always be given to find the other two: Then as these Rules are wrote for working of Plain Sailing, if you would work any other Sailing by them, as Mercator, Parallel, Middle Latitude, or any other Right-angled Triangle, you must suppose the Sides and Angles of that Triangle to be called by the same Name that the Sides and Angles they represent in Plain Sailing are called by, and then work them as if it was a Case in Plain Sailing.

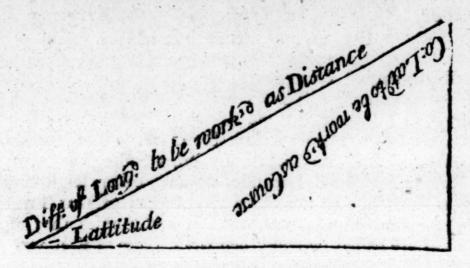
As for Example. The North and South Line, is any Right-angled Triangle (but whatever Name it is called in the Sailing it belongs to) must be work'd as if it was Difference of Latitude in Plain Sailing: The East and West Line as Departure; the long Side as Distance, and the Angle opposite to the East and West Line as Course. For

Example see the following Figures.

Figure for Mercator's Sailing.

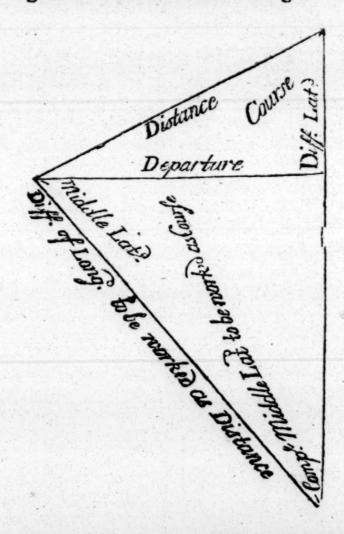


Figure



Distance to be work'd as Departure.

Figure for Middle Latitude Sailing.



### Mercator's Sailing, Cafe the First.

The Latitudes and Longitudes of any two Places being given, to find what Course and Distance a Ship must Sail from one Place to the other.

#### RULE.

Having the two Latitudes and two Longitudes given; find the proper Difference of Latitude, the Meridional Difference of Latitude, and the Difference of Longitude, (as by the Rules for that Purpose) then with the Meridional Difference of Latitude, and the Difference of Longitude (taken as Difference of Latitude and Departure) find the Course by the Sixth Case of Plain Sailing, and with that Course, and the proper Difference of Latitude, find the Distance by Case the Second of Plain Sailing.

### EXAMPLE.

What Course and Distance must a Ship sail from a Place in Latitude 50.00 North, and Longitude, 03.10 West, to a Place in Latitude of 17.10 North, and Longitude 59.11 West?

Having put two Cyphers to the Difference of Longitude, and divided it by the Meridional Difference of Latitude, I find the Quotient to be 138, against which in the Table of Numbers (under Difference of Latitude and Departure) I find 54 Degrees for my Course; and with that Course, and my proper Difference of Latitude, I find my Distance to be 3348 Miles. 3350 Miles.

The Course being thus found in Degrees, I want in the next Place to know what Quarter of the Compass it is in, that is, whether it be so many Degrees from the North towards the East, or from the North towards the West, &c. to do which take the following Rule.

If you are to fail from a greater North Latitude to a less, or from North Latitude into South; or from a lesser South Latitude to a greater, then you must fail to the Southward.

But if you are to fail from a greater South Latitude to a lesser, or from South Latitude into North; or from a less North Latitude to a greater, you must sail to the Northward.

If you are to fail from a Greater East Longitude to a Lesser, or from a Lesser West Longitude to a Greater; or from East Longitude into West, you must fail to the Westward, except the Difference of Longitude be more than 180 Degrees, and then you must fail to the Eastward.

But if you are to go from a Greater West Longitude to a Lesser, or from a lesser East Longitude to a greater, or from West Longitude into East, you must sail to the Eastward, except your Difference of Longitude be more than 180 Degrees, and then you must sail to the Westward.

### EXAMPLE.

In the foregoing Case of Mercator's Sailing, I find by the two Latit. that I am bound from a Greater North Latitude to a Lesser, viz. from 50.00 N. to 17.10 N. then by the Rule I must sail to the Southward; and I find by the two Longitudes, that I am bound from a Lesser West Longitude to a Greater, viz. from 3.10 West to 59.11 West, then by that Rule I am to go to the Westward, therefore my Course will be South 54.00 West, or SW. 3 West nearest.

This first Case of Mercator, being the Case that is always made use of, to find the Course and Distance from Place to Place, or to find the Bearing and Distance of any Place, from the Ship at any Time, I have set down the Work of it at large, and shall leave the other Case for the Reader to exercise himself with, by working them by the Rules

already given him.

A Table of the Angles which every Point and Quarter Point of the Compass makes with the Meridian.

	D M	D M	D M	D M
4	2 49	24 25 19	4 47 49 6	70 19
1234	5 37	21/2 28 07	41 50 38 6	1 73 07
3	8 26	23/4 30 56	4 53 26 6	75 56
1	11 15	3 33 45	5 56 15 7	
14	14 04	3 36 34	5 5 59 04 7	
11/2	16 52	$ 3\frac{1}{2} 39 22$	51/2 61 53 7	- 1.
134	19 41	3 4 42 11	5 6441 7	3 87 11
2	22 30	4 45 00	6 6730 8	

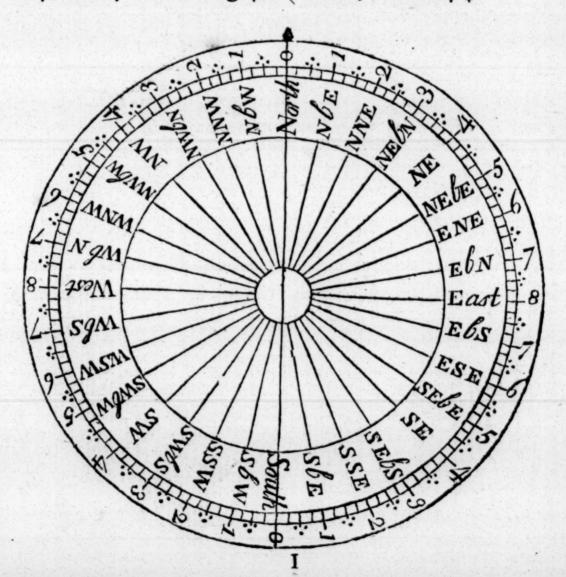
The Use of this Table is to turn Points into Degrees, or Degrees into Points, as follows: Suppose I would know how many Degrees 5 Points are, then I look for 5 Points, and against it I find 56 Deg. 15 Min. or if I would know how many Points 42 Deg. 17 Min. are, I look for the nearest to it, which is 42 Deg. 11 Min. and against that stands 33 Points.

The Courses and Distances being set down in a Traverse Table, as in Page (52) it will be found necessary for the ready looking them out in the Table of Difference of Latitude and Departure, to know what Angles they make with the Meridian, (or as we commonly say) to know how many Points there are, for which Reason I have here given the Figure of the Mariner's Compass, which is to be used as tollows.

Example 1st. Suppose I would know how many Points I must look out for in the Table of Difference of Latitude and Departure, for a SW. by W. Course.

Look in the Figure below, and against the Point mark'd with SW. by W. you will see the Figure 5, which shews that you must look out for 5 Points.

Example 2d. How many Points is E. by N. \(\frac{3}{4}\) E. against E. by N. I find 7, and my Course being \(\frac{3}{4}\) Point more, it makes  $7\frac{3}{4}$ .



3																	
DA	Lat	Dep	Dif	Lat	Del	Dift	Lat	Dep	Dift	La	Dej	Dift	Lat.	Dep	Dift	Lat	Dep
1	01.0	00.0	51	50.9	02.5	101	100.9	05.C	151	150.8	07.4	201	200.8	09 9	251	250.7	12.3
2	02.0	00.1	52	51.9	02.6	02	101.9	05.0	52	151.8	07.5		2018	09,9		251.7	12.4
1	03.0		53		02.6	03		05.1	53	152.8	07.5		202.8	100		252.7	12.4
	C4.0	1	54	53.9	02.7			05.1	54	153.8			203.8	10.0		253.7	12.5
		00,2	55	54 9	02.7	05	104.9	05.2	55	154.8	07.6		204.8	10.1		254.7	12.5
		00,3	56	55,9	02.7	106	105.9	05.2	150	155.8	07.7		205.8	10,1		255.7	12.6
7		00.3	57		02.8	08	106.9		57	156.8	07.7	1	206.8	10.2		256.7	12.6
8	10.5	CO.4	58	57.9	02.8	09		05.3	58	157.8	07.8	00	207.8	10.2		257.7	12.7
10	10,0	00,4	60		02.9	10	109.9	05.4	60	159.8	07.9	10	209,7	10.3		259.7	12.7
111	11.0	-	61	_	03 0	111	110.9	05.5	161	160.8	07.9	-	210,7	10.4	-	260.7	
12	12.0	1 2	62		03.0	12	111.9	05.5	62	161.8	08.0	11	211.7	10.4	62	261.7	
13	13.0	1	63	1.	03,1	13	112.9	05.5	63	162.8	08.0	100 15 100	212.7	10.5	63	262.7	12.0
14		00.7	64	10	03.1	14	113.9		64	163.8	08.1	14	213.7	10.5	64	263.7	13.0
15	15.0	00.7	65	64.9	03.2	15	114.9	05.6	65	164.8	08.1	15	214.7	10.6	65	264.7	13.0
16	16.0	00.8	66	65.9	03.2	116	115.9	05.7	166	165.8	08.2	216	215.7	10.6	266	265.7	13.1
17	17.0	00.8	67	66.0	03.3	17	116,9		67	166.8	08 2		216.7	10.7	67	266.7	13.1
18	1	00.9	68		03.3	18	117.9		68	1.67 8	08.3		217.7	10.7	68	267.7	
19	1	00,9	69			19	118.9		69	168 8	08.3		218.7	10.8	69	268.7	1
20	-	0.10	70	09.9	03.4	20	119.9	-	70	169.8	08.4		219.7	10.8	70	269.7	13.3
21	1	01.0	71	70.9		11	120.9	1 2 -	171	170.8			220.7	10.9	271	270.7	1 3 3
22	1	01.1	72		03.5	11	121,9		11	171.8			221.7	10.9	72 73	271,7	
23	1 -	01.1	73		03.6	11	122.9	1	74				1	1000	74	272.7	-
25		01.2	75			11	30	1 .							75	274.7	1 3 3
26	1	01.3	76		-		-	-		_	-	-		-	276	275.7	13.6
27		01.3	77		903.8	100			11 "			11	1 2 .		77	276,7	
28		01.4			9 03.8		1		78					100	78		3
29		01,4		78.	9 03.9	29	128.8	06.3	79	178.8	80 8				79	278.7	
30	30	01,5	80	79	903.9	30	129 8	06.4	80	179.8	08.	8 30	229.7	11.3	80	279 7	13.8
31	31.0	01.5			9 04.0							- 11		11.4	281	280.7	13.8
32		001.6			9 04.0							. 11			82		20
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35	35.			-	_			-	-	-	-			11.6	0.6		
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37	37.	0 01.9			9 04.		137.			187.			237.7				7 14.1
39		001.9	80		9 04.	39	138.8	06.8	80	188.	8 09.	3 39	238.	11.7	89	283.	7 14.2
40		@ 02.0			9 04.4			06.0	90		8 09.		239.		90	289.	7 14.3
41		0 02.0	-11		9 04.		140.		-	_	8 09.			-			7 14.3
42		9 02,1			9 04.		141.			191.	8 09.	4 42	241.	7 11.9			6 14.4
45	42.	9 02.1	9:	3 92.	9 04.	6 43	142.	3 07.0	93	192.	8 09.	5 4:	242.	7 11.9	93	292.	6 14.4
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45	14.	9 03.2			9 04.		-	07,1	9		8 09.	-			-11		6 14.5
46	45.	9 02.3	96	95.	9 04.	7 146	1145.	07.2	1 1190		8 09.	6 24		7 12.1			6 14.5
17	46.	9 02.3	97		9 04.	8 47	146.	8 07.2	97			7 4	246.				6 14.6
48		9 02.4			9 04.	4	147.	07.3	98	197.	8 09.	7 4	247.	7 12,2			6 14.6
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19 18.9 01.9			68 6-7 06.6							
20										
21       20.9       02.1       71       70.7       06.9       121       120.4       11.8       171       170.2       16.7       221       219.9       21.6       71       269.7       26       72       71.70.0       23       121.4       11.9       72       171.2       16.8       22       220.9       21.7       73       22.0       22.7       27.0       26.9       23       21.9       73       72.0       07.1       23       122.4       12.0       73       72.0       07.1       23       122.4       12.0       73       72.0       72.7       26.9       22.2       22.9       21.9       74       72.7       26.9       22.2       22.9       21.9       74       72.7       26.9       22.2       22.9       21.9       74       72.7       26.9       27       75       76.6       07.4       126.4       12.4       77       176.2       17.2       22.3       22.9 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1000</td> <td></td> <td></td>								1000		
22 21.9   02.2   72   71.7   07.0   22   121.4   1.9   72   17.1   16.8   22   22.0   21.7   72   270.7   26.7   23   12.9   02.2   73   73.6   07.2   24   12.3	-				70	109,2 16.6	20 218.9 21,5		-	5
23   22.9   02.2   73   72.6   07.1   23   122.4   12.0   73   172.2   16.9   23   221.9   21.8   73   271.7   26.8   24.9   02.4   75   74.6   07.3   25   124.4   12.1   75   174.2   17.0   25   223.9   22.0   76   27.5   27.7   26.9   22.6   25.9   02.6   76   75.6   07.4   27   126.4   12.4   77   176.2   17.1   26   224.9   22.1   276   274.7   27.7   2					171	170.2 16.7		271	269.7 26	6
24					72	171.2 16.8	22 220.9 21.7	72		
25	- 1	-				172.2 16.9	Company of the Compan	73		
26	1 1 1 1 1	The Part of the Pa							272.7 26.	9
27   26.9   02.6   77   76.6   07.5   27   126.4   12.4   77   176.2   17.3   27   225.9   22.2   77   275.7   27.2   28.9   02.8   27.9   02.8   79.6   07.8   30   129.4   12.7   80   179.1   17.6   30   229.9   02.9   80   79.6   07.8   30   129.4   12.7   80   179.1   17.6   30   229.9   22.6   80   277.7   27.5	25	24.9 02.4		25 124.4 12,2	75	174.2 17.1	25 223.9 22.0		273.7 27.	0
27   26.9   02.6   77   76.6   07.5   27   126.4   12.4   77   176.2   17.3   27   225.9   22.2   77   275.7   27.2   28.9   02.8   27.9   02.8   79.6   07.8   30   129.4   12.7   80   179.1   17.6   30   229.9   02.9   80   79.6   07.8   30   129.4   12.7   80   179.1   17.6   30   229.9   22.6   80   277.7   27.5	26	25.9 02.5	76 75.6 07.4	126 125.4 12.3	176	175.2 17.2	226 224.9 22.1	276	274.7 27.	1
28   27-9   02-7   78   77.6   07.6   28   127.4   12.5   78   177.1   17.4   28   226.9   22.3   78   276.7   27.3   30   29.9   02.9   80   79.6   07.8   30   129.4   12.7   80   179.1   17.6   30   228.9   22.5   80   278.7   27.5		26.9 02.6		27 126.4 12.4	77		27 225.9 22.2			100
29   28.9   02.8   79   78.6   07.7   29   128.4   12.6   79   178.1   17.5   30   227.9   22.4   79   277.7   27.4   30   29.9   02.9   80   79.6   07.8   30   129.4   12.7   80   179.1   17.6   30   228.9   22.5   80   278.7   27.5   31   30.9   03.0   81   80.6   07.9   131   130.4   12.8   82   181.1   17.8   32   230.9   22.6   281   279.6   27.				28 127.4 12.5	78	177.1 17.4	28 226.9 22.3			
31 30.9 03.0 81 80.6 07.9 131 130.4 12.8 82 181.1 17.8 32 230.9 22.6 281 279.6 27.6 27.6 32 31.8 03.1 82.8 16.6 08.0 32 131.4 13.0 83 182.1 17.9 33 231.9 22.8 82 280.6 27.7 33 32.8 03.2 84 83.6 08.2 34 133.4 13.1 84 13.2 85 184.1 18.1 35 233.9 23.0 85 283.6 28.0 35 34.8 03.4 85 84.6 08.3 35 134.4 13.2 85 184.1 18.1 35 233.9 23.0 85 283.6 28.0 35 36.8 03.6 87 86.6 08.5 37 136.3 13.4 87 186.1 18.3 37 235.9 23.2 87 286.6 28.1 37 36.8 03.6 87 86.6 08.5 38 137.3 13.5 88 187.1 18.4 38 236.9 23.3 88 87.6 08.6 38 137.3 13.5 88 187.1 18.4 38 236.9 23.3 88 286.6 28.3 39 83.8 03.8 89 88.6 08.7 39 138.3 13.6 89 188.1 18.5 30 237.9 23.4 89 287.6 28.4 40 39.8 03.9 90 89.6 08.8 40 139.3 13.7 90 189.1 18.6 40 238.8 23.5 90 288.6 28.5 41.8 04.1 92 91.6 09.0 44 143.3 14.0 91 90.6 08.9 141 140.3 13.8 14.1 94 193.1 18.9 42 240.8 23.7 92 290.6 28.7 44 43.8 04.3 94 93.5 09.2 44 143.3 14.1 94 193.1 19.0 424.2 823.9 94 93.5 09.2 44 143.3 14.1 94 193.1 19.0 424.2 823.9 94 93.5 09.2 44 143.3 14.1 94 193.1 19.0 424.2 823.9 94 292.6 28.9 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 48.8 47.8 04.7 98 97.5 09.6 48 147.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 48.8 47.8 04.7 98 97.5 09.6 48 147.3 14.2 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 49 247.8 24.4 99 297.6 29.3 59.4 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 246 244.8 24.1 296 294.6 29.1 49.8 04.9 100 99.5 09.8 1100 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4		28.9 02.8		29 128.4 12.6	79	178.1 17.5		79		
31 30.9 03.0 81 80.6 07.9 131 130.4 12.8 82 181.1 17.8 32 230.9 22.6 281 279.6 27.6 27.6 32 31.8 03.1 82.8 16.6 08.0 32 131.4 13.0 83 182.1 17.9 33 231.9 22.8 82 280.6 27.7 33 32.8 03.2 84 83.6 08.2 34 133.4 13.1 84 13.2 85 184.1 18.1 35 233.9 23.0 85 283.6 28.0 35 34.8 03.4 85 84.6 08.3 35 134.4 13.2 85 184.1 18.1 35 233.9 23.0 85 283.6 28.0 35 36.8 03.6 87 86.6 08.5 37 136.3 13.4 87 186.1 18.3 37 235.9 23.2 87 286.6 28.1 37 36.8 03.6 87 86.6 08.5 38 137.3 13.5 88 187.1 18.4 38 236.9 23.3 88 87.6 08.6 38 137.3 13.5 88 187.1 18.4 38 236.9 23.3 88 286.6 28.3 39 83.8 03.8 89 88.6 08.7 39 138.3 13.6 89 188.1 18.5 30 237.9 23.4 89 287.6 28.4 40 39.8 03.9 90 89.6 08.8 40 139.3 13.7 90 189.1 18.6 40 238.8 23.5 90 288.6 28.5 41.8 04.1 92 91.6 09.0 44 143.3 14.0 91 90.6 08.9 141 140.3 13.8 14.1 94 193.1 18.9 42 240.8 23.7 92 290.6 28.7 44 43.8 04.3 94 93.5 09.2 44 143.3 14.1 94 193.1 19.0 424.2 823.9 94 93.5 09.2 44 143.3 14.1 94 193.1 19.0 424.2 823.9 94 93.5 09.2 44 143.3 14.1 94 193.1 19.0 424.2 823.9 94 292.6 28.9 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 48.8 47.8 04.7 98 97.5 09.6 48 147.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 48.8 47.8 04.7 98 97.5 09.6 48 147.3 14.2 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 49 247.8 24.4 99 297.6 29.3 59.4 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 246 244.8 24.1 296 294.6 29.1 49.8 04.9 100 99.5 09.8 1100 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4	30	29.9 02.9	80 79.6 07.8	30 129 4 12.7	80	179.1 17.6	30 228.9 22.5	80	278.7 27.	.5.
32 31.8 03.1 82 81.6 08.0 32 131.4 12.9 82 181.1 17.8 32 230.9 22.7 82 280.6 27.7 33 32.8 03.2 83 82.6 08.1 33 132.4 13.0 83 182.1 17.9 33 231.9 22.8 83 281.6 27.8 33 33.8 03.3 84 83.6 08.2 34 133.4 13.1 84 183.1 18.0 34 232.9 22.9 84 282.6 27.9 35 34.8 03.4 85 84.6 08.2 35 134.4 13.2 85 184.1 18.1 35 233.9 23.0 25.0 286.6 28.0 284.6 28.1 35.8 03.5 86 85.6 08.4 136 135.3 133.3 186 185.1 18.2 236 234.9 23.1 286 284.6 28.1 37.3 13.5 88 187.1 18.4 38 236.9 23.3 88 286.6 28.3 39 38.8 03.8 89 88.6 08.7 39 138.3 13.6 89 188.1 18.5 39 237.9 23.4 89 287.6 28.4 40.8 04.0 91 90.6 08.9 141 140.3 13.8 191 190.1 18.7 241 239.8 23.6 291 289.6 28.6 28.7 41.8 04.1 92 91.6 09.0 42 141.3 13.9 92 189.1 18.8 42 240.8 23.7 92 290.6 28.7 43 42.8 04.2 93 92.6 09.1 43 142.3 14.0 93 192.1 18.8 42 240.8 23.7 92 290.6 28.7 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 290.6 28.9 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 290.6 28.9 48.8 04.8 95 98.5 09.5 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 49.8 47.8 04.7 98 97.5 09.6 48 147.3 14.5 98 197.0 19.4 48 246.8 24.3 98 296.6 29.2 49.8 04.9 100 99.5 09.8 150 149.3 14.5 98 197.0 19.6 250 248.8 24.5 300 298.6 29.2 49.8 24.8 24.5 300 298.6 29.2 49.8 24.8 24.8 24.5 300 298.6 29.2 49.8 24.8 24.8 24.5 300 298.6 29.2 49.8 24.8 24.8 24.5 300 298.6 29.2 49.8 24.8 24.8 24.5 300 298.6 29.2 49.8 24.8 24.8 24.5 300 298.6 29.2 29.2		30.9 03.0	81 80.6 07.9	131 130.4 12.8	181	180.1 17.7	231 229.9 22.6	281	279.6 27	.6
33 32.8 03.2 83 82.6 08.1 33 132.4 13.0 83 182.1 17.9 33 231.9 22.8 83 281.6 27.8 33 33.8 03.3 84 83.6 08.2 34 133.4 13.1 84 13.2 85 184.1 18.1 35 233.9 23.0 85 283.6 28.0 35.8 03.5 86 85.6 08.4 136 135.3 13.3 186 185.1 18.2 236 234.9 23.1 286 284.6 28.1 37 36.8 03.6 87 86.6 08.5 37 136.3 13.4 87 186.1 18.3 37 235.9 23.2 87 285.6 28.2 38 37.8 03.7 88 87.6 08.6 38 137.3 13.5 88 187.1 18.4 38 236.9 23.3 88 286.6 28.3 39 38.8 03.8 89 88.6 08.7 39 138.3 13.0 89 188.1 18.5 39 237.9 23.4 89 287.6 28.4 40 39.8 03.9 90 89.6 08.8 40 139.3 13.7 90 189.1 18.6 40 238.8 23.5 90 288.6 28.5 41.8 04.1 92 91.6 09.0 42 141.3 13.9 92 191.1 18.8 42 240.8 23.7 92 290.6 28.7 43 42.8 04.2 93 92.6 09.1 43 142.3 14.0 93 192.1 18.9 43 241.8 23.8 93 291.6 28.8 44 43.8 04.3 94 93.5 09.2 44 143.3 14.1 94 193.1 19.1 45 243.8 24.0 95 243.8 24.0 95 245.6 29.2 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.2 44.8 04.8 04.9 99 89.5 09.5 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 49.8 04.9 100 99.5 09.8 160 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.2 49.8 29.5 09.5 49 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 49 247.8 24.4 99 127.6 29.3 50.2 29.6 29.2 49.8 24.9 99 297.6 29.2 49.8 04.9 100 99.5 09.8 160 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.2 49.8 24.9 24.8 24.5 300 298.6 29.2 49.8 24.9 24.8 24.5 300 298.6 29.2 49.8 24.8 24.5 300 298.6 29.2 29.6 29.2			82 81.6 08.0		82			82		
34					83	182.1 17.9		83		
36 35.8 03.5 86 85.6 08.4 136 135.3 13,3 13.6 87 186.1 18.2 236 234.9 23.1 286 284.6 28.1 37 36.8 03.6 87 86.6 08.5 37 136.3 13.4 88 187.1 18.4 38 236.9 23.3 88 286.6 28.3 39 38.8 03.8 89 88.6 08.7 39 138.3 13.6 89 188.1 18.5 39 237.9 23.4 89 287.6 28.4 40.8 04.0 91 90.6 08.9 141 140,3 13.8 191 190.1 18.7 241 239.8 23.6 291 289.6 28.7 43 42.8 04.2 93 92.6 09.1 43 142.3 14.0 93 192.1 18.8 42 240,8 23.7 92 290.6 28.7 43 42.8 04.2 93 92.6 09.1 43 142.3 14.0 93 192.1 18.9 43 241.8 23.8 93 291.6 28.8 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 46 45.8 04.6 97 96.5 09.5 47 146.3 14.4 97 196.1 19.1 45 243.8 24.0 95 293.6 29.2 48.8 04.8 99 98.5 09.7 49 148.3 14.5 98 197.0 19.4 19.3 19.3 19.5 19.5 49.8 04.9 100 99.5 09.8 160 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.6 29.5 50.8 49.8 04.9 100 99.5 09.8 160 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4 50.9 100 99.5 09.8 160 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4 50.9 100 99.5 09.8 160 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4	34			34 133.4 13.1	84	183.1 18.0			282.6 27	,0
37       36.8 o 3.6       87       86.6 o 8.5       37       136.3   13.4       87       186.1   18.3       37       235.9 23.2       87       285.6   28.2         38       37.8 o 3.7       88       87.6 o 8.6       38       137.3   13.5       88       187.1   18.4       38       236.9 23.3       88       286.6   28.3         39       38.8 o 3.8       89       88.6 o 8.7       39       138.3   13.6       89       188.1   18.5       39       237.9 23.4       89       287.6   28.2         40       39.8 o 3.9       90       89.6 o 8.8       40       139.3   13.7       90       189.1   18.6       40       238.8 23.5       90       288.6   28.5         41       40.8 o 4.0       91       90.6 o 8.9       141       140.3   13.8       191       190.1   18.7       241       239.8 23.6       291       289.6 e 8.6         42       41.8 o 4.1       92       91.6 o 9.0       42       141.3   13.9       92       191.1   18.8       42       240.8 23.7       92       290.6 28.7         43       42.8 o 4.2       93.92.6 o 9.1       43       142.3   14.0       93       192.1   18.9       43       241.8 23.8       93       291.6 28.8         44	35	34.8 03.4	85 84.6 08.3	35 134.4 13.2	85	184.1 18.1	35 233.9 23.0	85	283.6 28	.0
37       36.8 o 3.6       87       86.6 o 8.5       37       136.3   13.4       87       186.1   18.3       37       235.9 23.2       87       285.6   28.2         38       37.8 o 3.7       88       87.6 o 8.6       38       137.3   13.5       88       187.1   18.4       38       236.9 23.3       88       286.6   28.3         39       38.8 o 3.8       89       88.6 o 8.7       39       138.3   13.6       89       188.1   18.5       39       237.9 23.4       89       287.6   28.2         40       39.8 o 3.9       90       89.6 o 8.8       40       139.3   13.7       90       189.1   18.6       40       238.8 23.5       90       288.6   28.5         41       40.8 o 4.0       91       90.6 o 8.9       141       140.3   13.8       191       190.1   18.7       241       239.8 23.6       291       289.6 e 8.6         42       41.8 o 4.1       92       91.6 o 9.0       42       141.3   13.9       92       191.1   18.8       42       240.8 23.7       92       290.6 28.7         43       42.8 o 4.2       93.92.6 o 9.1       43       142.3   14.0       93       192.1   18.9       43       241.8 23.8       93       291.6 28.8         44	36	35.8 03.5	86 85.6 08.4	136 135.2 12.2	186	185.1 18.2		286	284.6 28	.1
38 37.8 03.7 88 87.6 08.6 38 137.3 13.5 88 187.1 18,4 38 236,923,3 88 286.6 28.3 39 38.8 03.8 89 88.6 08.7 39 138.3 13.6 89 188.1 18.5 39 237.9 23.4 89 287.6 28.4 40 39.8 03.9 90 89.6 08.8 40 139.3 13.7 90 189.1 18.6 40 238.8 23.5 90 288.6 28.5 41 40.8 04.0 91 90.6 08.9 141 140,3 13.8 191 190.1 18.7 241 239.8 23.6 291 289.6 48.6 42 41.8 04.1 92 91.6 09.0 42 141.3 13.9 92 191.1 18.8 42 240,8 23.7 92 290.6 28.7 43 42.8 04.2 93 92.6 09.1 43 142.3 14.0 93 192.1 18.9 43 241.8 23.8 93 291.6 28.8 44.8 04.4 95 94.5 09.2 44 143.3 14,1 94 193.1 19.0 44 242.8 23.9 94 292.6 28.9 46 45.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 46 45.8 04.6 97 96.5 09.5 47 146.3 14.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.8 04.9 98 97.5 09.6 48 147.3 14.5 98 197.0 19.4 48 246.8 24.3 98 296.6 29.2 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4 59.4 59.4 50.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4 59.4 59.4 50.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4 59.4 59.4 50.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4	37	36.8 03.6	87 86.6 08.5	22 2 2 2						
39 38.8 03.8 89 88.6 08.7 39 138.3 13.6 89 188.1 18.5 39 237.9 23.4 89 287.6 28.4 40 39.8 03.9 90 89.6 08.8 40 139.3 13.7 90 189.1 18.6 40 238.8 23.5 90 288.6 28.5 41 40.8 04.0 91 90.6 08.9 141 140,3 13.8 191 190.1 18.7 241 239.8 23.6 291 289.6 48.6 42 41.8 04.1 92 91.6 09.0 42 141.3 13.9 92 191.1 18.8 42 240,8 23.7 92 290.6 28.7 43 42.8 04.2 93 92.6 09.1 43 142.3 14.0 93 192.1 18.9 43 241.8 23.8 93 291.6 28.8 44.8 04.4 95 94.5 09.2 44 143.3 14,1 94 193.1 19.0 44 242.8 23.9 94 292.6 28.9 45 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 45 80.4 5 97 96.5 09.5 47 146.3 14.3 196 195.1 19.2 246 244.8 24.1 296 294.6 29.1 46.8 04.6 97 96.5 09.5 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 49 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 49 247.8 24.4 99 297.6 29.3 50 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4	38	37.8 03.7	88 87.6 08.6	38 137.3 13.5					286.6 28	. 3
40       39.8       03.9       90       89.6       08.8       40       139.3       13.7       90       189.1       18.6       40       238.8       23.5       90       283.6       28.5         41       40.8       04.0       91       90.6       08.9       141       140.3       13.8       191       190.1       18.7       241       239.8       23.6       291       289.6       48.6         42       41.8       04.1       92       91.6       09.0       42       141.3       13.9       92       191.1       18.8       42       240.8       23.7       92       290.6       28.7         43       42.8       04.2       93.92.6       09.1       43       142.3       14.0       93       192.1       18.9       43       241.8       23.8       93       291.6       28.8         44       43.8       04.3       94       93.5       09.2       44       143.3       14.1       94       193.1       19.0       44       242.8       23.9       94       292.6       28.9         45       44.8       04.4       95       94.5       09.3       45       144.3       14.2	39	38.8 03.8	89 88.6 08.7	39 138.3 13.6						
41 40.8 04.0 91 90.6 08.9 141 140,3 13.8 191 190.1 18.7 241 239.8 23.6 291 289.6 28.6 42 41.8 04.1 92 91.6 09.0 42 141.3 13.9 92 191.1 18.8 42 240,8 23.7 92 290.6 28.7 43 42.8 04.2 93 92,6 09.1 43 142.3 14.0 93 192.1 18.9 43 241.8 23.8 93 291.6 28.8 44.8 04.4 95 94.5 09.3 45 144.3 14.1 94 193.1 19.0 44 242.8 23.9 94 292.6 28.9 45 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 46 45.8 04.5 96 95.5 09.4 146 145.3 14.3 196 195.1 19.2 246 244.8 24.1 296 294.6 29.1 46.8 04.6 97 96.5 09.5 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.7 98 97.5 09.6 48 147.3 14.5 98 197.0 19.4 48 246.8 24.3 98 296.6 29.2 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4 50.4		39.8 03.9								
42 41.8 04.1 92 91.6 09.0 42 141.3 13.9 92 191.1 18.8 42 240,8 23.7 92 290.6 28.7 43 42.8 04.2 93 92.6 09.1 43 142.3 14.0 93 192.1 18.9 43 241.8 23.8 93 291.6 28.8 44 43.8 04.3 94 93.5 09.2 44 143.3 14.1 94 193.1 19.0 44 242.8 23.9 94 292.6 28.9 45 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 46 45.8 04.5 96 95.5 09.4 146 145.3 14.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.9 98 97.5 09.6 48 147.3 14.5 98 197.0 19.4 48 246.8 24.3 98 296.6 29.2 49 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 49 247.8 24.4 99 297.6 29.3 50 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4										-
43 42 8 04.2 93 92,6 09.1 43 142.3 14.0 93 192.1 18.9 43 241.8 23.8 93 291.6 28.8 44.8 04.3 94 93.5 09.2 44 143.3 14.1 94 193.1 19.0 44 242.8 23.9 94 292.6 28.9 45 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 46 45 8 04.5 96 95.5 09.4 146 145.3 14.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 47 46.8 04.6 97 96.5 09.5 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.9 98 97.5 09.6 48 147.3 14.5 98 197.0 19.4 48 246.8 24.3 98 296.6 29.2 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4										
44 43.8 04.3 94 93.5 09.2 44 143.3 14,1 94 193.1 19.0 44 242.8 23.9 94 292.6 28.9 46 48 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 46 45.8 04.5 96 95.5 09.4 146 145.3 14.3 196 195.1 19.2 246 244.8 24.1 296 294.6 29.1 47 46.8 04.6 97 96.5 09.5 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.9 98 97.5 09.6 48 147.3 14.5 98 197.0 19.4 48 246.8 24.3 98 296.6 29.2 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4										
45 44.8 04.4 95 94.5 09.3 45 144.3 14.2 95 194.1 19.1 45 243.8 24.0 95 293.6 29.0 46 45.8 04.5 96 95.5 09.4 146 145.3 14.3 196 195.1 19.2 246 244.8 24.1 296 294.6 29.1 47 46.8 04.6 97 96.5 09.5 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.7 98 97.5 09.6 48 147.3 14.5 98 197.0 19.4 48 246.8 24.3 98 296.6 29.2 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4										
46						194.1 19.1	45 243.8 24.0		203.6 20	.0
47 46.8 04.6 97 96.5 09.5 47 146.3 14.4 97 196.1 19.3 47 245.8 24.2 97 295.6 29.2 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 49 247.8 24.4 99 297.6 29.3 5© 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4				The second second second	-			-		_
48 47.8 04.7 98 97.5 09.6 48 147.3 14.5 98 197,0 19.4 48 246.8 24,3 98 296.6 29.2 49.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 49 247.8 24.4 99 297.6 29.3 50 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4	47	46.804.6	97 95.5 09.4			195.1 19.2	47 244.8 24.1	290		
49 48.8 04.8 99 98.5 09.7 49 148.3 14.6 99 198.0 19.5 49 247.8 24.4 99 297.6 29.3 5© 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4	48	47.8 04.7		48 147 3 14.4	97	107 0119.3	48 246 8 24.2	97		
50 49.8 04.9 100 99.5 09.8 150 149.3 14.7 200 199.0 19.6 250 248.8 24.5 300 298.6 29.4	1			40 148 214 6						
222 221 222 223 223 223 223 223 223 223		49.8 04.0							208 6 20	.3
The plant   Deplat   Dill Deplat   Dill Dep   Lat   Depl Lat Lat   Dill Dep   Lat					11				The second second	_
		Deplat )	DillDepLat	Hom Dep Las	Ilpit	Dep  Lat	Depl Lat Lat	Dill	(Dep 11	at

for 7½ Points.

# 60 Difference of Latitude and Departure for 3 Points.

-		-	D:0	7	Derl	D:61	Lat	Dey	Diff	Lat	Depl	Dia	Lat.	Der	Did	Lat	Den
Di	Lat	Dep	יוים	Lat	-	-			-					_			
1	01.0	00.1	51	50.4		101	99.9	14.8		149.4	12 60 40	201		29.5		248.3	
2		00.3	52	51.4		45.17	100.9	15.0		1 50.3	22.3			29,6	52	249.3 250.2	37.0
3		00.4	53		07.8	1 -		15.1		151.3	22.4		_	29 9		251.2	
4		00.6	54	53.4	68.1	04	102.9	15.4	55	153.3	22.7		202.8	30.1		252.2	37.4
_5	04.9	-	55	34 4	-	-	-		156		-	_		30.2			
6	1 3 -	00,9	56	55,4			104.8	15.5		154.3	22.9		204.7	30.4		253.2	37.5
8		01.0	57	56.4	08.5			15.8			23.2		205.7	30.5			37.8
		01.2	59	8.4	08.6		-	16.0	59	157.3	23.3	1.27	206.7	30.6		256,2	
10		01.5	60	50.3	08.8	10	108.8	16.1	60	158.3	23.5	10	207.7	30.8	1 6 -	257.2	38.1
111	-	-	61		08.9	111	109.8	16.3	161	159.2	23,6	211	208.7	30.9	261	258.2	38.3
12	1		62		09.1	12	110.8	16.4	62		23.8	12	209,7	31,1	62	259.1	38.4
13	12.5		63		09,2	13	-	16.6	63	161.2	23.9	13	210,7	31.2	63	260.1	38.6
14	13.8		64	63.3	09.4	14	112.8	16.7		162.2		14	211.7	31.4	64	261.1	13-11
15	14.8	02.2	65	64.3	09.5	15	113.7	16.9	65	163.2	24.2	15	212.7	31.5	05	262.1	38.9
16	15.8	02,3	66	65.3	09.7	116	114.7	17.0	166	164.2	24.3	216	2137	31.7	266	263.1	
17		02.5	67	66.3	09.8	17	115.7	17.2	67		24.5				67		39.2
18		02.6		- /	10.0	100	116,7		68	166.2	24.6	11	215.6	32.0		265.1	39.3
19		02.8	11 -		10.1	19	117.7	17,5	69		24.8	19	216.6	32.1	70	266.1	39.5
20	-	02.9	70	09 2	10.3	20	118.7	17.6	76	168.1	24.9	11		-	-		39 6
21		303.1	73			121	119.7	17.7	171	169.1		11	218.6	32,4	271		39.7
22		03.2			1 2 2 4	22	120.7	1 -	72	170.1		u	219.6	77	72	269.0	1
23		03.4				23	121,7	18.0	73	171.1			1	1 0		271,0	
24		03.5	1			11			75	173.1				-	75	A section of	1.
25		03.7	-		-	126		_	176	_			-	-	276		
26	25.	03,8	76			11	124.6	1 0 2		174.1		11	223.5				1 21
27		04,0	77		111.4	11 6											1 -
29		04.3				11											
30			110.		1 11.7	30	128.6		80		26.4	30	227.5	33.7	80	277.0	41.1
31		-	11 =		111.0		129.6	19.2	181	179.0	26.	231	228.5	33.9	281	277.9	41,2
32			110		1 12.0	11 -			82	180.0	26.7		229.5	34.0		278.9	41.4
33		6 04.8	11 -	82.	1 12.2	11			11 0	181.0		11				279 9	
34		6 05.0	84		1 12.3	-								-	11 3	280.9	
35	34.	6 05.1	85	84.	1 12.5			19.8				_		_	85		41.8
36		6 05,3	86	1- ).	1 12.6	136	134.5	19.9	186						286	-0-	
37	36.	6 05 4	87	186	1 12.8	37	135.5			185.0	27.4	37	234.4	34.8	87	283.	42.1
38		5 05.6	88	87.0	12.9	38	136.5	20.2		186.0	27.0	30	235.4	34.9	80	284.	42.2
39		6 05,7	1 89	88,	13.0	39	137 5	20.4	1 00	186.9	27.	40	236.4	35.2	90	285.	42.5
41	39.	605.9			13.2				1173	1.99	20	40	37.4	25.0	201	287.5	1 42 5
41	40.	6 06.0	91		13.3	141	139.5	20.7	191	189.9	28.0	42	238.4	35.5		288.	
42		5 06.2	92		13.5	42	140.5	21.0	92	190.9	28.	42	239.4	35.6	93	289.	
43		06.3	93	92.	13.6	44	142.4	21.1	94	191.9	28.	44	241.3	55.8	94	290.	
44		06.5	95	04.	13.8	45	143.4	21.3	1 95	192.9	28.	45	242.3	35.9	95	291.	
45	1	26	1 06		-			_	106	102.0	28.	246		36.1	296	202.	8 43.4
140	45	06.7	96	195.	14.1	47	145.4	21.6	97	194.0	28.0	47	244 3	36.2	97	293.	3 43.6
47	47	06.9	1 98	06	14.4	48	146.4	21.7	98	195.8	29.0	48	245.3	36.4	98	294.	8 43.7
149	48.	07.2	99	97.	14.4	49		10. 0	99	194.9	29.2	49	1246.2	136.5	1 00	205	7/12.8
50	49.	07.3	100	98.	14.7	150	148,4	22.0	200	197.8	29.	2 50	247-3	36.7	300	296.	7 44.0
	De		Dif	De	Lat	Dif	Dep	Lat	Ditt	Dep	La	Dif	Dep	Lat	Dif	t. De	7 44.0 La 1
1-			1			-1		7	24, 24,	-	-	-		ALVE S		4.4	7

for 7 4 Points.

_	Dit Lat  Der   Ditt Lat  Dep   Dift Lat  Der   Dift Lat  Der   Dift Lat  Dep   Dift Lat  Dep																
D.11	Lat	Del	Ditt	Lat	Dep	Dift	Lat	De	Dift	Lat	De,	Dit	Lat	Dep	Dift	Lat	Dep
1	01.0	00 2	51	50.0	10.0	101	99.1	19,7	151	148.1	49.5	201	197.1	39.2	251	246.1	49.0
		00.4	52	51.0	10.1	02	100.0	19.9	52	149.1	29,7	02	198.1	39,4		247.1	
3	02.9		53	52.0	-	03	101.0		53	150.0	199	03	199.1	39.6	53	248.1	49.4
4	039		54	53.0		04	102.0		54	151.0	30.0	04	200.1	39.8		249.1	
_5	04.9	01.0	55	53.9	10.7	05	103.0	20.5	55	152.0	30.2	05	201.0	40.0	_	250.1	-
6		01.2	56	54 9	10.9	105	104.0			153.0	30 4	206	202.0	40.2		251.1	
7		01.4	57	55,9	11.1	07	104.9		57	1540	30.6		203,0	40.4		252.0	
8	07.8		58	56.9		08	105.9		-	154.9	30.8		204.0	40.6		253.0	
10		02.0	59 60	57·9 58.8	11.7	10	106.9			155.9	31.0	1 22 23	205.0	40.8		254,0	
	_	_	61	_	_	-					31,2	-	205.9	41.0		2550	-
11	10,8	02.3	62	59.8 60 8	11.9	111	108.9	17. 47. 7		157.9	31.4		206.9	41.2		256.0	
13		02.5	63	61.8	12.3	13	109.8	1		158.9	31.6			41.4	62	256,9	51,1
14	13.7	-	64	62.8		14	111.8		64	160.8	32.0	1	200.9	41.8		257.9 258.9	
15		02.9		63.7	12.7	15	112.8	2.7	65	161.8	32.2	1	210.8	42.0		259.9	
16	-	03.1	66	-	12.0	116	113.8		_	162.8	32.4	-	211.8	42.1		260.9	
17		03.3	67	65.7	13.1	17	114 7			163.8	32.6		212.8	42.3	67	261.8	52.7
18		03.5		66.7		18	115.7		1 4-	164.7	32.8			42.5	68	262.8	52.3
19	18.6	03.7		67.7		19	116.7	- 1		165.7	33.0			42.7	69	263.8	52.5
20	19.6	03.9	70	68.6	13 7	20	117.7	23.4	70	156.7	33.2	20	215.7	42.9		264.2	
21	20.6	04.1	71	69.6	13.9	121	118.7	23.6	171	167.7	33.4	221	216.7	43 1	271	265.3	52.0
22		24 3	72	70.6	14.0	22	1196	23 8	72		33.6		217.7	43.3	72	266.7	53.1
23	22.6	04.5	73	71.6		23	120,6		73	169.7	33.8	23	218.7	43.5	73	267.7	53.3
24	1	04.7	74	72.6		24	121.6		74	170.6	34.0	24	219.7	43.7	74	268.7	53.5
25	24.5	04.9	75	73.0	14 6	25	122.6	_	75	171.6	34.1	-	220.6	43.9		269.7	
26		05.1	76	74.5		126	123.6		176	172.6	34.3	1	221.6	44.1	276	270.7	53.9
27		05.3	77	75.5	15.0	27	124.5		77	173.6	34.5	27	222.6	44.3		271.6	
28		05.5				28	125.5			174.6	34.7		223.6	44,5		272,6	
30		05.7	79	77.5	15.4	30	127.5			175.5	34.9		224.6	44.7		273.6	
-	-	06.0	81	-	15.8	-	128.5		181		-					-	
31		06.2		79.4	16.0	32	129.5		-	177.5	35.3	32		45.1	82	275.6	55.0
33		06.4			16.2	33	130.4			179.5	35.5		228.5	45.5	82	277.5	55.0
34		06.6		82.4		34	131.4		84	180.4	35.9	34	229.5	45.7	84	278.5	55.4
35	34.3	1 001				35	132.4		85		36.1	35	230.5	45,9	85	279.5	55.6
36	35.3	07.0	86	84.3		136	133.4	26.5	186	182.4	36.3	236	231.4	46.0		280.5	
37		07.2	87	85.3	17.0	37	134.4		87	183.4	36.5	37	232.4	46.2	87	281.5	\$6.0
38	37.3	07.4	88	86.3	17.2	38	135.3	26.9	88	184 4	36.7	38	233 4	46.4	88	282,4	56.2
39		07.6	89	87.3	17.4	39	136,3	27.1	89	185.3	36.9	39	234.4	46.6	89	283.4	56.4
40		07.8		_	17.6		137.3			186.3				40.8			56.6
41		08,0	91	89 2	17.8	141	138.3	27.5	191	187.3	57.3	243		47.0	291	285.4	56.8
42		08.2	92	90.2	18.0	42	139.3	2777	92	188.3	37-5	42	237.3		92	286.4	57.0
43		08.4		91.2	18.1	43	140.2	27.9	93	189.3	37.7	43	238.3	47.4	93	287.3	57.2
44	43.2	08.6	94	92.2	18.3		141.2	28.2	94	190.2	37.9 38.0			47.8	94	280	57.4
45	-																
47	45.1	09.0	96	94.1	18,7	146	143.2	28.5	190	192.2	38.2	47	241.2	48.0	290	290.	57.8
48		09.4	97	95.1	19.1	47	144,2	28.0	97	194.2	28.6	48		48.4	08	202	2 58.1
49		09.4		97.1	19.3					195.2	28.8		244.2	48.6			2 58.3
50		09.8			19.5				200	196.1	19.0	250		48.8			2 58.5
	_	Lat	Diff	-	La		Dep		Dift		Lat	Diff		Lat	-		Lat
-			11-11	1000		11			11						II.		

for 7 Points.

# 62. Difference of Latitude and Departure for 14 Point.

54	T .	Dank	Dia	F 1	D	D:46	1	12-11	Diter	1	Del	117:4	La	D	ID:4	1	
Din	-	Dep	_	-	_	Dist	Lar		Ditt	Lat	De	Diff	Lac		Ditt	Lat	Dep
1	01,0			49.5		101	98.0			146.5		201	195,0			243.5	
2		00,5	52 53	50.4		02	98.9			147.4	30.9	02	195.9			244.4	
3		01,0	54	52.4			99.9			149.4		04	197.9		54	246.4	_
5	1 3 2	01.2	55	53 4		05	101 9		55	150.4		05	198.9		55	247.4	
6	-	01.5	56	54.3		106	102.8	-		151.3	-	206	199.8	50.1	256	248.3	_
7		01.7	57	55.3		07	103.8			152.3		07	200,8	50.3	57	249.3	62.5
8		01.9	58	56.3		08	104.8		58	153.3	38,4	08	201.8		58	250 3	
9		02.2	₹59		14.3	09	105.7		59	154.2	38.6	09	202.7			251.2	62.9
10	09.7	02.4	60	58.2	-	10	105,7	26.7	60	155.2	38.9	10	203,7	51.0	60	252.2	63.2
11		02.7	61	59 2	14.8	111	107.7		161	156.2	39.1		204.7		261	253.2	63.4
12		02 9	62	60. I	1	12	103.6		62	157,1	39-4		205.6		62	254.1	
13	126		64		3 3	13	109.6		63	158.1			206.6		63	255.1	
14		03.4	65	62.1	15.6	14	110.6		65	159.1			207.6		65	256.1	
16	-		66		-	-	_		166		-	-		_	266		-
17	15.5	03.9	67		16.0	116	112.5	28.2	67	161.0	40.5		209.5		67	258.0	
18	17.6	04.4	68		16.5		114.5		68		40.8		211.5		1 00	260.0	
19		04,6	69		16.8		115.4		69		41.1		212.4		1 4	260,9	
20		04,9	70		17.0	20	116.4		70		41.3				70	261.9	65.6
21	20.4	05.1	71		17.3	121		29.4	171	165.0	41.6	221	214.4		271	262.9	-
22		05.3	72		17.5		118.		72		41.8		215.3		72	263.8	
23	22.	3 05.6		70.8	17.7	23		29.9	2000		42.0	23			73	264.8	66.3
24	23.	05,8			18,0			30.1	74		42,3		217.3		74		66.6
25		06.1	75			25	-	30.4	75		42.5	-	218.3	54.7	75	260,8	66.8
26	1 3	2 06.3	76		18.5			2 30.6	176		42,8			2	276		67.1
27		06.6			18.7			30.9	77		7 43.0			100	77		67.3
29		06.8		11.3	19.0		124.2	31 1	78		43.3	11	221.2		78		67.6
30		1 07.3			6 19.4			31.3			43.5				83		68.0
31				1//	6 19.7		_	31.8	181		6 44.0	-	224.1		281	-	68.3
32	21.	0 07,8			5 19.9		128.	32,1	82	1	5 44.2			56.4	82		68.5
33	32.	0 08,0	8	100	5 20.2			32.3	83		5 44.5	11			83	274.	68.8
34	1 33.	0 38.3	84	181.	5 20.4			0 32.6	84	178.	5 44.7		227.0	56.9	84	275,	69.0
3.5		0 38.	8		5 20.7		131,	32.8	85		5 45.0		228.0	57.1	85	276.	
3		9 08.7	8	- 3.	4 20.9	136	131.	9 33.0	186		4 45.2		228.9	57-3	286	277.4	69,5
37				84.	4 21.1	37	132,	9 33.3	87	181.	4 45,4	37	229.9	57.6	87	278.	69.7
31		9 09.2	8		4 21.4	38		9 33.5	88		4 45.7		230.	57.8	88		70.0
39	37.	8 09.		80.	3 21.6	39	134.	8 33.8	89		3 45.5	39	231.8	50.1	00	280.	70.2
4	30.		_		3 21.9			8 34.0			3 46.2	-					70.5
4	39	8 10.0		88.	3 22.1	141	1 -	8 34.3		185.	3 46.4	42	233.8			282.	70,7
14	40.	7 10.2			2 22.4			7 34.5			2 46.9		234.7			284	71.0
1 4	4 42.	7 10.7		4 01.	2 22.8	44		7 35.0		188	2 47.1	44		59.3	94	285.	71,4
1 4	5 43.	7 10,			2 23.1			35.2		189,	2 47.4	4 45		59.5		286.	71.7
4:	5 44	6 11.2		-	1 23.3	1 - 6	141.	6 35.5	196		1 47.6					-	71.9
1 4	45.	6 11.4	9	194.	1 23.6	47	142.	6 35.7	11 97	191.	1 47,9	47	239.	60.0	97	288.	72.2
		6 11.	9	95.	1 23.8	48	143.	6 36.0	98	192.	1 48.1	48	240.	6 60.3	98	289.	1 72.4
49		5 11,9	9	96.	0 24.1	49	144.	5 36.2	99	193	0 48.4	49	241.				72.7
50		5 12.2		- 2/	0 24.3	1	-	5 36.5			0 48.6		-	5 60.7			72,9
Di	tt L'e	Lat	Di	It De	pLat	Dit	Dep	Lat	Dit	Dep	Lat	Dit	1 Dep	II.at		Dep	1L
					7.77				100	49 7 45		271/10	5 - 10 - 15		VE T		

for 6 3 Points.

											100		18.70				3
D:ft	Lat	Dep	Dift			Dift	Lat	De	Dift	Lat	De	Di	Lat	De	Dift,	Lat	Dep
1		00 3	51	48.8		101		29 3	151	144 5	43.8	2 - 1	192.4	58.3	251	240.2	72 8
1		00.6	52	49.8	-	02		29,6		145.5	44.1	02	193.3	58.6	52	241.2	73. T
3		00.9	53	50.7		03		29.9		146.4	44 4	1	194.3	58.9		242.1	
4		01.2	54	51.7 52.6		04		30.2	54	147.4	44,7	04	195.2	59.2		243.1	
_5		-	55	-	-	05	100.5	-	55	148.3	45.C	05	196.2	59.5			
6	05.7	01.7	56	53.6		106	101.4		156	149.3	45 2	206	197.1	59.7	256	245 0	74.2
7 8	07.7	02.3	57	54 5	16.8	08	102.4		57	150.2	45.8	08	198.1	60.3	57	245.9	74.5
9	08.6	02.6	59	56.5		09	104.3			152.2	46.1	09	200.0	60.6		246.9 247 9	
10	3	02.9	00	57.4		10	105.3		1 2	153.1	46.4	10	201.0	60.9	60	248.8	75,4
11	10,5	03.2	61	58 4	17.7	111	106.2	-	161	154.1	46.7	211	201.0	61.2		249.8	_
12		03.5	62			12	107,2	1	1 .		47.0	12	202.9	61.5		250.7	75.7
13	12.4		63	60.3		13	108.1			156.0	47.3	13	203,8	61.8	63	251.7	76.3
14	13.4	04.1	64	61.2		14	109.1		64	156.9	47.6	14	204.8	62.1		252.6	
15	14 4	24 4	65	62.2	18.9	15	110.1	33.4	65	157.9	47 9	15	205.8	62.4	65	253.6	76.9
16	15.3	1 270,3	66	63.2		116	1110	33.6	166	158.9	48.1	216	206.7	62.6	266	254,6	77.1
17	16.3		67			17	112.0		67		48.4	17	207.7	62.9	67	255.5	77.4
18		05.2		65.1		18	112,9			160.8	48.	I real	208.6	63.2	68	256,5	77.7
20		05.5	70	67.0		19	113.9		69	161.7	49.0	20	209.6	63.5		257.4	
-	-		-	-	-	-	114.8	-	-		49,3	-		-		258.4	-
21	20.1	06.4	71 72	68.9		22	115.8		171	163.6	49.6	1	211.5	64.1	271	259.3	73.6
23		06.7	73	69.9		23	117.7		72 73	165.6	49.9		212.5	64.4		260.3	
24		07 0	74	70.8		24	118.7		74	156.5	50.5	1	214.4	65.0		261.3 262.2	
25	11 100 100 100 100	07.3	75	71.8		25	1196		75	167.5	50.8	25	215.3	65,3		263.2	
26	-	07.5	76	72.7	22.0	126	120.6		176	168.4	51.0	226	216.3	65.5		264.1	-
27		07.8	77	73.7	22.3	27	121.5	36.8	77	169.4	51,3	27	217.2	65.8		265.1	
28		03,1		74.6		28	122.5	37.1	78	170.3	51.6	28	218.2	66.1		266.0	
29		08.4		75.6		29	123.5		79	171.3	51.9	29	219.2	66.4		267.0	
30	28.7	08.7	80	76.6		30	124.4	-	80	172.3	52.2	30	220.1	66.7	-	268.0	-
31		09.0	81	77.5		131	125.4	38.0	181	173.2	52.5	231	221.1	67.0	281	268.9	81.5
32		09.3	82	78.5		32	126.3	38.3	82	174.2	52.8	32	222.0	67.3	82	269.9	8.18
33		09.6	83	79.4 80.4		33	127.3	28.0	83	175.1	53.1	33	223.0	67.6		270.8	
35	33.5		85	81.3		34	129.2		85	177.0	53.4	34	223.9	68.2	1 0	271.8	10
36	34.5	-	86	82.3	_	136	130.2		186	178.0	-	236		68.4	-96	-	0
37	35,4			83.3		37	131.1		87	179.0	53.9	37	225.9	68.7		273.7 274.7	
38		11.0	88	84.2	25.5	1 0	132.1		88	179.9	54.5	1. 43	0.3.00	69.0	88	275.6	83.5
39	37.3	11.3	89	85.2	25.8	39	133.0	40.3	89	180.9	54.8	39	228.7	69,3	89	276.6	83.8
40	38.3	11.6	90	86.1	26.1	40	134.0	40.6	90	181.8	55.1	40	229.7	69.6	90	277.5	84.1
41	39.2	11.9	91	87.1	26.4	141	134,9	40.9	191	182.8	55.4	241	230.6	69.9	291	478.5	84.4
42		12.2			26.7		135.9	41.2	92	183.7	55.7		231.6		92	279.4	84.7
43		12.5			27.0		136,9	41.5	93	184.7	56.0	43	232.5	70.5	93	280.4	85.0
44		12.8		90.0	27.3		137.8	41.8	94	185.7 186.6	56.3	44		70.8	94	281.4	\$5.3
45	43.1	_	95		27.6	45	138.8	42.1	95	100.0	56.6	45	234.5	71.0	95	202,3	85.6
46		13.3	96	91.9	27.8	146	139.7	42.3	196	187.6	56.8	246	235.4	71.3	296	283.3	3 85.8
47	45.0	13.6	97	92.8	28.1	47	140.7	42,0	97	188.5	57.1	47	236.4	71.6	97	284.2	86.1
49		13.9		94.7		49	142,6	42.2		190.4		49	238.3	72.2		285.2	1 86 -
50		14.5			29.0		143.5	43.5	200	191.4				72.5	300	287.1	87.0
-	De		Dia	_	-		Dep	La	_	Dep	Lat			Lat		Dep	T Spinsteller
-	100	·La:	II Jill	1 ch	La	1 Din	.Dep	( ra.	1 Dill	Бер	(Lade	1011	Inch	Lai	Din	Inch	Latt

for 6 ½ Points.

## 64 Difference of Latitude and Departure for 13 Point.

1 01,9 00.3 51 48.0 17.2 101 95.1 34.0 151 142.2 50.9 201 189.2 67.7 25.2 336.3 84.9 3 2 01.9 00.7 53 449.0 17.5 02 95.0 34.4 52 143.1 51.2 02 190.2 68.0 55 217.3 84.9 34.9 34.9 34.9 35.9 34.5 15.2 34.5 15.	Diff	Lat	Del	Dift	Lat	D :p	(Diff)	Lat	Deyl	Diff	Lat	Deil	Dift	Lat	Deil	Dia	Lat	Dep
2 0.1 0 0.7 0 0.7 0 0.1	1	01,9	00.3	51	48.0	17.2	101	95.1	_	-		_	-	-	-	-	-	-
3 0.2. 8 01.0	2		- 1		49.0	17.5	02											
S	3						- 11-20						03			53		85.2
6 05.6 02.6 05 05 52.7 18.9 10.0 99.8 35 7 150 146.9 52.5 10.0 194.0 194.0 194.0 195.0 194.0 194.0 195.0 195.0 194.0 194.0 195.0 195.0 195.0 194.0 194.0 195	4							97.9	35.3		1000	The second second						
7 0.6.6   32.4   57   53   74   9.5   0.8   10   73   6.4   6.5   9.5   0.8   19.5   0.8   0.9   12.0   10	-3	-	-	-	-	-	-	-	_				-		_			_
8							1				140.9	52,5						
9 08 5   0.5							1				148.8	52.2						
10   09.4   03.4   60   56.5   20.2   10   103.6   37.0   60   150 6   53.9   10   193.7   70.7   60   24.5   87.6   88.6   87.6   11   10 4   03.7   64   62   58.4   20.9   12   105.4   37.7   62   152.5   54.6   11   198.7   71.1   62   24.5   78.7   88.6	9	08 5	03.0															
12 11.3 0.4.0 63 38.4 20.9 12 105.4 37.7 62 152.5 54.6 12 199.6 71.4 62 246.7 88.2 13 12 0.4.4 63 59.3 21.6 11.07.3 38.4 64 154.4 155.2 14.01.5 73.1 64 243.6 88.9 15 14.1 0.1 65 61.2 21.9 15 108.5 38.7 65 155.3 55.6 15 20.2 4 72.4 65 249.5 89.2 15 15.1 0.5.4 66 62.1 22.2 116 109.2 39.1 166 156.3 55.9 15 0.0 6.7 65.0 6.1 22.9 18 111.1 39.7 68 158.2 56. 17.0 06.1 68 64.0 22.9 18 111.1 39.7 68 158.2 56. 19 10 20.2 73.1 68 25.2 39.0 19 17.9 06.4 69 65.0 23.2 19 11.2 40.1 69 159.1 56.8 2.9 19 20.0 273.5 68 252.3 90.3 19 17.9 06.4 69 65.0 23.2 19 11.2 40.1 69 159.1 56.9 19 20.2 73.5 68 252.3 90.3 19 17.9 06.4 69 67.7 70 55.9 2.1 6.0 13.0 4.7 70 160.1 57.3 2.0 10.0 15.3 2.0 19 17.9 06.4 69 69.0 2.2 2 113.0 40.8 171 161.0 57.6 2.1 19.8 07.1 71 56.8 23.9 121 113.9 40.8 171 161.0 57.6 2.1 20.0 17.7 1.2 56.8 23.9 121 113.9 40.8 171 161.0 57.6 2.1 20.0 17.7 1.2 56.8 23.9 121 113.9 40.8 171 161.0 57.6 2.1 20.0 70.7 7.7 7.7 7.7 7.7 7.7 2.4 2.9 2.1 11.5 2.1	10	09.4	03.4	60	56.5	20.2	10	103.6	37.0	60			10	197.7	70.7	60	-	
13 12 2 04.4 63 59.3 21.2 13 106., 33.1 63 153.5 54.9 13 200.5 71.7 63 247.6 88.9 15 141 0.1 65 61.2 11.9 15 108.3 38.7 65 15.55.3 55.6 114 101.5 72.1 16 248.6 88.9 16 15.1 05.4 66 62.1 21.9 15 108.3 38.7 65 15.55.3 55.6 17 16 0.5.7 67 63.1 22.6 17 110.2 39.4 67 157.2 56.2 17 20.4 72.4 65 249.5 89.2 19 17.9 06.1 68 69 65.0 23.2 19 112.0 40.1 69 159.1 56.9 19 20.6 2.7 73.4 68 25.3 90.3 19 17.9 06.4 69 65.0 23.2 19 112.0 40.1 69 159.1 56.9 19 20.6 2.7 73.4 68 25.3 90.3 19 17.9 06.4 69 65.0 23.2 19 112.0 40.1 69 159.1 56.9 19 20.6 2.7 73.4 69 25.3 90.3 19 12.0 40.1 70 150.1 57.3 2.2 10.0 70.4 72 67.8 24.2 22 114.9 41 72 150.9 57.9 22 209.0 74.8 72 25.6 19 12.2 21.7 07.7 73 68.7 24.6 23 11.5 44.4 73 162.9 58.3 23 120.0 75.1 73 25.0 91.9 24 22.6 08.1 74 69.7 24.9 24 16.7 74.1 8.7 74.1 8.7 74.5 75 25.9 91.7 24.1 25.3 25.1 17. 42.1 75 164.8 58.9 25 211.8 75.8 75. 25.9 92.6 27 27 25.4 09.1 77 72.5 25.9 27 119.6 (2.8 77 166.5 59.6 23 21.8 76.1 37.7 72.5 25.9 91.9 20.2 20.9 07.4 72.5 25.9 92.6 27 24.5 24.5 24.5 24.5 24.5 24.5 24.5 24.5				1			111				151.0	54.2	211	198.7	71.1		245 7	87.9
14   13.2   04.7   64   60.3   21.6   14   107.3   38.4   64   154.4   55.2   14   201.5   72.1   64   243.6   88.9     15   14   10.1   65   66.2   11.9   15   108.3   38.7   66   155.3   55.6   15   20.2   47.2   65   249.5   89.9     17   16 0 0 5.7   67   63.1   22.6   17   110.2   39.4   67   157.2   56.6   17   204.3   73.1   67   251.4   89.9     18   17.0   06.1   06.6   69.6   69.2   32.9   18   111.1   39.7   68   158.2   56.6   18   205.2   73.4   68   252.3   90.3     19   19   19   19   20.6   27.3   68   25.0   23.2   19   112.2   40.1   69   159.1   56.9   19   20.6   27.3   68   253.3   90.3     19   19   19   20.6   27.5   27.4   27.1   255.1   27.1   255.2   27.1   2					1-	1 -1												
15	3 . m	1 -					1											
16										65							100	
17 16.0 0 557 67 63.1 22 6 17 110.2 39.4 67 157.2 56.2 17 204.3 73.1 67 251.4 89.9 18 17.0 06.1 168 64.0 12.9 18 111.1 39.7 68 158.2 56.6 18 205.2 73.4 68 253.3 90.6 18 8 06.7 70 65.9 23.6 20 113.0 40.4 70 160.1 57.3 20.00 27.1 74.1 70 254.2 90.3 113.0 40.4 70 160.1 57.6 22 20.0 7.7 4 72 67.8 24.2 22 114.9 41 72 161.9 57.9 22 20.0 74.8 72 256.1 91.6 23 21.7 7.7 73 68.7 24.6 23 115.5 41.4 73 162.9 58.8 75 70.7 25.3 25 117. 42.1 75 164.8 58.9 25 211.8 75.8 75 258.0 92.6 27.3 74 22.6 08.1 74 69.7 24.9 24 116.7 41.8 74 163.8 58.6 24 210.9 75.4 74 258.0 92.3 25 23.5 08.4 75 70.7 25.3 25 117. 42.1 75 164.8 58.9 25 211.8 75.8 75 258.9 92.6 27.3 09.8 76 71.6 25.6 126 118.1 42.4 76 165.7 59.3 26 212.8 76.1 74 259.9 93.0 77.2 72.5 25.9 27 119.6 12.8 77 166.6 59.6 27 21.3 76.5 93.3 29 27.3 09.8 79 74.4 26 6 29 121.5 43.4 79 168.5 50.3 29 215.6 77.1 79 262.7 94.0 29 121.5 43.4 8 20 169.5 50.6 20 21.2 8 76.1 93.6 8 27.2 20.0 20.0 20.0 20.0 20.0 20.0 20.0			-		_	-	-	_	-			-		_			-	
18       17.0   06.1   68   64.0   2.9   18   111.1   39.7   68   158.2   56.6   18   205.2   73.4   69   253.3   90.6   211.2   40.1   70   160.1   57.6   22   20.1   74.1   70   254.2   90.6   273.5   90.	17				100		1		1 1									
18 8   06.7   70   65.9   23.6   20   113.0   10.4   70   160.1   37.3   20   207.1   74.1   70   254.2   90.9   207.1   74.1   70   254.2   90.9   207.1   74.1   70   254.2   90.9   207.1   74.1   70   254.2   90.9   207.1   74.1   70   254.2   90.9   207.1   74.1   70   254.2   90.9   207.1   74.1   70   254.2   90.9   207.1   74.1   70   254.2   90.9   207.1   74.1   75.1   207.1   75.1   73   255.1   91.6   207.1   74.1   75.1   207.1	45.0	1 .				22.9		1200		68						68		
1		17.9	06.4		1.			1.5. 1.5. 1.										100000000000000000000000000000000000000
22 20.7 07.4 72 67.8 24.2 22 114.9 41 1 72 161.9 57.9 22 209.0 74.8 72 256.1 91.6 23 21.7 07.7 73 68.7 24.6 24 16.7 41.8 74 163.8 58.6 24 210.9 75.4 74 258.0 92.3 25.5 08.4 75 70.7 25.3 25 117. 42.1 75 164.8 58.9 25 211.8 75.8 75 258.9 92.6 24.5 08.8 76 71.6 25.6 126 118.6 42.4 176 165.7 59.3 226 212.8 76.1 276 259.9 93.0 27 25.4 09.1 77 72.5 25.9 27 119.6 12.8 77 166.6 59.6 27 213.7 76.5 77 260.8 93.3 20.4 09.4 78 73.4 26.6 29 121.5 43.4 79 168.5 50.3 28 214.7 76.8 78 261.7 93.6 29 27.3 09.8 87 77.4 26.6 29 121.5 43.4 79 168.5 50.3 30.1 10.8 82 77.2 27.6 32 124.3 34.5 82 171.4 61.3 32 218.4 78.1 83 78.1 28.0 33 13.1 11.1 83 78.1 28.0 33 125.2 14.8 83 172.3 61.6 33 219.4 78.5 83 266.4 99.3 34 32.0 11.5 85 80.0 28.6 35 127.1 45.5 85 174.2 62.0 37 34.8 12.5 87 81.9 29.3 37 129.9 46.1 87 176.1 63.0 37 222.1 79.5 85 268.3 96.0 38 35.8 12.8 88 82.5 29.6 88 82.5 29.6 38 89 177.0 66.7 3 38 222.1 80.2 88 77.2 29.6 78.2 90.0 44.4 14.4 14.8 94 88.5 31.7 44 135.8 97 91.3 32.7 47.8 92 180.8 64.7 42 227.8 81.5 92 274.9 98.3 44.4 14.4 14.8 94 88.5 31.7 44.1 135.6 48.2 91 182.6 65.3 44.2 227.8 81.5 99.0 273.0 97.7 99.4 44.1 15.8 97 91.3 32.7 47 138.4 49.5 91 182.5 66.7 44.2 227.8 81.5 99.0 273.0 97.7 99.4 44.1 15.5 99.0 33.3 3.0 49.1 31.8 33.3 49.4 39.5 99.2 33	-	-		-	-	-	20	-	-	70	-	-	-			_	254.2	90.9
23										1						11.5		
24	1999									100000								
25 23.5 08.4 75 70.7 25.3 25 117. 42.1 75 164.8 58.9 25 211.8 75.8 75 258.9 92.6 24.5 08.8 76 71.6 25.6 126 118.1 42.4 176 165.7 59.3 226 212.8 76.1 276 259.9 93.0 22.4 4.6 4.6 1.6 1.6 1.8 1.2 1.6 1.8 1.2 1.6 1.8 1.2 1.6 1.8 1.2 1.2 1.2 1.3 1.3 1.2 1.3 1.3 1.2 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	400.00																	
26	25																	
27	26	24.5	08.8	76	71.6	25.6	126	118.0	12.4	176	165.7	59.3				276	_	92.0
29								119.6	12.8	77	166.6	59,6	27			77	260.8	
30 28.2 10 1 80 75.3 26.9 30 122.4 43.8 80 169.5 50.6 30 216.5 77.5 8.3 263.6 94.3 31 10.8 82 77.2 27.6 32 124.3 44.1 81 170.4 61.0 231 217.5 77.8 82 265.5 95.0 30 110.8 82 77.2 27.6 32 124.3 44.5 82 171.4 61.3 32 218.4 78.1 82 265.5 95.0 33 31.1 11.1 83 78.1 28.0 33 125.2 44.8 83 172.3 61.6 33 219.4 78.5 83 266.4 95.3 33.0 11.8 85 80.0 28.6 35 127.1 45.5 85 174.2 62.7 35 221.3 79.1 85 268.3 96.0 37 34.8 12.5 87 81.9 29.3 37 129.0 46.1 87 170.1 63.0 37 223.1 79.8 87 270.2 96.7 38 35.8 12.8 88 82.5 29.6 38 129.9 46.5 88 177.0 63.3 38 224.1 80.2 88 271.2 96.0 37.7 13.5 90 84.7 30.3 40 131.8 47.2 90 178.9 64.0 40 226.0 80.8 90 273.0 97.7 41 38.6 13.8 91 85.7 30.6 141 132.8 47.2 90 179.8 64.3 32.0 14.1 92 86.6 31.0 42 133.7 47.8 91 181.7 65.0 42 133.7 44 135.6 48.2 44 14.4 14.8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 42 227.8 81.5 92 274.9 98.3 44 44.4 14.8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 42 227.8 81.5 92 274.9 98.3 45.4 44.4 14.8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 42 227.8 81.5 92 274.9 98.3 42.4 15.2 95 89 432.0 45 136.5 48.8 95 183.6 65.7 45 230.7 82.5 95 277.7 99.4 44.3 15.8 97 91.3 32.7 47 13.6 54.8 95 183.6 65.7 45 230.7 82.5 95 277.7 99.4 44.3 15.8 97 91.3 32.7 47 13.8 49.5 94 182.6 65.3 47 232.5 83.2 99 279.6 100.0 49 46.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67.0 49 234.4 83.9 99 281.5 100.4 94.1 16.8 100 94.2 33.7 150 141.2 50.5 141.2 50.	THE STATE						1.			3710								
31 29 2 10.4						100					160.5	50.3						
32 30.1 10,8 82 77.2 27,6 32 124.3 44.5 82 171.4 61.3 32 218.4 78.1 82 265.5 95.0 33 31.1 11.1 83 78.1 28.0 33 125.2 14.8 83 172.3 61,6 33 219.4 78.5 83 266,4 95.3 34.3 12.5 11.5 84.7 79.1 28.3 34.1 26.2 45.1 84.1 173.2 62.0 34.2 20.3 78.8 84.2 67.4 95.6 35.5 33.0 11.8 85 80.0 28.6 35 127.1 45.5 85 174.2 62.3 35 221.3 79.1 85.2 68.3 96.0 37.3 14.8 12.5 87 81.9 29.3 37 129.0 46.1 87.1 170.1 62.6 2.3 35.8 12.8 88 82.5 29.6 38 129.9 46.5 88 177.0 63.3 38.2 24.1 80.2 88.2 71.2 96.0 37.7 13.5 90 84.7 30.3 40.131.8 47.2 90 178.9 64.0 40.2 26.0 80.8 90.2 73.0 97.7 41.3 83.6 13.8 91 85.7 30.6 141 132.8 47.5 191 179.8 64.3 241 226 9 81.2 291 274.0 98.0 40.1 14.1 14.8 94 88.5 31.7 44.1 13.6 48.2 93 181.7 65.0 43.2 28.8 81.8 93.2 75.9 98.7 44.4 14.4 14.8 94 88.5 31.7 44.1 35.6 48.5 94.1 182.6 65.3 44.2 29.7 82.2 94.2 76.8 99.0 45.1 16.5 99.9 3.2 33.3 49.140.3 50.2 99.183.6 65.7 45.2 33.5 83.5 98.2 277.7 99.4 46.1 16.5 99.9 3.2 33.3 49.140.3 50.2 99.183.8 60.7 49.2 24.4 83.9 99.2 273.0 97.7 99.4 46.1 16.5 99.9 3.2 33.3 49.140.3 50.2 99.183.8 60.7 49.2 24.4 83.9 99.2 273.0 99.2 279.5 10.0 282.5 1		-	-		123	-		_	_	-			-			-	-	
33 31.1 11.1 83 78.1 28.0 33 125 2 14.8 83 172.3 61,6 33 219.4 78.5 84 267.4 95.6 35 33.0 11.8 85 80.0 28.6 35 127.1 45.5 85 174.2 62.3 35 221.3 79.1 85 268.3 96.0 37 34.8 12.5 87 81.9 29.3 37 129,0 46.1 87 176.1 63.0 37 223.1 79.8 87 270.2 96.7 38 35.8 12 8 88 82.5 29.6 38 129.9 46.5 88 177.0 63.3 38 224.1 80.2 88 271.2 96.0 37.7 13.5 90 84.7 30.3 40 131.8 47.2 90 178.9 64.0 40 226.0 80.8 90 273.0 97.7 41 38.6 13.8 91 85.7 30.6 141 132.8 47.5 191 179.8 64.3 241 226 9 81.2 291 274.0 98.0 40.5 14.5 93 87.6 31.3 43 134.6 48.2 93 181.7 65.0 43 228.8 81.8 93 275.9 98.7 44.4 14.8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 44 229.7 82.2 94 276.8 99.0 45.4 15.2 95 89.4 32.0 45 136.5 48.8 95 183.6 65.7 45 230.7 82.5 95 277.7 99.4 44.3 15.8 97 91.3 32.7 47 138.4 49.5 47 138.4 49.5 97 185.5 66.3 47 232.5 83.5 98 280.6 100.4 49 46.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67,0 49 234.4 83.9 99 281.5 100.7 50.7 116.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84.2 300 282.5 101.0	32										170.4	61.2	32	218.4	77.0			
34 32.0 II.5 84 79.1 28.3 34 I26.2 45.1 84 173 2 62.0 34 220.3 78.8 84 267.4 95.6 35 33.0 II.8 85 80.0 28.6 35 I27.1 45.5 85 174.2 62.3 35 221.3 79.1 85 268.3 96.0 37 34.8 I2.5 87 81.9 29.3 37 I29.0 46.1 87 176.1 63.0 37 223.1 79.8 87 270.2 96.7 38.3 35.8 I2.8 88 82.5 29.6 38 I29.9 46.5 88 I77.0 63.3 38 224.1 80.2 88 271.2 96.0 37.7 I3.5 90 84.7 30.3 40 I31.8 47.2 90 I78.9 64.0 40 226.0 80.8 90 273.0 97.7 41 38.6 I3.8 91 85.7 30.6 I41 I32.8 47.5 191 I79.8 64.3 40.5 I4.5 92 86.6 31.0 42 I33.7 47.8 92 I80.8 64.7 42 227.8 81.5 92 274.0 98.0 40.5 I4.5 93 87.6 31.3 43 I34.6 48.2 93 I81.7 65.0 43 228.8 81.8 93 275.9 98.7 44.4 I4.8 94 88.5 31.7 44 I35.6 48.2 95 I83.6 65.7 45 230.7 82.5 95 277.7 99.4 44.3 I5.8 97 91.3 32.7 47 I38.4 49.5 94 182.6 65.3 45 230.7 82.5 95 277.7 99.4 44.3 I5.8 97 91.3 32.7 47 I38.4 49.5 95 I83.6 66.7 45 230.7 82.5 95 277.7 99.4 46.1 I6.5 99 93.2 33.3 49 I40 3 50.2 99 I87.4 67.0 49 234.4 83.9 99 281.5 I00.7 50 47.1 I6.8 I00 94.2 33.7 I50 I41.2 50.5 141.2 50.5 200 I88.3 67.4 250 235.4 84.2 300 282.5 I01.0					78.1	28.0							7 7					
36 33 9 12.1 86 81,0 29.0 136 128.0 45.8 186 175.1 62.6 236 222.2 79.5 286 269.2 96.3 37 34.8 12.5 87 81.9 29.3 38 129.9 46.5 88 177.0 63.3 38 224.1 80.2 88 271.2 96.0 37.7 13.5 90 84.7 30.3 40 131.8 47.2 90 178.9 64.0 40 226.0 80.8 90 273.0 97.7 41 38.6 13.8 91 85.7 30.6 141 132.8 47.5 191 179.8 64.3 40.5 14.5 92 86.6 31.0 42 133.7 47.8 92 180.8 64.7 42 227.8 81.5 92 274.9 98.3 40.5 14.5 93 87.6 31.3 43 134.6 48.2 93 181.7 65.0 43 228.8 81,8 93 275.9 98.7 44 14.4 14,8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 44 229.7 82.2 94 276.8 99.0 45.4 41.4 14,8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 44 229.7 82.2 94 276.8 99.0 45.4 41.3 15.8 97 91.3 32.7 47.8 95 183.6 65.7 45 230.7 82.5 95 277.7 99.4 40.3 15.8 97 91.3 32.7 47 138.4 49.5 95 183.6 65.7 45 230.7 82.5 95 277.7 99.4 48.4 15.2 98 92.3 33.0 48 139.3 49.8 98 186.4 66.7 48 233.5 83.5 98 280.6 100.4 46.1 16.5 99 93.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84.2 300 282.5 101.0								1			173 2	62.0	T. T. C.	220.3	78.8			95.6
37 34.8 12.5 87 81.9 29.3 37 129.0 46.1 87 176.1 63.0 37 223.1 79.8 87 270.2 96.7 88 35.8 12 8 88 82.5 29.6 38 129.9 46.5 88 177.0 63.3 38 224.1 80.2 88 271.2 96.0 37.7 13.5 90 84.7 30.3 40 131.8 47.2 90 178.9 64.0 40 226.0 80.8 90 273.0 97.7 41 38.6 13.8 91 85.7 30.6 141 132.8 47.5 191 179.8 64.3 42 227.8 81.5 92 274.0 98.0 42 39.5 14.1 92 86.6 31.0 42 133.7 47.8 92 180.8 64.7 42 227.8 81.5 92 274.9 98.3 40.5 14.5 93 87.6 31.3 43 134.6 48.2 93 181.7 65.0 43 228.8 81,8 93 275.9 98.7 44 14.4 14.8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 44 229.7 82.2 94 276.8 99.0 45.4 41.4 15.2 95 89.4 32.0 45 136.5 48.8 95 183.6 65.7 45 230.7 82.5 95 277.7 99.4 46.3 15.8 97 91.3 32.7 47 138.4 49.5 97 185.5 66.3 47 232.5 83.2 97 279.6 100.0 48.4 40.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67.0 49 234.4 83.9 99 281.5 100.7 50 47.1 16.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84.2 300 282.5 101.0			_			_	_	-			***	-	-	221.3	79.1			-
38 35.8 12 8 88 82.5 29.6 38 129.9 46.5 88 177.0 63,3 38 224.1 80.2 88 271.2 96.0 37.7 13.5 89 83.8 30.0 40 131.8 47.2 90 178.9 64.0 40 226.0 80.8 90 273.0 97.7 41 38.6 13.8 91 85.7 30.6 141 132.8 47.5 191 179.8 64.3 42 227.8 81.5 92 274.0 98.0 42 39.5 14.1 92 86.6 31.0 42 133.7 47.8 92 180.8 64.7 42 227.8 81.5 92 274.9 98.3 40.5 14.5 93 87.6 31.3 43 134.6 48.2 93 181.7 65.0 43 228.8 81,8 93 275.9 98.7 44 14.4 14.8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 44 229.7 82.2 94 276.8 99.0 45.4 41.4 15.2 95 89.4 32.0 45 136.5 48.8 95 183.6 65.7 45 230.7 82.5 95 277.7 99.4 46.3 15.8 97 91.3 32.7 47 138.4 49.5 97 185.5 66.3 47 232.5 83.2 97 279.6 100.0 48.4 40.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67.0 49 234.4 83.9 99 281.5 100.7 50 47.1 16.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84.2 300 282.5 101.0																		
39   36.7   13.1   89   83.8   30.0   39   130.9   46.8   89   177.9   63.7   39   225.0   80.5   89   272.1   97.3   90.1   13.8   47.2   90.1   178.9   64.0   40.2   226.0   80.8   90.2   273.0   97.7   13.5   90.8   14.1   132.8   47.5   191   179.8   64.3   241   226.9   81.2   291   274.0   98.0   40.1   41.4		34.0	12.5	88	82.5	29.3	37	129,0	40.1				37	223.1	79.8	88		
40 37.7   13.5   90 84.7   30.3   40   131.8   47.2   90   178.9   64.0   40   226.0   80.8   90   273.0   97.7   98.0   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   64.3   99.0   179.8   179.		36.7	13.1	89	83.8	30.0	39	1 30,0	46.8		177.0	63.7	39	225.0	80.5			
42       39.5       14.1       92       86.6       31.0       42       133.7       47.8       92       180.8       64.7       42       227.8       81.5       92       274.9       98.3         43       40.5       14.5       93       87.6       31.3       43       134.6       48.2       93       181.7       65.0       43       228.8       81.8       93       275.9       98.7         44       14.4       14.8       94       88.5       31.7       44       135.6       48.5       94       182.6       65.3       44       229.7       82.2       94       276.8       99.0         45       42.4       15.2       95       89       432.0       45       136.5       48.8       95       183.6       65.7       45       230.7       82.5       95       277.7       99.4         46       43.3       15.5       96       90.4       32.3       146       137.5       49.2       196       184.5       66.0       246       231.6       82.9       195       277.7       99.4         47       44.3       15.8       97       91.3       32.7       47       138.4       49	40	37.7	13.5	30	84.7	30.3	40	131.8	47.2	90	178.9	64.0						
42       39.5       14.1       92       86.6       31.0       42       133.7       47.8       92       180.8       64.7       42       227.8       81.5       92       274.9       98.3         43       40.5       14.5       93       87.6       31.3       43       134.6       48.2       93       181.7       65.0       43       228.8       81.8       93       275.9       98.7         44       14.4       14.8       94       88.5       31.7       44       135.6       48.5       94       182.6       65.3       44       229.7       82.2       94       276.8       99.0         45       42.4       15.2       95       89       432.0       45       136.5       48.8       95       183.6       65.7       45       230.7       82.5       95       277.7       99.4         46       43.3       15.5       96       90.4       32.3       146       137.5       49.2       196       184.5       66.0       246       231.6       82.9       195       277.7       99.4         47       44.3       15.8       97       91.3       32.7       47       138.4       49	41				85.7	30.6	141			191	179.8	64.3	241	226 9	81.2			
44 41.4 14.8 94 88.5 31.7 44 135.6 48.5 94 182.6 65.3 44 229.7 82.2 94 276.8 99.0 45 42.4 15.2 95 89.4 32.0 45 136.5 48.8 95 183.6 65.7 45 230.7 82.5 95 277.7 99.4 46.1 15.8 97 91.3 32.7 47 138.4 49.5 97 185.5 66.3 47 232.5 83.2 97 279.6 100.0 48.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67.0 49 234.4 83.9 99 281.5 100.7 50.5 47.1 16.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84.2 300 282.5 101.0	42	39.5	14.1	92	86.6	31.0	42	133.7	47.8	92	180.8	64.7	42	227.8	81.5	92	274,9	98.3
45       42.4       15.2       95       89.4       32.0       45       136.5       48.8       95       183.6       65.7       45       230.7       82.5       95       277.7       99.4         46       43.3       15.5       96       90.4       32.3       146       137.5       49.2       196       184.5       66.0       246       231.6       82.9       296       278.7       99.7         47       44.3       15.8       97       91.3       32.7       47       138.4       49.5       97       185.5       66.3       47       232.5       83.2       97       279.6       100.0         48       45.2       16.2       98       92.3       33.0       48       139.3       49.8       98       186.4       66.7       48       233.5       83.5       98       280.6       100.4         49       46.1       16.5       99       93.2       33.3       49       140.3       50.2       99       187.4       67.0       49       234.4       83.9       99       281.5       100.7         50       47.1       16.8       100       94.2       33.7       150       141.2					87.6	31.3	43	134.6	48.2	93	181.7	65.0	43	228.8	81,8			
47 44.3 15.8 97 91.3 32.7 47 138.4 49.5 97 185.5 66.3 47 232.5 83.2 97 279.6 100,0 48 45.2 16.2 98 92.3 33.0 48 139.3 49.8 98 186.4 66.7 48 233.5 83.5 98 280.6 100.4 49 46.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67.0 49 234.4 83.9 99 281.5 100,7 50 47,1 16.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84.2 300 282.5 101.0	45							135.0	48.9				44	229.7	82.5			
47 44.3 15.8 97 91.3 32.7 47 138.4 49.5 97 185.5 66.3 47 232.5 83.2 97 279.6 100,0 48 45.2 16.2 98 92.3 33.0 48 139.3 49.8 98 186.4 66.7 48 233.5 83.5 98 280.6 100.4 49 46.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67.0 49 234.4 83.9 99 281.5 100,7 50 47,1 16.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84.2 300 282.5 101.0	46						-		-		-						-	
48 45.2 16.2 98 92.3 33.0 48 139.3 49.8 98 186.4 66.7 48 233.5 83.5 98 280.6 100.4 49 46.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67.0 49 234.4 83.9 99 28 1.5 100.7 50 47.1 16.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84 2 300 282.5 101.0	47	44.3	15.8			32.3		1 28.4	49.3	97	185.5	66.2	47	222.5	82.2		270.7	
49 46.1 16.5 99 93.2 33.3 49 140.3 50.2 99 187.4 67,0 49 234.4 83.9 99 28 1.5 100,7 50 47,1 16.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84 2 300 282.5 101.0	48	45.2	16.2	98				139.3	49.8	98	186.4	66.7	48	233.5	83.5	98		
50 47,1 16.8 100 94.2 33.7 150 141.2 50.5 200 188.3 67.4 250 235.4 84 2 300 282.5 101.0	49	46.1	16.5	99	93.2	33.3	49	140.3	50.2	99	187.4	67,0	49	234.4	83.9	99	281.5	100,7
Diff Dep Lat	50			_						200	188.3	67.4			_		_	
	· ntt	Lep	Lat	Diff	Dep	Lat	Dift	Dep	Lat	Dit	Dep	Lat	Dift	'Dep	Lat	Diff	l Dep	Lat

for 6 Points.

1. 500			12.4							-	-		-				
Dut	Lat	Dep	_	Lat	Dep	Ditt	Lat	-	Ditt		Dep	Diff			Diff	Lat	_
1	00,9	00.4		47,1		101	93,3	38.7	151	139 5	57,8	201	185.7	76.9	251	231.9	96.
2	01.8			48.0		02	94,2		52	140.4	58.2		186.6	77.3		232.8	96.
3	02.8		0.70	49 0	1000	03	95.2		53		58.0	03				233 8	96
4		01.5	10.7	49.9		04	96.1		54	142.3		04	188.5		- 1 / D N. / 1	234.7	97
5	04.0	01.9	55	50.8	21.0	05	97.0	40.2	55	143.2	59.3	05		_	55	235.6	97
6	05.5	92.3	56	51 7		106	97-9	40.6	156	144.1		206	190.3		256	236.5	98.
7	06.5	02.7	57	52.7		07		410	57	145.1		07	191.3		57	237.5	98.
8	97.4		58	53 6	22.2	08		41.3	. 58	146.0		and the same	192.2		58	238.4	98.
9	08.3	- 0	59		22.6	-09	1	41.7	59	146.9					59	239.3	99
10	09.2	03.8	60	55.4	23.0	10	101.6	42,1	60	147.8	_	10	194,0	_	60	240.2	99.
11	10.2	94,2	61	56.4	23.3	111	102.6	42.5	161	148.8		211	194.9		261	241.1	99
12	11.1	04,6	62		23.7	12	103-5	42.9	62	149.7		12	195.9	81.1	62	242,1	100,
13	12.0	05.0	63	58.2	24.1	13	104.4	43.2	63	150.6		13	196.8		63	243.0	100.
14		05-4	64	59.1	24.5	14	105.3		64	151.5		14	197.7		64	243.9	101,
15	F3.9	05,7	65	60.I	24.9	15	106,3	14.C	65	152.5	63.1	15	198.6		65	244.8	101
16		06.1	66	61.0	25.3	116	107.2	44.4	166	153.4	63,5	216	199.6	82.7	266	245.8	101,
17		06.5	67		25 6	17	1.801	44.8	67	154.3	63.9		200,5		67	246.7	102
18	16.6	06.9	68		26.0	18	109.0	45.2	68	155.2			201.4			247.6	
19		07.3	69		26.4	19	109,9	45.5	69	156.1			202.3		69	248.5	
20	18 5	07.7	70	64.7	26.8	20	1109	45.9	70	157,1	65.1	20	203,3	84.2	70	249.5	103
2.1	19.4	08,0	7.1	65.6	27.2	121	111.8	46.3	171	158.0	65.4		204.2		271	250 4	103
22		08.4	72	66.5	27.6	22	112.7	46.7	72	158.9	65.8	22	205.1	85.0	72	251.3	104
23		08.8	73		27,9		113.6		.73	159.8		23	206.0	85.3	73	252.2	104
24	22.2	09.2	74		28.3	24	114.6	47.5	74	160.8			207.0		74	253.2	104
25	23.1	09.6	75	69.3	28.7	25	115.5	47.8	75	161.7	67,0	25	107,9	86.1	75	254.1	105
26	24,0	10.0	76	70.2	29.1	126	116.4	48,2	176	162.6	67.4	226	208.8	86.5	276	255.0	105
27	24.9	10.3	77	71.1	29.5	27	117.3	48.6	77	163.5	67.7	27	209.7	86.9	77	255.9	
28		10,7	78	72.1	29.9	28	118.3	49.0	78	164.5	68,1		210.7			256.9	106.
29	26.8	II.I	79	73.0	30.2	29	119.2	49.4	79	165.4		29	210.6			257.8	
30	27.7	11.5	80	73,9	30.6	30	120.1	49.8	80	166.3	68.9	30	211.5	88.0	80	258.7	107
31	28.6	11.9	81	74.8	31.0	131	121.0	50.1	181	167.2	69.3	231	213.4	88.4	281	259.6	107.
32		12.2	82	75.8	31.4	32	122.0		82	168.2	69.7	32	214.4	88.8	82	260.6	
33	30.5	12.6	83	76.7	31.8	33	132,9	100000	83	169.1	70.0	33	215.3	89.2	83	261.5	108.
34	31.4	13.0	84		32.1	34	123.8	51.3	84	170.0	70.4	34	216.2	-	84	262.4	108
35	32.3	13.4	85	78.5	32.5	35	124.7	51.7	85	170.9	70.8	35	217.1	89.9	85	263.3	109
36	33.3	13.8	86	79.5	32.9	136	125.7	52.0	186	171.9	71.2	236	218.0	90.3	286	264.2	109
37		14.2	87	80.4	33.3	37	126.6		87	172.8		37	219.0	90.7	87	265.2	109
		14.5	88	81,3	33.7		127.5	52.8	88	173.7	72.0	38	219.9	91.1	88	266,1	110
		14,9	89	82.2	34.1	39	128.4	53.2		174.6		39	220.8	91,5	89	267.0	110
40		15.3	90	83.2	34.4	40	129,4	53.6	90	175.6	72.7	40	221.7	91.9	90	267.9	111.
41	1000000000	15.7	QI		34.8		130,3	54.0	191	176.5	73.1	241	222.7	92.2	-	268.9	
42		16.1	92	85.0	35.2	42	131.2			177.4			223.6			269.8	
43		16.5	93	85.9	35.6	43	132,1			178.3			224.5		93	270.7	112
44	40.6	16.8	94	86.9	36.0	44	133.0			179.2	74.2	44	225.4	93.4	94	271.6	112
45	41.6	17.2	95		36.4		134.0		95	180.2	74.6	45	226.4	93.8	95	272.6	112
46	42.5	17,6	The state of the state of	-	36.7	THE RESERVE	134.9	-	196	181.1	75.0	246	227.3	_	296	273.5	112
47	43.4	18.0			37.1		135.8	56.2	97	182.0			228.2			274.4	
48	44.4	18.4	98		37.5	48	136.7	56.6	98	182.9			229.I			275,3	
49		18.8		91.5	37.9	49	137.7		99	183.9	76.2	49	230.1	95,3		276.3	
50		19.1	100	92.4	38,3	150	138.6	57.4		184.8	76.5	250	231.0	95.7	300		
	-	Lat	1-	1	1		Dep							Lat			L

for 6 Points.

									1483		11 11 11 11	2000				7210	
Dill	Lat	Det	Dift	Lat	Dep	[Ditt]	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep
1	00,9	00.4	51		21,8	101	91.3	-		136.5		201	181.7	85:9	251	226 9	107.3
2	01.8		52	47,0	22.2	02	92,2		-	137.4		02	182.6	86 4	52	227,8	
3	02.7		53	47.9		03		44.0		138,3			183.5	86.8		228.7	
4	03.6	02.1		48.8		04		44.5	54	139 2		04	184.4	87.2		229.6	
5	04.5		55		23.5	05	-	44.9	55				186.2	88.1	55	_	-
6	05.4	03.0	56		23.9	106		45.8	156	141,9		07	187.1	88.5	256 57	231.4	1
7 8		03.4	58		24.8	08	97.6		58	142.8	67.6		188.0	88.9	58	232.3	110.3
9		03.8	59		25.2	09		46.6	59		68,0		188.9	89.4	59	234.1	110.7
10		04,3	60		1	.10		47.c	60	144.6	68.4	10	189.8	89 8	60	235.0	
11	09.9	04,7	61	55.1	26.1	111	100.3	47.5	161	145.5	68.8	211	190.7	90.2	261	235.9	111.6
12		05.1	62					47.9		146.4	69.3		191.6		62	236.8	112.0
13		05.6	11 0			11 -		48,3			69.7	13			63	237.7	1 31
14	12.7							48.7			70.1	14		91,5	64	238.6	10. 20 14.
15	-	-			27.8	-		49.2			70.6			91.9	05	239.5	113.3
16		96.8	66	132.1			104.	49.6	166		71.0		1 3		266	240.4	1 3 / 1
18		07.3			28.6	11 0	105.1	50.5	67	151.0	71.4			1	11. 60	241.3	
19		07.7	69		1 29.1			50.9	11 -		72.3		1	1	11	242,2 243.1	1
20		38.6	11	1 .	3 29.9		108.			153.		11	1 0 0		70	244.0	1 - 1
21	10.0	09.0		-	_		-	4 51.7		-	73.1		-		11-	245.0	-
22		09.4	11		1 30.8	111	1	3 52.2		155.		11	200,7			245.9	
23		09.8			31.			2 52.6	110000	156.			201.6	1 2	11		116.7
24	1	10.3		66.	31.6		112.		11	157,	3 74.4	24	202.5	95.8	74	247.7	117.2
25	22.6	10.7	75	67.	8 32.	25	113.	53.5	75	158.	2 74.8	25	203,4	96.2	75	248.6	117.6
26	23.5	11.1	76	68.			113.		176		1 75,3		204.3	96.6	276	249.5	118.0
27		11.5	11 0		10			8 54.			0 75.7	11					118.4
28		12.0					115.		11		9 76.1	11	206.1	13,3		251.3	
29		12.4			. 33		116.	100			7 77.0		107,9			252.2	1 200
30		-	11-	-	-	_	118.		-	-	_	-	-	-		-33.	119.7
31		13.7	111	1,3,				3 56.4			5 77.8		209.7		11 0	254.0	
33		14.1			100		120.	2 56.9			4 78.2		210.6				
34		and the same	11 0	75.					84	166.			211.9		11 0		
35			11 0		8 36.		122.	2. 10. 10. 10.	. 0	167.		11 1	212.4	100.5	85	257.	
36		15.4	86	77.	7 36.	8 136	122,	9 58.2	186	168.	1 79,5	236	213.3	100.0	286		
37	33.4	15.8	87	7 78.	6 37.2	2 37	123.		87	169.	80,0	37		101.3	87	259.4	
38	34.4	16.2	88		6 37.6	38	124.	7 59.0	88	169.	9 80.4	38	215.1				3 123.1
39		16.7			5 38,		125.	6 59.4	89	170.	8 80.8	39	216.0			261.	123.6
40	30.2	17.1			4 38.	-				171.	_		216.9			-	124.0
41	37.1	17,5	91	82.	3 38.9	141	127.	4 60.	191	172.	6 81,7	24	217.8	103.0	11		124.4
42	38.0	18.0	92	83.	39.	42	128.	4 6 6 7	92	173.	82.1	1	218.7			263.	124,9
43	30.9	18.4	93	85	39.8	44	130,	61.6	94	174.	82.0	4	220.5				8 125.3 7 125.7
44	49.7	19.2	94	85.	40.6	45	131.	62.0	95	176.	83.6	4		104.8			6 126.1
46	1 4 4				41.0		132.0			177.	82.8	246	222.4				6 126.6
47	41.0	19.7			41.5		122.0	62.0	97	178	1 84.2	4	223.				5 127.0
48	42.4	20,5	98		41.9	48	133.	8 63.3	98	179.	0 84.7	48	224.2	106.0	98	260	4 127.4
49	44.3	21.0	99		42,	49	134.	7 63.7	99	179.	9 85,1	49	225.	106.	5 99	270.	3 127.8
50		21.4			42.8	150	135.	6 64.1	200	180.	8 8 5.5	250	226.			271.	2 128.3
Diff	L'eo	Lat	Dif	De	Lat	Dift	Dep	Lat	Dit	Dep	Lat	Di	d Dep	1 1.a	Di	ft De	Lat
-			11				AMEL E	112,72		57th 1 - 2 3		ber i		V 1000	-		-

for 5 3/4 Points.

## Difference of Latitude and Departure for 21 Points. 67

2 4.	Lat	Deu	1Dit	·L	at 1	Dep	Dift	Lat	Depl	Dift	Lat	Devl	Diff	Lat.	Dep	(Dift	Lat	Dep
	-	_	-	-	-			89,1	-	-		-		177.3	94-7	251 2	21.	118 0
- 1	00.9	11 15 15 10	51		1000		101				133.2			178.2	95.2			118.7
	01.8			100.00	60 may 1	24,5	02	90.0	48.	7.7	11.7			179.0				119.2
	02.6					25.0	03	100 The 100 Stap	49.0		134.9		-	179 9	96.1			119.7
	03.5			1.4			04	92.6			136.7		05	180.8	96.6			120.1
5	C4·4	-	-		_	2 5.9	-	-	-	12.0		-	-		-		-	-
6	05.3		110			26.4	106	93.5		156	137.6			181.7	97.1			120.6
7		03.3			-	26.9	07	94.4			138.5		07	182.6	97.5			121.1
8	the same of the same	03.8				27.3	08		50.9		139.4	1000	08	183.5	98.0			121.6
9		04.2				27.8	09		51.4	59	140,2		09	184 3	98.5			122.0
10	08.8	04.7	41-	- 1-	_	28.3	10	-	51.8	-	141.1	75.4	10	-	90,9	-	29.3	-
11	09.7	05.2	6:	53	3.8	28.7	111		52.3	161		75.9	211	185,1	99.4			1230
12		05.		13		29.2	12		52.8		142.9		12	187:0				123.4
13		06.				29,7	13	99-7	53.2		143.8		13		100.4			123.9
14	1	06,				30.2	14	100.5	12.0	64	144.6				100.8		-	124.4
15	13.2	07.	6	5 5	7.3	30.6	15	101.4	54.2	65		77.7	15	_	101.3	-	233.7	
16		107.		5 5	8.2	31.1	116	102.3	54.7	166	146.4	78.2		190.5	101.8	266		125,3
17		08.		- 12		31.6		103.2	55.1		147.		17	1 1 1 1	102.2			125.8
18	15.9	08.			0.0	32.0		104.1				79.2			102.7			126.3
19	16.8	3 09,	11			32.5	19	105.0		69	149.1	179.6			103.2			126.7
20	17.6	09,	4 7	0 6	1.7	33.0	20	105.8	56.5	70		80.1	20	194.0	103.7	70	238.1	127.2
21	18.	5 09.	9 7	1 6	2.6	33.5	121	106.7	57.0	171	1 50.	8 80.6	221	194.9	104,1	271	239.0	127.7
22	1 . 1 . 57	4 10.		_   -	6 1 1 1 1	33.9	22	107,6		72	151.	7 81.0	22	195.8	104.6	72	239.9	128,2
23	20.	3 10,	8 7			34.4		108.		11	152.	6 81.5	23	196.	105.1	73	240.8	128.6
24		2 11.				34,9	24	109.	58.4	74	153.	5 82.0	24	197.	105-	74	241.7	129 1
25	22.	1 11.	8 7	5 6	6.2	35.3	25	110.	58,9	75	154.	3 82.5	25	198.	106.	75	242.5	129.6
26	22.	Q 12.	3 7	6 6	7.0	35,8	126	111.	59.4	176		2 82.9		199.	106.	276	243.4	130.0
27		8 12.		7 6	7.9	36.3	27	112.			156.	1 83.4	27		107.0			130.5
28		7 13.				36.8			60.		157.	0 83.9	28	201.	1 107.	1 78	245.2	131.0
29		6 13.	11 -			37.2		113.	8 60.8	79	157.	9 84.	29	202.	107.			131.5
30	26,	5 14.	1 8	0 7	70.6	37.7	30	114.	7 61.	80	158.	8 84,8	30	202.	9 108.	4 80	247.0	131.9
31		3 14,	6 8	1	71.4	38.2	131	115.	5 61.	181	159.	6 85.	231	203.	7 108.	281	247.8	132,4
32		2 15	110	2 7	72.1	38.6	32		4 62.	8:	160.	5 85.8	32		6 109.	3 82	248.	132.9
33		1 15	5 8	3 7	73.2	39.1	33		3 62.		,161.	4 86 :	2 33	205.	5 109.	8 83	249.6	133.3
34		0 16	0 8	4 7	74.1	39.6	34		2 63	1 84	1 162.	3 86.	7 34	206.	4 110.			5 133.8
35	30.	9 16	5 8			40.		119.	1 63.	8	163.	2 87.	2 3	207.	3 110.	7 85	251.	4 134.3
36		8 17		2		40.	-	-	0 64.	181	6 164	1 87.	6 23	208.	2 111.	2 286	252.	3 134.8
37		6 17	4 8	7 1	76.	41.	37	120.		5 8	164.	9 88.	1 3	7 209.	0 111.	7 87	253.	1 135.2
38	22.	5 17	0 8	8	77.6	41.	38	121,	7 65.		8 165.	8 88.	6 3		9 112.	1 88	254.	0 135.7
39	124.	4 18	4 1	39	78.	5 41,	39	122.	6 65.	5 8	166.	7 89.	1 3	210.	8 112.	6 1 9	254.	9 1 30.2
40	35.	3 18	8 9		79.	4 42.	4 40	123.	5 66.		167	.6 89,	5 4		7 113.	1 90	255.	8 136.6
41		2 19				42.			4 66,			.5 90.	0 24	1 212	6 113.			7 137.1
42	27	0 19	8		81.	1 43.	4 42	125	2 66.	9 9	2 160	.3 90.	5 4		4 114		257.	5 137.6
4:	27	9 20	3			43.			1 67,	4 9	3 170	.2 90	9 4		3 114	5 93	258.	4 138.1
44		8 20				9 44.			0 67.			.1 91.			2 115			3 138.5
4		7 21	.2			8 44.		127	9 68.	3 9		0 91.			1 115	4 95	260	2 139.0
46		6 21				7 45.		128			-	.9 92.		-	0 115			1 139,
4		5 22			8.	6 45.			7 69,		7 172	,8 92			9116	4 97	262	0 139
4		3 22		98	86	4 45.	2 4	8 120	5 69	7 9	8 174	6 93	3 4	8 218	7 116	.8 98	262	8 140.
4		3			0	114.	4	O Tax	4 70	2 9	9 17	.5 93	.8 4		.6 117	3 99	262	7 140.
	9 42	2 2 2	. 11	991	87	2140.	OH A											
5	9 43	1 23	6 1	99	88.	3 46.	6 4	0 1 22	3 70	7 20	0 176	5.4 94	.2 25			.8 300	264	.6 141,
5	9 43	1 23	,6 1	00	88,	2 47.	1 15	0 132	.3 70.	7 20	0 176	5.4 94	.2 25		.5 117	.8 300	264 t De	.6 141,

for 5½ Points.

3		Pares.	1									-						18 7 19 1
1	Dift	Lat	Dep	Dia	Lat	Dep	Dift		-	DiA	Lat	-	Diff	Lat	Dep	Dift	Lat	Dep
1	1	00.9	00.6	51								77.6	100					
5 04-3 03-6				-				87.5	52.4					100000000000000000000000000000000000000	-	1		
5 0.4.3 0.6.6 5.5 4.7.2 18.5.3 0.5 90.1 54.0 55.1 32.0, 19.7.7 0.5 175.8 105.4 55.8 18.7.1 11.6 0.5 17.9 1.5 18.0 19.8.1 11.6 0.5 17.9 18.8 19.9 19.3 19.7 19.8 19.8 19.8 19.8 19.8 19.8 19.8 19.8	3	1200	1 21 21			1 0					1000							The state of the s
6 05.1 03.1 56 48.0 24.8 106 90.9 54.5 156 133.8 80.2 206 776.7 105.9 256 219.6 131.7 7 06.0 03.6 7 48.9 29.3 07 91.8 55.0 57 134.7 80.7 07 177.5 106.4 57 2120.4 13.9 07.7 04.6 59 50.6 30.9 09 93.5 56.0 59 1 16.4 81.7 09 179.3 107.4 59 322.1 13.2 10 08.6 05.1 00 51.5 30.8 10 04.3 56.5 60 137.2 82.2 110 100.4 05.7 6 1 52.3 31.4 111 95.2 57.0 161 138.1 83.7 10 180.1 107.9 60 23.2 13.1 12 95.1 57.6 62 138.9 83.3 110 107.9 60 23.2 13.4 111 95.2 57.0 161 138.1 83.7 211 181.0 108.4 261 223.9 134. 121 95.2 57.0 161 138.1 83.7 211 181.0 108.4 261 223.9 134. 121 95.2 57.0 161 138.1 83.7 211 181.0 108.4 261 223.9 134. 13 15.0 07.2 64 54.9 33.9 11 97.8 58.6 64 140.7 84.3 13 18.5 100.6 63 225.6 135. 15 13.9 07.7 65 55.8 83.3 15 98.6 59.1 65 142.4 85.3 114 183.5 110.0 62 225.7 13.6 16 13.0 07.2 65 55.8 83.3 15 98.6 59.1 65 142.4 85.3 116 185.3 111.0 66 225.7 131.9	10				1.											1000		1
0   0   0   0   0   0   0   0   0   0	-	04.3	02.0	1	-	-	-	90.1	54 0		_	_	-					
10   05   05   04   1   58   49   72   29   80   92   615   55   58   13   50   9   17   93   10   40   59   50   6   30   30   30   90   93   55   56   60   137   32   32   11   33   10   30   30   30   30   30		-		11 -										11 11 11 11	- 2		100 C	
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11	3 1 2			11 2 2	1-	1		/ 100 Table 10				0	11					1 33 -
12 10,3   05.2   62   53.2   31.9   12   96.1   57.6   62   138.9   83.8   13   182.7   109.5   63   224.7   134.1   12.0   107.2   64   54.9   32.9   14   97.8   58.6   64   140.7   84.3   14   183.5   110.0   65   227.3   136.1   15   12.9   07.7   65   55.8   33.4   15   98.6   59.1   65   141.5   84.8   15   184.4   110.5   65   227.3   136.1   17   14.6   68.7   76   57.5   34.4   71   100.4   66.1   67   143.8   53.8   17   185.1   110.0   65   227.3   136.1   13   15.4   09.5   68   58.3   35.0   18   101.2   60.6   68   144.1   86.3   17   185.1   111.0   67   229.1   13.0   17.2   10.3   70   60.0   36.0   20.2   96.1   70   70   145.8   87.4   20   188.7   113.1   72   233.0   13.3   13.3   13.2   13.0   17.2   10.3   70   60.0   36.0   20.2   96.1   70   70   145.8   87.4   20   188.7   113.1   72   233.6   13.3	-	-	-	-	13-	-	-	-		-	-		-			-	-	
13 1.1.2   60.7   63   54.0   32.4   13   96.9   58.1   63   13.9   83.8   13   13.8.2   71   10.9.5   64   22.6   13.5   12.9   97.7   65   55.8   33.4   15   98.6   59.1   65   141.5   84.8   15   184.4   110.5   65   227.3   13.6   13.7   08.2   66   56.6   33.9   116   99.5   59.6   166   142.4   85.3   11.6   111.6   65   227.3   13.6   13.8   1	1		1 3 .	11	13.					11 /		82.7	113					1
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34       29.2       17.5       84       72.0       43.2       34       114.9       68.9       84       157.8       94.6       34       200.7       120.3       84       243.6       146         35       30.0       18.5       86       73.8       44.2       136       116.6       69.9       186       159.5       95.6       236       202.4       121.3       286       245.3       147         38       31.7       19.0       27       74.6       44.7       37       117.5       70.4       87       160.4       96.1       37       203.3       121.8       87       246.2       147         38       32.6       19.5       88       75.5       45.2       38       118.4       70.9       88       161.2       96.6       38       204.1       122.3       88       247.0       148         39       33.5       20.0       89       76.3       45.7       39       119.2       71.4       89       162.1       97.1       39       205.0       122.8       89       247.0       148         40       34.3       20.6       90       77.2       46.3       40       120.1       7	32	27.				3 42.	11 -			- 11	156.		- 11		-1 -		-	9 144.
35 30.c 18.0 85 72.9 43.7 35 115.8 69.4 85 158.7 95.1 35 201.6 120.8 85 244.4 146.3 30.9 18.5 86 73.8 44.2 136 116.6 69.9 186 159.5 95.6 236 202.4 121.3 286 245.3 147.3 117.5 70.4 87 160.4 96.1 37 203.3 121.8 87 246.2 147.3 117.5 70.4 87 160.4 96.1 37 203.3 121.8 87 246.2 147.3 117.5 70.4 87 160.4 96.1 37 203.3 121.8 88 247.0 148.3 118.4 70.9 88 161.2 96.6 38 204.1 122.3 88 247.0 148.3 119.2 71.4 89 162.1 97.1 39 205.0 122.8 89 247.9 148.4 135.2 21.1 91 78.1 46.8 141 120.9 72.5 191 163.8 98.2 241 206.7 123.9 90 248.7 149.2 250.4 150.4 250.4 250.4 250.4 250.4 150.4 250.4 250.4 250.4 250.4 150.4 250.4 250.4 250.4 250.4 150.4 250.4	33	28.	3 17.			1							- 11					11-43
36 30.9 18.5 86 73.8 44.2 136 116.6 69,9 186 159.5 95.6 236 202.4 121.3 286 245.3 147 37 31.7 19.0 87 74.6 44.7 37 117.5 70.4 87 160.4 96.1 37 203.3 121.8 87 246.2 147 38 32.6 19.5 88 75.5 45.2 38 118.4 70.9 88 161.2 96.6 38 204.1 122.3 88 247.0 148 40 34.3 20.6 90 77.2 46.3 40 120.1 72.0 90 163.0 97.6 40 205.8 123.3 90 248.7 149 42 36.0 21.6 92 78.9 47.3 42 121.8 73.0 92 164.7 98.7 42 207.6 124.4 92 250.4 150 43 36.9 22.1 93 79.8 47.8 43 122.7 73.5 93 165.5 99.2 43 208.4 124.9 93 251.3 150 43 37.7 22.6 94 80.6 48.3 44 123.5 74.0 94 166.4 99.7 44 209.3 125.4 94 252.2 15.4 45 38.6 23.1 95 81.5 48.8 45 124.4 74.6 95 167.3 100.2 45 210.1 125.9 95 253.0 15 46 39.5 23.6 96 82.3 49.3 146 125.2 75.0 196 168.1 100.7 246 211.0 126.4 296 253.9 153 46 12.2 24.7 98 84.1 50.4 48 126.9 76.1 198 169.8 101.8 48 212.7 127.4 98 255.6 15 49 42.0 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15 50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.5	-					1.3					1 57.	8 94.						
37 31.7 19.0 87 74.6 44.7 37 117.5 70.4 87 160.4 96.1 37 203,3 121.8 87 246.2 147 88 32.6 19.5 88 75.5 45.2 38 118.4 70.9 88 161.2 96.6 38 204.1 122.3 88 247.0 148 40 34.3 20.6 90 77.2 46.3 40 120.1 72.0 90 163.0 97.6 40 205.8 123.3 90 248.7 149 42 36.0 21,6 92 78.9 47.3 42 121.8 73.0 92 164.7 98.7 42 207.6 124.4 92 250.4 150 43 36.9 22.1 93 79.8 47.8 43 122.7 73.5 93 165.5 99.2 43 208.4 124.9 93 251.3 150 43 37.7 22.6 94 80.6 48.3 44 123.5 74.0 94 166.4 99.7 44 209.3 125.4 94 252.2 15.4 45 38.6 23.1 95 81.5 48.8 45 124.4 74.6 95 167.3 100.2 45 210.1 125.9 95 253.0 15 40 3 24.2 97 83.2 49.9 47 126.1 75.6 97 169.0 101.2 47 211.9 126.9 97 254.7 15 48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15 99 22.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.5	-	-	_	-11-			-   -	-		_	_	7 95.		-	-	-	_	4 140.
38       32.6       19.5       88       75.5       45.2       38       118.4       70.9       88       161.2       96.6       38       204.1       122.3       88       247.0       148         39       33.5       20.0       89       76.3       45.7       39       119 2       71.4       89       162.1       97.1       39       205.0       122.8       89       247.9       148         40       34.3       20.6       90       77.2       46.3       40       120.1       72.0       90       163.0       97.6       40       205.8       123.3       90       248.7       149         41       35.2       21.1       91       78.1       46.8       141       120.9       72.5       191       163.8       98.2       241       206.7       123.9       291       249.6       149.6         42       36.0       21,6       92       78.0       47.3       42       121.8       73.0       92       164.7       98.7       42       207.6       124.4       92       250.4       150.4         43       36.9       22.1       93       79.8       47.8       43       122.7       <	130	30.	9 18.	211		61	11	1		- 11 -	1 33					214	1-43.	-
39       33.5       20.0       89       76.3       45.7       39       119       2       71.4       89       162.1       97.1       39       205.0       122.8       89       247.9       148         40       34.3       20.6       90       77.2       46.3       40       120.1       72.0       90       163.0       97.6       40       205.8       123.3       90       248.7       149         41       35.2       21.1       91       78.1       46.8       141       120.9       72.5       191       163.8       98.2       241       206.7       123.9       291       249.6       149         42       36.0       21.6       92       78.0       47.3       42       121.8       73.0       92       164.7       98.7       42       207.6       122.4       92       250.4       150         43       36.9       22.1       93       79.8       47.8       43       122.7       73.5       93       165.5       99.2       43       208.4       124.9       93       251.3       150         45       38.6       23.1       95       81.5       48.8       45       124.4 </td <td></td> <td></td> <td></td> <td>11 0</td> <td>- 1</td> <td></td> <td></td> <td></td> <td></td> <td>"   - :</td> <td></td> <td></td> <td>-10</td> <td>0</td> <td></td> <td>11 0</td> <td>0</td> <td></td>				11 0	- 1					"   - :			-10	0		11 0	0	
40 34.3 20.6 90 77.2 46.3 40 120.1 72.0 90 163.0 97.6 40 205.8 123.3 90 248.7 144  41 35,2 21.1 91 78.1 46.8 141 120.9 72,5 191 163.8 98.2 241 206.7 123.9 291 249.6 149  42 36.0 21,6 92 78.9 47.3 42 121.8 73.0 92 164.7 98.7 42 207.6 124.4 92 250.4 150  43 36.9 22.1 93 79.8 47.8 43 122.7 73.5 93 165.5 99.2 43 208.4 124.9 93 251.3 150  44 37.7 22.6 94 80.6 48.3 44 123.5 74.0 94 166.4 99.7 44 209.3 125.4 94 252.2 15  45 38.6 23.1 95 81.5 48.8 45 124.4 74.6 95 167.3 100.2 45 210.1 125.9 95 253.0 15  46 39.5 23.6 96 82.3 49.3 146 125.2 75.0 196 168.1 100.7 246 211.0 126.4 296 253.9 153  47 40.3 24.2 97 83.2 49.9 47 126.1 75.6 97 169.0 101.2 47 211.9 126.9 97 254,7 153  48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15  49 42.0 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15  50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 155	3	32	0 19.	5	0 75	5 45.	3 3									8 8	247.	148.
41 35,2 21.1 91 78.1 46.8 141 120.9 72,5 191 163.8 98.2 241 206.7 123.9 291 249.6 149.9 2 36.0 21,6 92 78.9 47.3 42 121.8 73.0 92 164.7 98.7 42 207.6 124.4 92 250.4 150.4 37.7 22.6 94 80.6 48.3 44 123.5 74.0 94 166.4 99.7 44 209.3 125.4 94 252.2 15.4 45 38.6 23.1 95 81.5 48.8 45 124.4 74.6 95 167.3 100.2 45 210.1 125.9 95 253.0 15.4 46 39.5 23.6 96 82.3 49.3 146 125.2 75.0 196 168.1 100.7 246 211.0 126.4 296 253.9 15.4 40.3 24.2 97 83.2 49.9 47 126.1 75.6 97 169.0 101.2 47 211.9 126.9 97 254,7 15.4 48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15.5 99.2 42.0 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.5 15.5 15.5 15.5 15.5 15.5 15.5 15			5 20.									97.				2 0	0 248	7 140.
42       36.0       21,6       92       78.9       47.3       42       121.8       73.0       92       164.7       98.7       42       207.6       124.4       92       250.4       150.4       150.4       150.5       150.2       150.5       150.2       165.5       16	4	_	_					-		-	-		_	_	_	- Inches		
43 36.9 22.1 93 79.8 47.8 43 122.7 73.5 93 165.5 99.2 43 208.4 124.9 93 251.3 156 44 37.7 22.6 94 80.6 48.3 44 123.5 74.0 94 166.4 99.7 44 209.3 125.4 94 252.2 15 45 38.6 23.1 95 81.5 48.8 45 124.4 74.6 95 167.3 100.2 45 210.1 125.9 95 253.0 15 46 39.5 23.6 96 82.3 49.3 146 125.2 75.0 196 168.1 100.7 246 211.0 126.4 296 253.9 153 47 40.3 24.2 97 83.2 49.9 47 126.1 75.6 97 169.0 101.2 47 211.9 126.9 97 254.7 15 48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15 49 42.0 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15 50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 150		35	2 21.		78	40.	141											
44 37.7 22.6 94 80.6 48.3 44 123.5 74.0 94 166.4 99.7 44 209.3 125.4 94 252.2 15. 45 38.6 23.1 95 81.5 48.8 45 124.4 74.6 95 167.3 100.2 45 210.1 125.9 95 253.0 15. 46 39.5 23.6 96 82.3 49.3 146 125.2 75.0 196 168.1 100.7 246 211.0 126.4 296 253.9 15. 47 40.3 24.2 97 83.2 49.9 47 126.1 75.6 97 169.0 101.2 47 211.9 126.9 97 254.7 15. 48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15. 49 42.0 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15. 50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.			0 21,		2 70	8 47	8 4											
45 38.6 23.1 95 81.5 48.8 45 124.4 74.6 95 167.3 100.2 45 210.1 125.9 95 253.0 15 46 39.5 23.6 96 82.3 49.3 146 125.2 75.0 196 168.1 100.7 246 211.0 126.4 296 253.9 153 47 40.3 24.2 97 83.2 49.9 47 126.1 75.6 97 169.0 101.2 47 211.9 126.9 97 254.7 153 48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15 49 42.0 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15 50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.		30.	7 22	6 0	4 80	6 48					156	4 00						
46 39.5 23.6 96 82.3 49.3 146 125.2 75.0 196 168.1 100.7 246 211.0 126.4 296 253.9 153 47 40.3 24.2 97 83.2 49.9 47 126.1 75.6 97 169.0 101.2 47 211.9 126.9 97 254,7 153 48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15 49 42.0 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15 50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.			6 22		5 81	. 5 48.	8 4									- 11		
47 40.3 24.2 97 83.2 49.9 47 126.175.6 97 169.6 161.2 47 211.9 120.9 97 254,7 15 48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15 49 42.6 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15 50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.	1		-	-				-	_		-			-		_		-
48 41.2 24.7 98 84.1 50.4 48 126.9 76.1 98 169.8 101.8 48 212.7 127.4 98 255.6 15 49 42.c 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15 50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.	140	139.			7 82	2 40	0 47	126	175	6 0	160						7 254	7 152
49 42.c 25.2 99 84.9 50.9 49 127.8 76.6 99 170.7 102.3 49 213.6 128.0 99 256.5 15 50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.								126	9 76.	08	160	8 101	8 4	212.	7 127	4 0	8 250	6 152
50 42.9 25.7 100 85.8 51.4 150 128.7 77.1 200 171.5 102.8 250 214.4 128.5 300 257.3 15.								127.	8 76.	6 00	170.	7 102.	3 4	217.	6 128.	0 9	9 256	5 153
			9 25.	7 10	0 85	8 51.											0 257	3 154
																	otropodia.	_

for 5 4 Points.

## Difference of Latitude and Departure for 3 Points. 69

_					0 1	D:Al	1	IDa. I	D. #	· Co.	Den	m:a	Lat.	Det	MD:A	1 7	.0
DA	Lar		Diff	Lai	-	Dilt			Ditt		Dep	-		Dep	Dift	_	Dep
1	00.8	00,6	51	42.4		101	84.0		151	125.5	83.9		167.1				139.4
2	01.7	01.1	52	43.2		.02	84.8	17 Y 6.1	52	120.4	84.4	02		112.2		209 5	
3	02.5	01.7	53	44.1		03	85.6		53	127.2	85.c	04	Service Services	112.8	and the second		140.5
4	03.3	02.2	54	44.9		05	86.5		54	128.0	86 1	05		113.9	54	211.2	
-5	C4-2	02.8	55	_	30.6	-		58.9	-		86.7	-		-	-		
		03.3	56	46.6	-	106	88.1		158	129.7	87.2	07	171.3	115.0	256	1	142.2
7	1 2	03.9	57	48.2	31.7	08	80.8	60.0	57	131.4	87.8	08	172.9			213.7	
	1.00	04.4	59		32.8	09			59	132.2	88.3	09	173,8				
10		05.6	60	49,9		10	91.4	61.1	60	133.0	88.9	10	174.6				144.4
-	-	06.1	6:	-	33.9	111	92.3	61.7	161	133.8	89 4	211	175.4	117.2	261	217.0	145.0
11	1 -	06,7	62		34.4	12	93.1	16	62	134.7	90.0	12	176.2			217.8	
13		07.2	63		35.0	13	93.9			135.5	90.5	13	177.1	118.3			
14		07.8	64		35,6	14	94.8	63 3	64	136.3	91.1	14	177.9		64	219.5	146.7
15	12.5	28.3	65	54 0	36.1	15	95.6	63.9	65	137.2	91.7	15	178.7	119.4	_	220.3	147.2
16	13.3	08.9	66	54.9	36.7	116		64.4	166	138.0	92.2	216		120.0			
17		09.4	67	55,7		17		65.0		138.8	92.8	17	180.4			222.0	
18	15.0	10.0	68		37:8	18		65.5	68	139.7	93,3	18	181.2			222 8	
19	1 -	10,6	1 59	57.4	38.3	19	98.9	66.1	70	140.5	93.9	19	182.1		11		
20	16.6	11.1	70	58.2	38.9	20	99.8		-	141.3	94.4					214.5	150.0
21		11.7	71		39.4	121	100.6	67,2	171	142.2	95.0	221	183.7			225.3	150.5
22		13.2	72		40.0	22	101.4	68.0		143.0	95.5	22	184.6	123.9	72	37	151.1
23	and the same	12.8	73		40.6	23	102.3		73	143.8	96.7	24	186,2			227 0	0 1
24		13.9	74		41.7	25	103.9			145.5	97.2	25		125,C		228.6	
25	-	-	76	-	-	_	104.8			146.3	97.8	226		125.5	-		_
26	1		77	63.2	42.2	11	105.6		77	147.1	98.3	11		126.1		230.0	153.3
28		15,0			43.3	28	106.4		78	148.0	98.9			126.7	78		154.4
29		16.1	79		43.9	29	107,2		79	148.8	99.4	29		127.2	79	231.9	
30		10	1 4		44.4	30			80	149.6	100.0	30	191.2	127.8	80	232.8	155.5
31	-	17.2	81	_		131	108.9	72.8	181	150.5	100.5	231	192.0	128,3	281	233.6	156.1
32		17.8	11 0		45.6	32	109.7		82	151.3	1.101	32	192.9	128.9	82	234.4	156.7
33		18.3			45.1	33	110.6	73.9			101.7			129 4	83	235.3	157.2
34		18.9			46.7	34	111.4	4.7.	84		102.2		1	130.0		236,1	
35		1 19.4	85	70.9	47.2	35	112.2	75.0	-	153.8		-	195.4	-	85	236.9	-
36	29,			1/		136	113.1		186		103.3			131.1		237.8	
37	30.	20.6	87		48.3	37	113.9	76.1	87	155.5	103.9	37	197.0	131.7	87	238.6	160.0
38		21.1	88	73.2	48.9	38	114.7	70.7	88	156.3	104.4	30	197.9	132,2	80	239.4	160.5
39		4 21.7	89	74.9	49.4	39	115.0	77.2	09	157.1	105.5	40	100.5	122.2	90	241.1	161.1
40		22.2			50.0					0.0	106.	241	-99.3	- 33.3	201		-6-
41	34.	1 22.8	91	75.7	50 6	141	117.2	78.3	191	158.8	106.7	42	201.2	133.9	102	242.8	161.7
42	34.	23.3	92		51.1	42	118.1	70.9	92	160.4	107.2	43	202.0	135.0	93	242.6	162.8
43		23,9			51.7	43	110.9	80.0	94	161.3	107.8	44	202.8	135.5	94	244.4	163.3
45		25.0			52.8	45	120.5	80.5	95	162.1	108.3	45	203.7	1 36.1	95	245.2	163.9
46		25.6			53.3		127.4	81.1	106								164.4
		26.1	97	180.	6 52.0	47	122.2	81.7	97	163.8	109.4	47	205.3	137.2	97	246.9	165.0
48		26.7	98	81.	5 54.4	48	1123.0	82.2	1 98	164.6	110.0	40	200.2	137.8	98	247.7	7 165.5
49	40.	27.2	11 00	182	alee c	1 40	1122.0	182.8	11 99	105.4	1110.4	49	1207.0	138.5	99	248.	51166.1
53		6 27.8	1100	82	1 55.6	1 50	124.7	183.3	1200	166.	111.	1 250	207.8	138.0	300	249.4	4 166.7
Ci		La	Di	De	Lat	Dif	Dep	Lat	Diff	Dep	Lat	Dif	Dep	Lat	Di!	t De	p' Lat
-	-		4			4			-	The same		1. 12.00				100	W-157 10 1

for 5 Points.

# 70 Difference of Latitude and Departure for 31 Points.

	10.00		5.0			D:0			10.0.			D. #1		-	D:4	-	-
_	-	Dep	Diff	Lat	Dep	Dift		De	Diff	Lat	Dep	Dill	-		Dift	Lat	Deb
1		00.6	-51	41.0	30.4	101	81.1	60.2	151	121.3	90.0	201	161.4	119,7	-	201.6	
	01.6	77.2		41.8		02		8.00	52	122.1	90.6	02	162.2	- 1		10 - 4 bay 57 k	150.1
3	10000	01.8		10000	31.6	03		61.4	53	122.9	91.1	03	163.0	1000	100		150.7
4	-	02.4	54	43.4		04		62,0		123.7	91.7	04	164.6	121.5	( ) ( TO ) (TO )	1 A 1 TO 1 TO 1	151.3
_5	-	03.0	55	44.2	32.8	05		02.0	55	124.5		-			-		151.9
6		03.6	56	45.0	33.4	106	85.1	63.1	156	125.3	92.9	206	165.4	122.7		205.6	
7 8	05.6		57	45.8	34.0	08	85.9	64.3	57	126.0	93.5	08	167.0	123.3			153.1
1.0	06.4	05.4	58		35.1	09	_	64.9	58	127.7	94.7	09	167.8				154.3
10	-	06.0	60	48.2	35.7	10		65.5	60	128.5	95.3	10	168.6	125,1	60	208.8	154.9
11	08.8	06.6	61	49.0	-	111	89.1	66.1	161	129.3	.95.9	211	169.4	125.7	-	-	155,5
12	-	07.1	62	49.8	36.9	12		66.7	62	130.1	96.5			126.3			156.1
13		07.7	63	50.6		13		67.3	63	130.9	97.1	13	171.0	126 9	63		156.7
14	11.2		64	514	38.1	14		67.9	64	131.7	97.7	14	171.8		64		157.3
15	12.C	08.9	65	52.2	38,7	15	92.4	68.5	65	132.5	98.3	15	172.7	128.1	65	212.8	157 9
16	12.8	09.5	66	53.0	39.3	116	93.2	69.1	166	133.3	98.9	216	173.5	128.7	266	2136	1 58.5
17		10.1	67	53.8	39.9	17	94.0	69,7	67	134.1	99.5	17	174.3		67	214.4	159.1
18	14.5	10.7	68	54.6	40.5	18	94.8	70.3		134 9	100.1	18	175.1				159.7
19	15.3	11.3	69		41.1	19		70.9	69	135.7		19	175.9		69		160.3
20	16.1	11.9	70	56.2	41.7	20	96.4	71.5	70	136.5	101.3	20	176.7	131,1	70	216.8	160.9
21	16.9	12.5	71	57.0		121	97.2		171	137.3	1	110000	177.5	131.7	271		161.4
22		13.1	72	1	42.9	22		72,7	11	138.1		11	178.3		72		162.0
23		13.7	73	1	43.5	23	98.8		73	138.9		11	100	132.9	73		162.6
24	1	14.3	74	1	44.1	24		73.9	74	139.7			1			The second	163.2
25	-	14.9		-	_	-	-	_	-			-		_	276		-
26	20.9	1	76	61.0	45.9	126	101.2	75.1	77	141.3	12.50	11	- 0				164,4
27	22.5	16.1	78		46.5	28		76.3			106.0						165.6
29		17.3	79	10	47.1	29	103.6			143.7			1 -	136.4	11	-	166 2
30	24.1		80	10.	47.7	30	104.4			144.5	10 -1-	30	1 -		11 0 -		8 166.8
31	24.9	18.5	81	65.0	48.3	131	105.2	78 c	181	145.4	107.8	231	185.5	137.6	281	225.	167.4
32	25.7		82	65.8	48.9	32	106.0	78.6	82	146.2			186.3	1 38.2		226.	5 168.0
33	1	19.7	83		49.4	33	106.8	79.2			109.0			138.8			3 168.6
34	27.3	20.3	84		50.0			79.8			109.6		1		84	228.	1 169.2
35	28.1	20.9	-	_	50.6	35	108.4	80.4	-	-	110.2	-	-				9 169.8
36		21,4	86	1		11		2 81.0	1	1 12		11 -	1 2 3			12	7 170.4
37	30.7	22.0			51.8	37		81.6	87		111.4	37	190.3	141.2	87	230.	5 171,0
38	30.5	22.6	80	1/0.	52.4		111	8 82.2	88	151.8	112.0	30	191.1	141.8	8	231.	3 171.6
39	31.3	23.2	90	72.	53.6		112	4 83.4	90		5 113.2			142.4	00	222	1 172.2
40		23.8		7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1													
41		24.4		73.1	54.8	141		284.6	191	154.2	1114	42	104	143.6	29	2 2 24	5 174.0
42	33.7	25.0	92	74	7 55.4	43		8 85.2	02	155.0	115.0	43	105.1	144.8	9	3 235.	3 174.6
44	35.	26.2	94	75.	56.0	44	115.	5 85.8	94	155.8	3 115,6	44	195	145.4	9		1 175.
45	36.	26 8	95	76.	56.6	45	116.	4 36.4	95	156.6	116.2	45	196.	146.0			9 175.
45	-	27.4	96	77.1	57.2	146	117.2	87,0	196	157.4	116.8	246	197.	146.6	29		7 176
47	37.	7 28.0	97	777.0	9 57.8	47	118.0	0.87.6	97	158.2	117.4	47	198.4	1 147.1	9	7 238.	5 176.
48	138.	5 28.6	98	78.	7 58.4	48	118.	8 88.2	98	159.0	118.0	48	199.2	147.7	9	8 239.	3 177.
49	139.4	4 29.2	99	79.	5 59.0	49	1119	7,88.8	99	159.8	118.6	49	200.0	148.	9	9 240.	1 178.
50	40.	2 29.8	100	80.	59.6	150								148.9			9 178.
-	1		IITS:	aln.	T	HTY: 0	10	IT -	ID:6	III	T	III Dia	Dep	Lat	IID:	Dep	1 7

for 4 3/4 Points.

11	11120 1	1 7.41	1 0:1	David	(D) 61	Lat I	Detail	D al	Lat	IDen I	ID:#I	Lar	Day I	113.00	Lati	1000
Din Lat	De,	-	_	_	D.r.	Lat	-	-			-			Dift	Lat	
	00 6		39.4		101	78.1			116.7	958		155.3			194.0	
1	01.3		40.2		02	78.8		7	117.5	96,4		156.1		52		159.8
	01.9		41.7		04	80,4			119.0	97.0		157.6	128.7		196.3	160 4
	03.2		42,5		05	81.1	15.63		119.8	98.3		158.4			197.1	161.7
		_	_	_	106	81.9	-	-	120.6	98.9	-		130.6	_	197.8	162.3
1	603.8		43.3		97	82.7			121.3	- 1	1.		131,3	57		163.0
1 / 1 3	205.1		44.8		08	83.5				100.2		and the second	131.9	58		163.6
	05,7	10000	45.6	The same of	09	84.2				100.8			132.5	59		164,2
	7 06 3	60	46 4	38.0	10	85.c	69.8		1236	101,5		162.3		60		164.9
11 08.	07 0	61	47.1	38.7	111	8 5 8	70.4	161	124.4	102.1	211	163.1	133.8	261	201 7	165.5
	3 07.t	62	47.9	39.3	12	86.6		62	125.2	102.7	12	163.8	134.4	62		166.1
13 10.	108.2		48.7		13	87.3				103.4			135.1	63		166.8
	8 08.9		49.5	D 307	14	88.1				104.0	1		135.7			167.4
-	6 09.5		50,2	41.2	15	88 9	-	-		104.6	15		136.3	65	-	168.0
	4 10.1		51.0		116	89.6		166		105 3	216		137.0	266	205 6	
	1 10,8		51.8		17	90.4		68		105 9	17		137.6			169.3
	9 11.4		53.3		19	91.2	75.5	69		107.2	19		138.9			170.0
20 15	7 12.0	1000	54.1		20	92.7		70	-	107.8	20		139.5	70		171.2
-	2 13.3	71	_	45.0	121	93.5	_	171		108.4	221	_	140 1	271	-	-
1-17	0 14.0		55.6		22		77-4	72		109.1	22		140,8			171.9
	8 14.6			46.3	23		78,0			109.7	23		141.4			173.1
	5 15,2		57.2		24		78,6	74	134.5	110.3	24	173.1	142.0			173.8
25 19.	3 15.9	75	58.0	47.6	25	96.6	79-3	75	135.2	111.0	25	173 9	142.7	.75	212.	174,4
26 20.	1 16 5	76	58.7	48.2	126	97.4	79.9			111.6	226	174.6	143.3	276	213.	175.0
	9 17.1			48.8	27	98.1	80.5			112,2	27		144.0			175.7
	6 18.8			49.5	28	98.9	81.2	78		112.9	28		144 6	11		8 176.3
	4 18.4			50.1	29	99.7	81.8	79 80		113.5	29	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	145,2	11 0	215,	1 2
-	2 19.0	-	618		30	100.5	_	-	_	114.1	30		145.9	-	-	
	0 19,7	81		51.4	131	101.2	-	181		114.8	231		146.5		217.	
	7 20.3			52.0	32	102.8		11		115.4	32		147.1	11 -		7 179.5
	3 21 6			53.3	34	103.6				116.7	34		148.4			5 180.1
	1 22.2			53,9	35	104.3		11 0		117.3			149.0			2 180.7
	8 22.8			54.5	136	105.1	2.4			118.0		_	149.7	-	_	0 181.4
	6 23.5			55.2	37	105.0	86.9	87	144.	5 118.6	37	183.	1 150.		221.	8 182.0
	4 24.1	88	68.0	55.8	38	106.6	87.5	1 88	145.	3 119.2	38	183.	9 150.9	88	1	6 182.6
39 30	1 24.7	89	68,8	56.4	39	107.4	188.1	89	146.	1 119.9	1 39	184,	7 151.0	89		3 183.3
	9 25.4		69.6	57.1	40	108.2	88.8	90		8 120.5			5 152.			1 183 9
41 31	7 26.0	91	70.3	57.7	141		89,4			6 121.1		186.	2 152.	8 29		9 184.5
42 32	.5 26,6	92		58.3						4 121.8		187,	0 153.			6 185.2
	.2 27.3			59.0		110.				1 122.4			8 154.			4 185.8
	.8 28.5		72.	59.6	44		3 91.		149	7 123.		180.	6 154.	7 94		0 187,1
	_	-11					-				_				_	
46 35	,6 29.2	96	74.	60.9	146		8 92.			2 124.		7 100.	1 156.	6 97		7 187.7
47 36	.3 29.8	08	3 75	7 62.1	47		493.		152	0 125.		8 191.	6 157.	3 9	3 230	.3 189.6
	.9 31.1			5 62.8			1 94,		9 153	8 126	2 4		4 157			.1 189.6
	.6 31.7		77.	3 63.4	1 150		9 95.		0 164	.6 126.	8 25		2 158			.8 190.2
	ep Lat			Lat		H Dep	_	-	il De			epl La	I La	t Di	AlDe	Lat
-	1	/1	1	-	11			. 11							-	-

for 4 ½ Points.

## 72 Difference of Latitude and Departure for 3 3 Points.

		1.5		-	.15	113	1.	(1)	1:3 4	11	10- 1	10:4		D	I D. in	11	15
Din	Lau	De	Diff	La	Dep	Du	-		חטו	Lat	Dep	Din	Lat		Dut	Lat	Deb
1	00.7	00.7	51	37.8	34.2	101	74.8	67.8	151	111.9	101,4	201		135.0	251	185.9	168,
2	01.9	01.3		38.5		02	75.6	68 5	52	112.6	102.1	03		135.6	52	186.7	3 7 7
3	02.2	02.0	53	39.3	35.6	03	76.3	692	53	113.3	102.7	03	150,4	136.3	53	187.4	
- 4	03.0	92.7	54	40.0	36.3	04	77.0	69.8	54	1141	103.4	04	151.1	137.0	54	188.2	
5	03.7	03.4	55	40.7	36.9	05	77.8	70.5	55	114.8	104.1	05	151.9	137.6	55	188.9	171
6	04.4	04.0	56	41.5	27.6	106	78.5	71.2	156	115.6	104.7	206	152.6	138;3	256	189.6	171
-		04.7		42,2		07	79.3	71.8	57	116.3		07	45.00	139.0	57	190.4	
8		05.4			38.9	08	80,0	72.5	58	-	106.1		154.1		58	191.1	173
9		06,0		43.7		09	80.7	73.2	59	117.8			154.8		59	191.0	
10		06.7		44.4		10	81.5	73.9		118.5		10		141,0	60	192.6	4
-		_			-	111	82.2	74.5	161	119.3	108.1	211	156,3	TAL	261	193.3	-
11	08.2	10000		45.2		12			62	120.0			157.0		62	194.1	
12	08.9			45.9		10000	83.0	75.9		120.7	1			143:0	63	194.8	175.
13	09.6			46.7		13		76.5	64	121.5					64	195.6	
14		09.4		47.4		14	84.4		65	1000	1108	15	158.5	and the same same	6.5	196.3	7.0
15	11.1	10.1		48.2		15	85.2	77.2	-	-	-	-	159.3	-	-		177.
16	11.9	10,7		48.9		116	859	77.9	166	123.0		216	160.0		266	197.0	
17	12:6	11.4	67	49.6	45.0	17	86.7	78,6	1 00	1-23.7		17		145,7	67	197.8	
18	13.3	12.1		50,4		18	87.4	79.2	68	124.4	2 2 2 2 8	18		146.4	68	198.5	179
19		12.8		51.1		19	\$8.2	79.9	69	125.2		19	All and the same	147.0	69	199.3	
20	14.8	13.4	70	51.9	47.0	20	88 9	80.6	70	125.9	114.1	20	_	147.7	70	200.0	181.
21	15.6	14.1	71	52.6	47.7	121	89.6	81.2	171	126.7	114.8	22 I	163.7	148.4	271	200 7	182
22		14.8	72	53.3	48.3	22	90.4	81.9	72	127.4	115.5	22	164.4	149.1	72	201 5	182
23		15,4		54.1		23	91.1	82 6	73	128.2	116.2	23	165.2	149.7	73	20 ,2	183
24		16.1		54.8		24	91.9	83.3	74	128.9	116.8	24	165,9	150.4	74	203.0	184
25	18.5	16.8		55.6		25	92.6	83.9	75	129.6	117.5	25	166.7	151.1	75	203.7	184
26	19.3	_	7.6	_	51.0	126	93.3	84.6	176	130.4	118.2	226	167.4	151.7	276	204 4	185
27	1 0 0	18.1		57.0	-	27	94.1	85.3	77	131.1		27		152.4	77	205,2	
28		18.8		57.8		28	94.8	85.9		131.9	100	28		153.1	78	205.9	
29		19.5		58.5		29	95.6			132.6		29		153.8	79	206.7	-
30		20.1	80		53.7	30	96.3	87,3		133.3		30	and the same of	154.4	80	207.4	
-	_	_	81			_	-	-00	181	-	-	231			281	208.2	-
31	23.0		-	60.0		131	97.0		82	134.1	121.5	32	171.1		82	208.9	
32	23.7	-	82	60.7		32	97.8	1.2.21		135.6	122.2				83	209,6	
33	24.4	-		61.5		33			0			1 2	172.6		84		
34	25.2			62.2		34	99.3	90.0	85	136.3			173.3		85	210.4	191
35	25.9	23.5	-	63.0	57.1	35	100.0	90.6		_	124.2	35	174.1		-	211.1	191
36	- A	24.2		63,7	57.7	136	100.7	91.3		137,8			174.8		286	211.9	192
37	27.4	24.8	87	64.4	58.4	37	101.5	92.0	87	138.5	125.6	37	175.6	159.1	87	212.6	
	28.2	25.5	88	65.2	59.1	38	102.2	92.7	88	139.3	126.2	38		159.8	88	213.3	193
39		26.2			59.8		103.C		89	140.0	126.9	39	177.0	160.5	89	214.1	194
40	29.6	26,9	90	66,7	60.4	40	103:7	94.0	90	140.7	127.6	40	-	161,1		214.8	194
41	30.4	27.5	91	67.4	61.1	141	104.4	94,7	191	141.5	128.2	241		16118		215,6	195
42	31.1	28.2	92	68.2	61.8	42	105.2	95.3	92	142.2	128.9			162.5		216,3	196
43	31,9	28.9	93	68,9	62.4	43.	105.9	96.0	93	143.0	129.6			163.2	93	217.0	
44		29.5	94	69.6	63.t	44	106.7	96.7	94	143.7	130.3			163.8		217.8	197
45	-	30.2			63.8	45	107 4		95		130.9	45		164.5		218.5	198
46	_	-	_	71.1			108.2				131.6	-	182.2	165.2	296	219.3	
47	34.1	31.6		77.0	65.1			98.7			132,3		183.0	165,8	97	220,0	
48		32.2		22.6	65,8		109.6				132.9			166.5		220.7	
49	36.3		99	72.2	66.5	40		100.0		147.4	133,6			167.2		221.5	
50	37.0		100	74.7	67.7	150		100.7					185.2	167'9	300		
		-		-											-	-	-
71111	Depl	Lat	אושן	Deb	Lat	Din	Dep	Lat	Inni	Dep	Lat	Poeb	Lat	Lat	IJUIA	1Dep	<sup>1</sup> La

for 4 4 Points.

Difference of I	Latitude and	Departure fo	OF 4	Points.
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	D	iff	er	en	ce	of l	Lati	tude	e an	d I	epa	rtui	e f	or 4	Poi	nts	. 7	3
Diff	16 Lat Dep Dift La																	
-	3 00,7 00,7 51 36.1 36.1 101 71 4 71,4 151 106.8 106.8 201 142.1 142,1 151 177.5 177.5 177.5 177.5 02.4 01.4 02.4 52 36.8 36.8 02 72,1 72.1 52 107.5 107.5 02 142.8 142.8 52 178.2 178.2 178.2 102.1 53 37.5 37.5 03 72.8 72.8 53 108.2 108.2 03 143 5 143.5 53 178.4 178.9 02.8 32.8 54 38.2 38.2 64 73.5 73.5 54 108.9 108.9 108.9 04 144.2 54 179.6 179.6 03 5 03.5 55 38.9 38.9 05 74.2 74.2 55 109.6 109.6 05 144.9 144.9 55 180.3 18																	
2				T			8, 8, 1			-				142.8	100	52		
3																		178.9
4				-				7. 7	22.2					70.00				179.0
5	-	-	-11-					-					-	-	-	_		-
-	0 1 3	04 9	-	-	40.3	T 500 100	07	75.7	75.7	57		111,0	07	146.4	140 4	57	181.5	181
8		05	Ai		41.0		08	76.4	76.4	58	111.7	111 7	00	147.1	147.1	58	182 4	182 4
9	05 4	06.	. 11		+1 7		09	77:1	77.	59	112,4	112 4	09	47,8	147.8	59	183.1	183 1
10	07 1	07	-11-		42.4	42 4	10	77.8	77.8	60	113.1	113.1	10	148.5	148.5	60	183.5	153.8
11	01.8	1				43.1	111	78.5	78.5	161	113.8	113.8	211	149.2	149,2	261	184.5	
12	03.5		- 11	. 1	+3.8	2 4 1	12	79.2	79.2	62	114 5		12	149.9	149 9	62	185.	
13	03.2		- 11	64	44 5	44.5	14	79,9	79.9 80.6	63	116.0	115.3	13		150,6	63		185.0
14		10.				46.0	15	81.3	81.3	65	116.7	116 7	11	152.0	151.3	65	187.4	186 7
15	11 3		-H-	-	46,7	-	116	82.0	82.0	166	117 4	117.4	#	-	1000	266	188.1	188.1
17	12 0	1800	-11	-	47.4		17	84.7	82.7	67	118.1	118.1	H			67		188.8
18	12 7		-		48 1	48.1	16	83.4	83.4	68	118.8		41 /	1	1322	68		199.5
19	13.4	13	4	69	188	48,8	19	84.1	84.1	69	119.5	119.5	19	154.8	154.8	69		190.2
20	14 1	14	1	70	19,5	49.5	20	84 8	84.8	70	120.2	120.2	26	195.6	155.6	70	190.9	190 9
21	14 8	14	8	71	1-	50 8	121	85.6	85.6	173	120.9	120,9	1221	156.3	156.3	271	191.6	191.6
22		15	- 11	1000		50.9	22	86.3	86.3		121.6	121.6			100	72	192.	192.3
23		16.	-11	73	31.6	10	23	87 0	87.0	73	122.3	122.3		- 0	1 0 .	73	1	193.0
24		17.	H	74	53.0		11	87.7	88.4	11	123.7	13			1 2 2 2	74	193.7	
25		17	- 1	75				89 1	89 1	-	-	-		33		75	194.4	-
16	1 30	1 10	. 11	77	53.7	53.7	11	89.8	89.8			124,4	1226		160.5	11	1	
27		19	- 11	78		55.2		90.5	90.5	11 2	125.9	125	27	1-6		77	195	195.9
29	1	5 20	- 11	79		55.5		91.2	91.2	11					161,9	11		197.3
30		2 2 1	.2	80	56.6	56.6	30	91.9	91.9	80	127.	127.	3 30	162.	162.6		1	198.0
31		9 21	.0	81	57.	57.3	131	92,6	93.6	181			23	163.	163.3	281	108.	198.7
32		6 23	.6			58.0			93.	82	128.	128.	7 3		154,0	82	199.	1000
33		3 23		83						11					164.7	11 -	200.	200.1
34	The said to the	0 24	.0	84		1 60.		94,7			130,	1 130.	1 3		165.5	113		8 200.8
35		7 24	-			60.	-	333				-	-		-		201.	-
36	-	2 26		86		61.	11 -	96.2	96,		131.	5 131.	5 23	160	6 167.6	87		2 202.2
37		9 26				62.			97.		112.	1 132.	3		3 168.			9 202.9
39		6 27		89		9 62.		98.3	98.		133,	6 133.	6 3	160	169.	89	1	3 204.
40		3 28		90	10.	6 63.					134.	3 134	3 4		7 169.7			1 205.
41		0 29	.0	91	64.	3 64.					135,	1 125.	1 24	1 170.	170,	291		205.
42	-	7 29		92	65.	1 65,	42	100.4	100.	4 92	135.	135.	8   4	2 171.	1 171.	92		5 206.
4:		4 30		93	100	8 65.		101.1		9:	130.	5 136.	5 4		8 171.		207.	2 207.2
4	31.	1 31	.1	94	10	5 66.	44	and the second second	101.	11 -	37	2 137.	2 4		5 172.	94		9 207.
4		8 31	-	95		67.			102.	-		9 137.		_	2 173.			6 208.
40	32.	5 32		96		9 67.					138.	6 138.	6 24	6 173.	9 173.9	290		3 209.
47		2 33		97		6 68,			103,	97	139.	3 139.	3 4		6 174,			0 310,
45		9 33		99								7 140.	7	176	1 176.	9		7 210.
50				100		1.	150				141,	4 141	1 25	176.	8 176.	300		1 212
1	A L'e		-	_				Dep				_	-		Lat			La
		7,00		خفنا		-	11-4	, <u> </u>		1			11-1	-		1	100	PI Da

for 4 Points.

# 72 Difference of Latitude and Departure for 3 3 Points.

3 4	00.7			-	Dep	D I	Lat	Deb	DI	Lat	Dep	Dill	Lat	DCP	Dut	Lat	Top
3 4	01.5		91	1 0		20 30 10	-					The same of	0 -	-		-0	-60
3 4					34.2	101	74.8	67.8		111.9			148.9			185.9	168,5
4	02.21	-			34.9	02	75.6	68 5		112.6		03	149.6	136.3	52	187.4	
		02.0			35.6	03	76.3	69.8	53	114.1	103.4		151.1	-	54	188.2	
2	03.7	02.7		40.0		04	77.8	70.5	55	114.8		05	151.9		55	188.9	171,2
		-		_	-	05	78.5	_	156	115.6	-	-	152.6		256	189.6	1719
	04.4	12.0		42,2	37.6	106	79.3	71.2	57	116.3			153.3		57	190.4	1.0
2	05.2			43.0		08	80,0	72.5	58	117.0			154.1		58	191.1	
1 1 1	06.7			43.7		09	80.7	73.2	59	117.8			154.8		59	191.9	A
	07.4			44.4		10	81.5	73.9	60	118.5	107.4	10	155.6	141,0	60	192.6	174,6
-	08.2	_		45.2	-	111	82.2	74.5	161	119.3	108.1	211	156,3	141.7	261	19.3.3	175.2
	08.9			45.9		12	83.0	75.2	62	120.0			157.0		62	194.1	175.9
	09.6			46.7		13	83.7	75.9	63	120.7	109 4	13	157,8	143:0	63	194.8	
- 1	10.4			47.4		14	84.4	76.5	64	3	110.1		158.5		64	195.6	
15	11.1	10.1	65	48.2	43.6	15	85.2	77.2	65	122.2	1108	15	159.8	144.4	6.5	196.3	177.9
10	11 9	10,7	66	48.9	44.3	116	859	77.9	166	123.0		216	160.0		266	197.0	178.6
17	12:6	11.4		49.6		17	86.7	78,6		123.7		17	160.7		67		179.3
	13.3			50,4		18	87.4	79.2	68	124.4	0	18	161.5		68	198.5	
	14.1			-	46.3	19	\$8.2	79.9	69	125.2		19		147.0	70	199.3	181.3
20	14.8	13.4	70	_	47.0	20	88 9	80.6	70	125.9	_		163.0	_	-	-	-
	15.6		71		47.7	121	89.6	81.2	171		114.8	221			271	200 7	1-0-
7	16.3				48.3	22	90.4	81.9	72		115.5	22	164.4		72 73	201 5	182.6
23	17.0				49.0	23	91.1	82 6	73		116.2		165.2		74		184.0
24	17.8	16.8		54.8		24	91.9	83.9	74	- 2	117.5		166.7		75.		184.6
25		-	-	_		-			176		_	-	167.4		276	204 4	1 -
	19.3		7.6		51.0	126	93.3	84.6	77	130.4	118.8		168.2		77	205,2	
	20.7			57.8		28	94.8	85.9	78	131.9			168.9		78	205.9	
	21.5				53.0	29	95.6	86.6	79		120.2	29	169.6		79	206.7	
	12.2		80		53.7	30	96.3	87,3	80		120.9	30	170.4		80	207.4	188.0
_	23.0	20.8	81	60.0		131	97.0	88.0	181		121.5	231	171.1	155.1	281	208.2	188.7
	23.7			60.7		32	97.8	88.6	82		122.2	32	171.9		82	208.9	189.
	24.4			61.5		33	98.5	89,3	83	135.6	122.9	33	172.6	156.4	83	209,6	190,0
	25.2		84	62.2	56.4	34	99.3	90.0	84	136.3			173.3		84	210.4	
	25.9	23.5	85	63.0	57.1	35	100.0	90.6	85	137.0	124.2	35	174.1		85	211.1	191.4
36	26.7	24.2		301	57.7	136	100.7	91.3	186	137,8			174.8		286	211.9	
37	27.4	24.8	87	64.4	58.4	37	101.5	92.0	87		125.6		175.6		87	212.6	
	28.2	25.5	88	65.2	59.1			92.7	88	139.3	126.2	38	170.3	159.8	88	213.3	
		26.2	89	65,9	59.8					140.0	120.9	40	177.0	160.5			
	29.6		-	66,7	_		103:7	94.0	90		127.6					214.8	194.
41	30.4	27.5		67.4			104.4	94,7	191		128.2			16118		215,6	
42	31.1	28.2		68.2				95.3	92	142.2			180.0	162.5	02	216,3	
44		28.9		68,9	63.1		105.9	96.7		143.0	130.3	/. II	180.7	163.8	94	217.8	
45	33.3	29.5		70.4		45	107 4	97.4	95		130.9		181.5	164.5	95		198.
-	_		_	71.1			108.2	98.0						165.2	_	219.3	
47	34.1	30.9		77.0	65.1			98.7	07	145,0	122.2	47	183.0	165,8	97	220,0	
48	34.6	22.2	98	72.6	65,8	48		99.4	98	146.7	132 0	48	183.7	166.5	98		200.
49		32.9	99	73.3	66.5			100,0	99	147.4	133,6	49	184,4	167.2	99		200.
50	37.0		100	74.1	67,1	150	111.1		200	148.2	134.3	250	185.2	167'9	300		201.4
			Dif	Dep	Lat	Dift	Dep	_	Dift	Dep	Lat	Dep	Lat	Lat		Dep	Lat

for 4 4 Points.

# Difference of Latitude and Departure for 4 Points.

Diff	00,	-		t Lat			Lat	Dep	UDII	المسد ال	Dep	IDIII	Lat	Dep	.I Diff	TAL	4.00
•		/   ~ ~ .			36.1	11.00	-	-	-	-		4-	_	- Lack	.11	Tal	Dep
3	101.1	01,	. 11 -		36.8		71 4				106.8		142.1	THE REAL PROPERTY.	151	177.	177.4
	02.1	02.	1 5	1 -	37.5	11	72.8		11 3		107.5				52	178 2	178 2
1	02,5	32.	oll -		38.2	71 -	73.5	73.5	11	108.9		11 -3		1	53	178.	178.9
5	03	33.	5 55	38.9	38.9	05	74.2	74.2	11 3.		109.6		144.0	144.0	11 24	179.6	179.6
6	04.2	04	2 50	39 6	39.6	100	74.9	74.5			-	-	1157	144	55	180.3	-
7	01 6	04	9 57		43.3	07	75.7	75.7	57	1110	1	07	145.7	145 7	57	181.0	121 0
8	05.7	1 .	7 58	1	410	03	76.4	76.4	58	111.7	1117	00	147.1	147.1	1 38	182 4	182 4
9	03 4	05.	1 59		41 7	10	77.1	77.	59	112,4	112 4	09	47,8	147.8	59	183.1	183.1
10	07.8		-		42 4	-	77.8	77.3	-	113.1	113.1	10	148.5	148.5	60	183.5	
11	03.0	1-0	62	1.0	43.8	111	78.5		161	113.8	113.8	211	149.2	149,2	261	184.5	184 5
12	03.2	1-	1 4.	1.3		13	79.2	79.2	11	114 5	114,5	12	149.9	149 9	62	185.	185 3
14	03.9		64		45.3	14	80.6	1 0 2	11	116.0	115.3	13	150 6	150,6	63	186.c	185.0
15	E3.6	10.	65	46 0	46.0	15	81.3	81.3		116.7	116 7	14	152.0	152.0	64	186,7	186 7
16	11 3	11.	66	46,7	46.7	116	82.0	82.0	166	117 4	-	-	30.0	-	-	187.4	187.4
17	12 0	12.0			47.4	17	84.7	82.7	11	118.1	117.4	210	152.7	153.4	67	188.1	188.1
18	127	12.	68		48.1	16	83.4	83.4	68	118.8	118.8	18	154.1	154,1	68		188.8
19	13.4	13	69	1	48,8	19	84.1	84.1	69	119.5	119.5	19		154.8	60	A	199.5
20	14 1	14	70	-	49.5	20	84 8	84.8	70	120.2	120.2	20	155.6	159.6	70	100.6	190 9
21	11 8			1-	50 2	121	\$5.6	85.6		120.9	120,9	221	156.3	156.3	271	191.6	191.6
22	15.0	16.	11	7	50.9	22	86.3	86.3	11	121.6	121.6	22	1570	157.0	72	192.3	192.3
23	17 0	1 '	11		52.3	23	87.7	87.0	11 . 2	122.3	122.3	23	157.7	157.7	73	193.0	193.0
25		17.			53.0	25	88.4	88.4	74	123.0	123.0	24	158.4	158.4	74	193.7	193.7
16	18.4	18.			53.7	126	89 1	89 1	-	-	123.7	25	159.1	159 1	75	194.4	194.4
27	19.1			54.4	54.4	27	89.8	89.8	77	124.4	124,4			159.8	276	195 2	195.2
28	19.8	19.		55.2	55.2	28	90.5	90.5		1	125.2	27	161.2	161.2	77	195.9	195.9
29	20,5	20.	- 11		55.9	29	91.2	91.2	79	126.6	126,6	20	161.0	161.0	78		196.6
30	21.2	21.	80	56.6	56.6	30	91.9	91.9	80	127.3	127.3	1	162.6	162.6	80	197.3	197.3
31	21 9	21.	81	57.3	57.3	131	92.6	93.6	181	128.0	118 0		163.3	163.3	281		-
32	22.6	1	11	1 0	58.0	32	93.3	93.3	82	128.7	128.7	1	- 0 - 1	154,0	82	190.4	198.7
33	24,0		83		58.7	33	94.0	94 0	.,	129 4	139.4	33	164.7	164.7	83		200.1
34	24.7	24.0	84	60.1	59,4	34	94,7	94.7	84	130,1	130.1	34	165.5	165.5	84	0	200.8
36	25.5	25.	86	60,8	_		95.5	95,5	-3	130,8	130.8	3.5	100.2	100.2	85	201.5	201.5
37		26.	" -	1 -	61.5	37	96.9	96,2	186	131.5	131.5	236	166.9	166.9	186	201.2	202,2
	26.9		1 00	62.2		28				122.0	132.2	37	- 60 -	167.6	1 00	202.9	
	27.6	27.6	89	62.9	62.9	39	97.6	98.3	8.	133,6	132.6	30	169,0	160.0		203.6	
40	28.3	28.	90	63.6	63.6	40	99.0	99.0	90	134.3	134'3	40	169,7	169.7		204.3	
41	29 0		91	64.3	64.3	141	99.7	99.7	TOI	135,1	126 1	241	170.4				
	29.7			65.1	65,1	42	100.4	100.4	92	35.0	125.8	42	171.1			205.8	206.
43	90.4	30.4	93	65.8	65.8		101,1		93	130.5	1 26. 5	43	171.8	171.8	93	207.2	207.2
44	31.1	31.1	94	66.5	67.5		101.8		94	-37.2	177.2	44	72.5	72.5		207.9	
	-						102.5		95	137.9	137.9	45	73,2	73.2		208.6	
46	32.5 33.2	32.5	90	67.9 68.6	68.6	146	103.2	103.2	196	138.6	138.6	246	73.9	73.9	296	209.3	209.3
48	33.9	33.2	08	69.3	50.2	47	103.9	104.6	97	139.3	139.3	47	74.6	74,6	97	210.0	10,0
	34.6	34.6	99	70.0	70,0	49	105.4	105,4	90	140.7	140.0	40	75.4	75.4		10.7	210.7
50	35 4	35.4	100	70.7	70.7	150	106.1	06.1	200	141,4	41.4	250	76.8	76.8	100	211.4	111.4
ifil	L'ep	Lat	Dift	Dep	Lat	Dif	Dep	Lat	Dif	Dep	Lat	Dif	Deal	1.20	Dia		
100	12.33			-	- 11						11			- At 1	Dist.	Dep	Lat

for 4 Points.

Days					Ye	ar	17	66	5.				ys				7	ea	r	17	67	•			
Month Da	January	February	March	April	May	June	July	August	September	October	November	December	Month Days	January	February	March -	April +	May	June	July	August	September	October	November	December
3 4	29 30 31 32	31 32 33 34	30 31 32 33	31 32 33 34	32 33 34 35	33 34 35 36	34 35 36 37	35 36 37 38	38	38 39	39 40 11	39 40 11	3 4	11 12 13 14	13 14 15 16	12 13 14 15	13	16	17	16 17 18	18	19 20 21 22	1 5 20 21 22	21 22 23 24	21 22 23 24
56 78	35	35 36 37 38	34 35 36 37	35 36 37 38		37 38 39 40	38 39 40	39 40 11	11 12 13 14	11 12 13	13 14 15 16	13 14 15 16	5 6 7 8	15 16 17 18	17 18 19 20	16 17 18 19	17 18 19 20	18 19 20	19 20 21	20 21 22	21	23 24 25 26	23 24 25 26	25 26 27 28	25 26 27 28
9 10 11 12		39 40 11	38 39 40	39 40 11	40 11 12 13	11 12 13 14	13 14 15	13 14 15 16	15 16 17 18	17	19	17 18 19 20	910	19 20 21 22	21 22 23 24	20 21 22 23	21 22 23 24	-	23 24 25 26	24 25 26 27	25 26 27 28	27 28 29 30	10.00	30	31
13 14 15 16	12	13	13	13 14 15 16	14 15 16 17	15 16 17 18	16 17 18	18	19 20 21 22	20	21 22 23 24	2 I 2 2 2 3 2 4	13	23 24 25 26	25 26 27 28	24 25 26 27	-	28	27 28 29 30	28 29 30 31		31 32 33 34	31 32 33 34	33 34 35 36	33 34 35 36
17 18	17	17 18 19 20	16 17 18 19	19	21	20 21 22	21 22 23	21 22 23 24	-7	24	27	28	19 20	27 28 29 30	29 30 31 32	28 29 30 31		30 31 32 33	31 32 33 34	32 33 34 35	33 34 35 36	35 36 37 38	35 36 37 38	37 38 39 40	37 38 39 40
21 22 23 24	19 20 21 22	21 22 23 24	21 22 23	21 22 23 24	22 23 24 25	23 24 25 26	24 25 26 27	25 26 27 28	29	29 30	31	30 31 32	21 22 23 24	31 32 33 34	33 34 35 36	32 33 34 35	33 34 35 36	37	35 36 37 38	39	40	12	12	11 12 13 14	11 12 13 14
27 28	23 24 25 26	25 26 27 28	25 26 27	27 28	27 28 29	28 29 30	30 31	31	33	33	35	33 34 35 36	25 26 27 28	35 36 37 38	37 38 39 40	36 37 38 39	37 38 39 40	38 39 40 11	39 40 11	4C 11 12 13	11 12 13 14	13	14	15	15 16 17 18
30 31	27 28 29		28 29 30	29 30	30 31 32	31	32 33 34	33 34 35	35	35 36 37	37	37 38 39	30	39 40 11		11112	11	12 13 14	13	14	15	17	17	19	20

) S				Y	ea	r	170	58.					ys				Y	ea	r	17	69	•			
Month Days	January	February	March	April	May	June	July	August	September	October	November	December	Month Days	January	February	March	April	May	June	July	August	September	October	November	December
1 2 3 4	22 23 24 25	25 26	24	24 25 26 27	26 27	27 28	28	29	31	31	33 34	32 33 34 35	1 2 3 4	33 34 35 36	35 36 37 38	34 35 36 37	35 36 37 38	36 37 38 39	30	38 39 40	39 40 11	1 1 1 2 1 3 1 4		13 14 15 16	1 1 1
5678	28	29	28	28 29 30 31	30	31	32 33	33 34 35	37	34 35 36 37	39		5678	37 38 39 40	11	40	39 40 11 12	I I 1 2	12	12 13 14 15	13	17	17	17 18 19 20	1
910	31	33	12	32 33 34 35	33 34 35 36	35 36	35 36 37 38	38	<b>3</b> 9	39	11	1	910	11 12 13	1.2	13	13 14 15 16	15	16	18	18	21	20	22	2
14	35		136	38	38	39 40	39 40 11	11	14	13	14 15 16		13 14 15	16	19	17	19 20	19	20	21	21 22 23 24	24	24	25 26 27 28	2
17	39	11	10	11	12	13	15	1000		100	100	19	17 18 19 20		23	22	22	24	24	25	25 26 27 28	29	28 29	31	
2:	2 1 3	3 1 4	5 1	1 1 5	17	18	18	18 19 20 21	21	22	24	23	21 22 23 24	23 24 25 26	26	25	25 26 27 28	27	28	30	29 30 31 32	32	32	33 34 35 36	3
2 2 2 2	5 I 6 I 7 I	7 10	911		20	21 22	21 22 23	22 23 24	24 25 26	25 26	26 27 28	26 27 28 29	25 26 27	28	29	29	30	30 31 32	31	32 33 34	33 34 35	35 36	35 36 37	38 39	3
3 3	9 2	0 2		1 2 2 2 3	2 2 3	24	-	26	28	28	30	30	30	32		32 33 34	33	34	35		37 38	39	39		1

ays				Y	ea	r	17	70	•				iys				Y	ea	r	17	73.				
Month Days	January	February	March	April	May	јине	July	Auguft	September	October	November	December	Month Days	January	February	March	April	May	June	Julg	August	September	October	November	December
1 2 3 4	14 15 16	16	16	16	18	18	20	21	23	23 24	25	24 25 26 27	3 4	26 27	zt 27 28 29	26 27	27	27 28 29 30	29 30 31 32	29 30 31 32	31 32 33 34		334 34 35 36	35 36 37 38	35 37 18
5 6 7 8	19 20 21	20 21 22 23	21 22	-	24		24	27	2.8 29	27	30	28 29 30 31	5678	29 30 31 32	30 31 32 33	29 30 31 32	30	31 32 33 34	33 34 35 36	33 34 35 36	35 36 37	37 38 39	37 38 39 40	39 40 11	35 45 13
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14	28	29 30 31	28 29 30	29 30 31	31 32	31	32	34 35	37	36 37	36 37 38 39	36 37 38 39	13 14 15 16	38 39	39 40 11	38	400		13	11 13 14	13 14 15 16	15	15 16 17 18	19 20	18
19	31	33 34 35	33 34	35	33 34 35 36	36 37	38	37 38 39	38 39 40 11	39		11 12 13	19 20	11 12 13 14	13	11 12 13 14	13	13	15 16 17 18	15 16 17 18	18	- 1	19 20 21 22	21 22 23 24	2:
21 23 24	36	39	36 37 38	38	39 40	39 40 11	12	11 12 13	13	13	15 16 17	17	_	17	17 18 19	17	18	19	21	21	2 I 2 2 2 3 2 4	24 25 26	24 25 26	26 27 28	25
26 27 28	39 40 11	12	11	12	12 13 14	13 14 15	14 15 16	15 16 17	17 18	17 18	19 20 21	-	26 27 28	20 21 22	21	20 21 22	20 21 22	22 23 24	24 25 26	24 25 26	25 26 27 28	28 29 30	28 29 30	30 31 32	31
30	13		13	14	15	17	17	19	21	2C 21 22	23		30			23 24 25	23	25° 26° 27	27 28	27 28 29	29 30 31	31	31 32 34	33	33 34 35

178					Ye	ar	17	72			Ţ		Days				2	Čez	ır	17	73				
Month Days	January	February	March.	April	May	June	July	Auguff	September	October	November	December	Month D	January	February	March	April	May	June	July	Auguff	September	October	November	December
2 3 4	36 37 38 39	39		38 39 40		11	40 11 12	11 12 13 14		15 16 17 18	1	18	3 4	18	20 21 22 23	18 19 20 21	19 20 21 22	1200	21 22 23 24	22		25	25 26 27 28	28	20
56 78	10 11 12 13	13	11 12 13	13	13	14 15 16 17	14 15 16	15 16 17 18	19	19 20 21 22	20 21 22 23	22	5679	22 23 24 25	24 25 26 27	22 23 24 25	24		25 26 27 28	27	1 6	28 29 30 31	30	31 32 33 34	32334
9 10 11	14 15 16	16	1 2	16 17 18 19	16 17 18	19	18 19 20 21		22	24	26	25 26 27 28	910	26 27 28 29	28 29 30 31	26 27 28 29	28		29 30 31 32	29 30 31 32	T	32 33 34 35	33 34 35 36	35 36 37 38	35 37 38
13	18 19 20 21	20 21 22 23	19 20 21 22		20 21 22 23	22 23 24 25	22 23 24 25	23 24 25 26	27		30	30 31 32	13 14 15 16	30 31 32 33	32 33 34 35	30 31 32 33	31 32 33 34	32 33 34 35	33 34 35 36	33 34 35 36	35 36 37 38	36 37 38 39	37 38 39 40	39 40 11	39 40 11
17 18 19	22 23 24 25	24 25 26 27	23 24 25 26	24 25 26 27	24 25 26 27	26	26	27 28	31	33	33 34 35	33 34 35 36	1 /	34 35 36 37		35 36	36 37	37	39	37 38 39 40	39 40 11	11 12 13	11 12 13 14	13	14
21 22 23 24	26 27 28 29	30		28 29 30 31			30 31 32	31 32 33 34	33	35 36 37 38	36 37 38 39	38	21 22 23 24	38 39 40	40	-	40	11 12 13	11 12 13	11 12 13	13 14 15 16	14 15 16 17	15 16 17 18	-	17
25 26 27 28	30 31 32 33	32 33 34 35	31 32 33 34		32 33 34 35					39 40 11		11 12 13 14 15 16	25 26 27 28	14	14 15 16	13	13 14 15 16	15	15	15 16 17 18	17 18 15 20	18	19 20 21 22	21 22 23 24	21 22 23 24
29 30 31	34 35 36	36	35 36 37	36 37	36 37 38	38	38	39	13	13	14	15 16 17	29 30 31	16		16	17	18	19	19	21 22 23	22	23	25	25 26 28

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	bers,	800	3	

Davs	2			7		Y	ea	ır	I	7	7	4.				
Month D	. 1	January	February	March	Antil	mider	May	June	lulii	Jung	August	Sentember	Septemon!	October	November	December
7 8	333333333333333333333333333333333333333	32 33 34 56 78 90 1 2 3 4 56 78 90 1 2 3 4 5 5 6 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7	4 5 6 7	33 34 35 36 37 38 39 40 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	3 3 3 3 3 3 3 3 3 3 3 3 3 3	1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	2 3 4 5 5 7 8 9 0 1 2 3 4 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	19 20 11 12 13 14 15 16 17	3 3 3 3 3 3 3 4 1 1 1 1 1 1 1 1 1 1 1 1 1	3 4 5 5 3 3 4 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2	3 4 5 5 7 8	33 39 40 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 29 29 29 29 29 29 29 29 29	0 3 3 3 3 3 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8 90 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	3	3 3 4 4 1 1 1 1 3 1 4 1 5 1 6 1 7 1 8 1 9 2 0 2 7 2 8 2 9 3 0 3 1 3 2 3 3 3 4 3 5 1 5 1 6 1 7 1 8 1 9 1 9 1 9 1 9 1 9 1 9 1 9 1 9 1 9
9 0 1	28			27 28 29	28	29	3		11 2	3:34	3 3	4	33 34 35	3	6	36 37 38

# A TABLE answering to any of the foregoing Numbers.

Num- bers	Ti	mes an	swering.
Carte	H.	- M.	10.215.000
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	3 - 4 - 4 - 5 - 6 - 7 - 8 - 9 - 10 - 11 - 12 - 12 - 12 - 12 - 12 - 12	48 36 24 12 00 48 36 24 12 00 48 36 24 12	Afternoon
26 27 28 29 30 31 32 33 34 35 36 37 38 39	0 — 1 — 2 — 3 — 4 — 4 — 5 — 6 — 7 — 8 — 9 — 10 — 11 — 12 — 12 — 12 — 12 — 12 — 12		After Midnight

### The Use of the foregoing Tables of Numbers.

IN these Tables, each Page is divided into two Parts, by a double Line drawn down the Middle; and each of the Parts are marked at the Top with the Year for which they shew the Numbers, and under that, the Lest-hand Column of each Part is marked with the Days of the Month, and the other Columns with the Months of the Year: So that if you would know the Number for any Day, suppose for Example, on the 20th of March, 1766.

First, Find the given Year 1766, at the Top of the Table, and then under the given Month, which is March, and right against the given Day of the Month (which in this Case is 20) you will find the Number 19, which is the Number for that Day; and if from the Number so found you subtract 10, the Remainder will be the Moon's Age

for that Day.

The Use of the Table of the Times answering to the foregoing Numbers.

In this Table the Left-hand Column is mark'd with the given Numbers from 11 to 40, and the Figures right against any of these Numbers, give the Time answering to it, in Hours and Minutes.

#### EXAMPLE I.

I would know what Time answers to the Number 23?

Answer. 10 Hours 24 Minutes Afternoon, that is, at 24 Minutes past 10 at Night.

#### EXAMPLE II.

What Number and Time answers to the 8th of January, 1774.

First, By the Tables of Numbers, I find the Number to be 36, and against that Number, in the Table of Times, I find 8 Hours 48 Minutes after Midnight, that is 48 Minutes past Eight in the Morning.

At Army A.	H	M		H	1
At Army —	or	03	At Cork, Calis, Cape Clear,		
At Amsterdam and Armontie	03	00	and in the Creek —	04	
At Abarwark -	04	20	At Caldy and Comarthen Bay	05	3
At Abarmorick and Antwerk		-		06	
			Without the Cafkets	08	
The Himself englis	1	13	Between the Cafkets and		,
. В		-	Guernsey, before Cromer, at		
At Beachy, Blacktail, and			Segret Cliffs and at Catal	_	
ofore the Dace of Planaust	1	00	Seven Cliffs, and at Catness -	09	C
Throat of Beach	12	00	At the Caskets and Cham-		
I hwart of Beachy	12	45	berness	09	4
At Blackneys in Bluet, and		1	At Cows, in the Foss of Caen, in Calice and Chamber-		
it Bell-Ijle	01	30	Caen, in Cauce and Chamber-		
			ness Roads		3
oick———	02	15	Before the Haven of Caen,		
Bourdeaux River, the South	1	1 1 1	in the Chamber, between	1	-
Coast of Bretaigne, the Coast			Cripple Sand, and the Croyle,		
of Biscay, and at Bockness -	03	00	and at Calfhot -	11	1
At Brest, before the Base,	,				1
and the River of Bourdeaux,			D.	1	
within the Haven———		45	At Dover Pier, and before		
In Breefound, Bloy and Bal-			Dunkirk —	12	C
imore —	-04	30	At Denbeigh & Downs Road	02	1
Before Bremen and at Black-		1	At Dort	02	0
ney, and in the Channel be-	1	100	At Dungarven—	03	0
ore Bourdeaux———		00	At Dartmouth -	06	3
At Bristol Key-			At Dublin -	20	,
At Bridgewater ——				00	
Bullen Deep		30			
Butter Decp	1.	30	At Dungeness and Dunnose	09	4
C.	1		At Dover, Diepe and Deal	10	(1)
교육 교육하다 아니라의 그리고 하지만 모르고 그리고 하는데 하는데 하는데 그리고 모르게 되었다.		-	<b>.</b>		
In Condado		00		1	
In the Chamber of Rye —		45	At Emden, before the Elve		1
Without Calis, at Corpus			before the Eyder, and before		3
Christi Point, and at Camfer-	- 1	30		12	C
Between Calis, and Dover,	1 1			01	3
before Conquet, and at the			Before the Eastern & West-		1
North Cape	03	00	ern Emes, and at Engoments-	000	C

MIN F.	H	MI	1 2 1	H	MI
On the Coast of Flanders-	12	00	Under Holy Island & at Horn	01	20
At Flushing -	00	45	Before Hartlepoole ———————————————————————————————————	02	30
Before the Fen in the	dr	1	At Huntcliff-Foot	03	15
Channel	01	20	At Humber	05	45
Without Fountny-	02	15	Before Hamhorough, at Hull,	00	, 2
Without the Banks of	-		at the Holmes, and before		
		00	Humbers Mouth ———	06	00
At Flamborough and Brid-	-3		At Haerlem, Havre de Grace		
lington —	04	20	and Home-bead	00	00
At the Forn, in Foy at Fal-		3-	At St. Hellens, and Harwich	29	00
mouth -		15	and without the Banks of		
Between Foy & Falmouth in		1	Harwich —		20
		15	At Harwich within —	11	30
Before the Coast of Friez-		13		1	. 2
land and the Fly		20	I.		
Without the Fly	0	15	At Jutland Islands -	12	00
At Frieze and Fair Isle -	00	00	On the W. Coast of Ireland	02	00
At the Frith and South	1 -		In all the Havens on the		
Foreland —	10	20	South Coast of Ireland —	05	1.5
In Fair Isle Road, & at the		3	South Court of Trums	2	. 2
North Foreland —		15	K.	1.0	
1.01		- 3	Kentish Knock	10	00
G.			At Kelliers		
In Gibralter Road, Gravel-			At Kingfale -		
ing and before Cherburg -		00	At Kilduyn	07	30
Before Goree, at Guernsey &				09	
at Gravesend		20		0.9	
At Groine, at Gascoign, and		3	L.		
the Coast of Galicia -	03	00	At Leith	12	00
Thwart of Guernsey -	1 0	45	At Lisbon	02	1.5
In the Chamber, and Goree-		1	At London -	03	00
end —	1	15	Thwart of Londey and be-	3	00
		1	fore Lynn	05	1.
H.	0		At Lynn half Tide, at	05	. 5
Before the Hever, before	1		Londey	1.53	00
Horn, and at Hampton-Key -	1	00	At Lynn	06	15
	!		12		+3
A		1	M	1.5	

	H	M	0.	H
At the Lizard by the Land	07	30		030
At Lambay	08	15	At Orkney-	og'c
At Leystoff, and thwart off			At Orfordness -	00
it without the Banks	09	45	At Orfordness, without the	1
In Leystoff Road, and at			Banks, and between Orford	
Long Sand-Head -	10	30	and Orwell Waves -	10
		1	At Orfordness within the	
M.			Sands —	
Within the Maes at Mal-				
don	00	45	P.	
Before the Maes -	01	30	At Portsmouth Half-Tide-	l i
At the Maes and before			At the Pens. Porthus and	
St. Matthew's Point -	03	45	Poietu —	02
In Mouse-bole, at St. Mat-		-	On the Coast of Portugal-	02
thew's, & within Mount's-Bay		30	In Plymouth, and before	3
In Milford, at Moonless and		١	St. Paul's	05
at St. Maloes		15	In the Haven at St. Paul's	06
Between Mouse - Hole, and			Before Podessemeck -	
Falmouth, & in Milford-Haven		30	Thwart of Plymouth-	
In St. Magnes Sound and	·	٦	At the Race of Portland -	
Magnes Castle ———	08	15		
At the Isle of Man -	00	00	0.	
Before Margate -				12
N.			R.	
At Newport Half-Tide -	12	00	At Rochester -	00
At the West-end of the			At Ramkins —	01
	1.00	45		
	22.75		bood's-Bay, and from the Race	
보고 이 사용하다 중에 대한 성장을 통해 시간 성상에 보았습니다. 하고 이번 경기를 하지만 하지 않는데 수 있는데 하다고 있다.			to the Pole-Head -	03
Before St. Nicholas -	06	45	At Rouen and before Rochel	02
At the Needles, at the Isle	3.		In Ramsey	05
	08	15	s.	3
All the Coast of Normandy		-	In the Sleeve, between U-	
A TABLE OF THE ACT OF		30	Chant and Scilly, at the Shoe,	
Between the Naze and		,	at the Spitts, at Southampton,	
그는 사람들은 아니라 아니라 아니라 아니는 사람들이 얼마나 나는 사람들이 되었다. 그는 사람들이 아니라	2. 2. 2.	16	and along the Swin —	10.00
IT WINCIPH OF THE COL		- 2	and by the comment	U

	H M	l and the second of the second	HIM
Upon the Coast of Spain,		Without Ushant -	0600
Upon the Coast of Spain, and in Shetland	0300	St. Vallery———	1030
At Scilly, in the Sound,			
Scarburgh, and at Staples -	03 45	W.	
At Seven Isles, without the		At Winchelsey -	00 45
Haven in the Broad-Sound -	04 30	At the Weilings, and from	
At the Mouth of Severn,		the West-end of the Wight -	
between Scilly and the Lizard,	111	Before the Weilings	
between Scilly and the Lizard, at the Spurn and Stockton—	05 15	At Whithy —	0300
Without Scilly, in the		In the Sea of Wales and	
Channel, and at Salcomb			04 30
At Sedmouth & at the Start	06 45	In Wales ————	
Off the Start in the Channel	1 - 1		1 7
Within the Seyn and before		at Waterford -	
Shelburgh -			
At Shorehom ————	09 45	At the Ness, by Wiering	-1 1.5
At Seyn-Head -	1030	ben, at Winterton	07 20
		Thwart of the Isle of Wigh	t
T.		in the Channel, all within the	e
Within Tervere -	0045	Wight, between the Wight and	d
Before Tervere, before the	1.3	Beachy by the Shore -	0815
Thames and at Tinmouth -	1 1		
Before the Tees & Tinmouth		and on Wieringhen-Flats	
before the Bay of Tinmouth-	The second second		109
At the Cliffs of the Texel			
In Torbay and before the		Before Yarmouth -	-01 30
Texel	0600	At Youghall —	
In the Road of the Texel	0720	At Yarmouth —	04 30
At Torgen	0945	In Yarmouth Roads, and	08 15
216 1018011	09 75	Yarmouth Haven —	2 4 4 1
U.		Tar mound 13aven	- 10 30
Before Ureck-	1200	Z.	A
At Use		On the Coast of Zealand -	-
Between Ushant & the Main	0300		01 30
		In the Zerick-Sea	-03 00
In the Vourd, at the Bay,		the said, all large	100
within Usbant —	04 30	The second of the first the second	- 11
rooU	N/		rit
	M		The

# The Use of the TIDE-TABLE, in finding the Time of High-Water.

I N this Table the Names of the Places being set in Alphabetical Order, they will always be found under the Letter they begin with, as for Example, London, will be found under the Letter L, Torbay under T. Scilly under S, &c. and the Figures right against any Place shews the Time of High-Water at that Place, on the Full and

Change of the Moon.

Then if it be required to find the Time of High-Water at any Place upon any given Day, First, (by the Tables of Numbers and Times answering) find the Number and Time answering for that Day, (as before taught) and to that Time, add the Hours and Minutes that stand in the Tide-Table against the Place you would know the Time of High-Water at, the Sum, if it does not exceed 12 Hours, will be the Time of High-Water required; but if it should be more than 12 Hours, then subtract 12 from it, and the Remainder will be the Time of High-Water.

#### EXAMPLE I.

Suppose it was required to find the Time of High-Water at London, on 30th of January, 1773

By the Table of Numbers, I find the Number for the 30th of January, to be 17, with which Number entring the Table of Times, I find the Time answering to be 5 H. 36 M. then looking for London in the Tide-Table, I find against it 3 Hours, which added to the Time before found, gives 8 H. 36 M. for the Time of High-Water at London, on the 30th of January, 1773.

#### EXAMPLE II.

Suppose it was required to find the Time of High-Water at St. Hellens, on the 19th of August, 1774.

Having found the Number (as before) to be 22, and the Time answering to be 9 H. 36 M. I look in the Tide-Table under the Letter H, for St. Hellens, against which I find 10 H. 30 M. which added to the Time (as before) 9.36 gives 20,06, from which subtract 12,00 and the Remainder 8 H. 06 M. is the Time of High-Water required.

### A TABLE of the Sun's Declination for the Years 1765, 1769, 1773, and 1777.

M. Day.	1	Jan.		reb.		March		April		May		June		July		Auguit	,	Septem.		October		Novem.	1	Decem.
1017	Sou	th	Sou	ith	Sou	ıth	No	rth	No	rth	No	orth	No	rth	No	orth	No	rth	Soi	ath	Son	ith	Son	ıth
1	22	58	16	56	27	22	04	45	15	14	22	08	23	07	17	56	08	<b>c</b> 8	03	23	14	37	21,	55
2	22	53	16	39	06	59	05	08	15	32	22	16	23	02	17	41	07	46	03	46	14	56	22	04
3	22	47	16	21	06	36	05	31	15	49	22	23	22	57	17	25	07	24	24	09	15	15	22	13
4	22	41	10	03	00	13	05	54	16	24	22	30	22	52	17	09	07	02	04	33	15	34	22	21
5	-	3.4	15	45	5	30	_	-		-4	_	37	_	4/	_	53	_	39	4	50	1.5	52		20
6	22	26	15	26	05	27	06	39	16	41	22	43	22	41	16	37	06	17	05	19	16	10	22	35
7	22	19	15	07	05	03	07	02	16	57	22	49	22	34	16	20	05	55	05	42	16	28	22	42
												54												
												59												
10	21	53	14	10	03	53	-		17	45	-3	04		13	15	20	-	40	00	51	17	19	23	00
11	21	43	13	50	03	30	08	30	18	10	23	08	22	05	15	10	04	28	07	13	17	36	23	0.
12	21	34	13	30	03	06	08	52	18	16	23	12	21	56	14	52	04	01	07	3.6	17	5.2	23	0
13	21	23	13	10	02	42	09	14	18	31	23	15	21	48	14	34	03	38	07	58	18	08	23	1
14	21	13	12	50	02	19	09	30	18	45	23	18	21	39	14	15	03	14	08	21	18	24	23	1
15	21	02	12	29	01	55	09	57	10	59	23	21		29	13	50	OZ	51	00	43	10	39	23	19
												23												
												25												
												26												
												27												
20	20	00	10	43	-			42	-	05	-5	28	-	3/			_	>>	-	32	19	51	23	2
21	19	47	10	21	00	27	12	02	20	17	23	28	20	25	11	59	00	31	10	54	20	04	23	2
22	19	33	09	59	00	51	12	22	20	29	23	28	20	13	11	39	00	08	11	15	20	17	23	2
23	19	19	09	37	01	.14	12	42	20	41	23	27	20	01	11	19	301	115	111	36	20	29	23	2
34	19	04	109	15	01	38	13	02	20	52	23	26	19	40	10	50	00	39	11	57	20	41	23	2
25	10	49	08	53	02	02	13	21	_	_	-3	24	19	30	-	30	-	-	-		20	53	23	2
26	18	34	08	30	02	25	13	41	21	13	23	22	19	22	10	17	01	26	12	39	21	05	23	2
27	1.8	19	08	08	02	49	14	00	21	23	23	20	119	09	109	56	10	49	12	59	21	16	23	2
	18			45					21	33	23	17	18	55	09	34	02	13	13	19	2 1	26	23	
	17				03	1.10	14				23	14	18	41	09	13	02	30	13	39	21		23	
1 12 11 13	17	. 7			03			. 56	21	51	23	10	10	11	08	51	132	59			21	40	23	
11	117	13	-		104	. 22	1	100	1-2			12. 7.3	1.0		.00	3	1	-	14	10			23	0

### A TABLE of the Sun's Declination for the Years 1766, 1770, 1774, and 1778.

M. Day.		Jan.		reb.		March		April		May		June		July		August	,	Septem.		October		Novem.		Decem.
	Soi	ath	Sou	ith	Sou	ıth	No	rth	No	rth	No	orth	No	rth	No	orth	No	rth	Soi	uth	Sou	ith	Soi	ath
1	23	oc	17	00	07	28	04	39	15	09	22	06	23	c8	18	00	08	13	03	17	14	33	21	5.
2	22	54	16	43	0.7	05	05	02	15	27	22	14	23	03	17	45.	07	51	03	41	14	52	22	0
3	22	48	10	25	00	42	05	25	15	45	22	21	22	59	17	29	07	24	24	04	15	11	22	11
4	22	42	10	07	00	19	05	48	10	03	22	29	22	54	17	13	07	07	04	27	115	29	22	1
_5	22	35	15	49	05	50	00	11	10	20	_	35	22	40	10	57	00	45	04	50	15	40	22	Z
6	22	28	15	31	05	32	06	34	16	37	22	42	22	42	16	40	06	23	05	13	16	06	22	34
7	22	21	15	12	05	09	06	56	16	53	22	47	22	36	16	24	56	00	05	36	16	23	22	4
		15																						
		04																						
10	21	55	14	14	03	59	08	03	17	41	23	03	22	15	15	32	04	52	00	45	17	15	22	5
11	21	46	13	55	03	35	08	25	17	57	23	07	22	07	15	14	04	29	07	08	17	32	23	0
		36																						
13	21	26	13	15	02	48	09	09	18	27	23	15	21	50	14	38	03	43	07	53	18	04	23	1
14	21	15	12	54	32	24	09	30	18	42	23	18	21	41	14	20	03	20	08	15	18	20	23	1
15	21	04	12	34	02	01	09	52	18	56	23	20	21	32	14	01	02	57	08	38	18	36	23	1
16	20	53	12	13	01	37	10	13	19	10	23	23	21	22	13	42	02	34	09	00	18	51	23	2
		41																						
18	20	29	11	31	00	50	10	55	19	37	23	26	21	01	13	04	01	47	09	44	19	20	23	2
19	20	16	11	09	00	26	11	16	19	50	23	27	20	51	12	44	01	24	10	06	19	34	23	2
20	20	03	10	48	00	02	11	37	20	02	23	28	20	40	12	24	01	00	10	27	19	47	23	2
21	10	50	10	26	No	0.21	11	57	20	15	23	28	20	28	12	04	00	37	10	40	20	01	22	2
22	119	36	10	04	00	45	12	17	20	26	23	28	20	16	11	44	00	14	11	io	20	14	23	2
2	110	22	00	42	101	00	12	37	20	38	23	27	20	04	11	24	Sou	011	11	31	20	26	23	2
24	119	08	109	20	10	32	12	57	20	49	23	26	19	52	11	03	00	33	11	52	20	39	23	2
2	18	53	08	58	01	56	13	17	21	00	23	25	19	39	10	43	00	57	12	13	20	50	23	2
20	5,15	3 38	08	26	02	10	12	26	21	11	23	23	10	26	10	22	01	20	12	34	21	02	22	2
2	7 18	2:	08	12	02	41	12	55	21	21	23	21	10	12	10	01	01	44	12	54	21	13	23	2
2	8.18	3 0	07	50	03	06	14	14	21	31	23	18	18	58	09	40	OZ	07	13	14	21	24	23	1
		7 50			103	30	14	33	21	40	23	15	18	44	09	18	02	30	13	34			23	
		7 34			103	53	14	51	21	49	23	11	18	30	08	57	02	54	13	54	21	-	23	1
3	11:				04	16		10	21	58	1		18	15	108	35		1	14	14	Sil	20	23	0

### A TABLE of the Sun's Declination for the Years 1767, 1771, 1775, and 1779.

M. Day		Jan.	1-0	reo.		March		Aprıı		May		June		Juny		Auguit		septem.		October		Novem.		Dec.
	Sou	ıth	Sou	ıth	Sou	th	No	rth	No	rth	No	rth	No	rth	No	rth	No	rth	Sou	ıth	Sou	ith	Sou	ith
1			17																					
2	22	56	16	47	07	10	04	57	15	23	22	12	23	04	17	48	07	57	03	35	14	47	22	00
3	22	50	16	30	06	47	25	20	15	41	22	20	23	00	17	33	97	35	03	5.8	15	00	22	09
4	22	44	16	12	06	24	05	43	15	58	22	27	22	55	17	17	07	13	04	21	15	25	22	17
5	22	37	15	54	00	01	06	05	16	16	22	34	22	49	17	01	06	50	74	45	15	43	22	25
6	22	30	15	35	05	38	56	28	16	33	22	40	22	44	16	45	06	28	05	08	16	01	22	32
7	22	23	15	17	05	15	06	51	16	49	2	46	22	37	:6	28	06	05	05	31	16	15	22	39
			14																					
9	22	06	14	39	04	28	27	30	17	22	22	57	22	24	15	54	05	20	06	17	10	54	22	51
10	21	57	14	19	04	04	97	58	17	38	23	02	22	10	15	30	04	58	26	4c	17.	11	22	5
11	21	48	13	59	03	41	08	20	17	53	23	06	22	09	15	19	04	35	07	02	17	28	23	0:
12	21	38	13	40	03	17	08	42	18	09	23	10	22	01	15	01	04	12	07	25	17	44	23	07
			13																					
			12																					
-		- (	-		_		-	-0	_		-		-		-		_		-		-		-	
			12																					
			11																					
10	20	10	11	10	00	12	11	11	10	33	22	27	20	52	13	40	01	20	10	30	10	20	22	2
20	20	06	10	53	00	08	11	32	19	59	23	28	20	42	12	29	21	06	10	22	19	44	23	27
21	10	£2	10	22	No	.16	-	52	20	12	22	28	20	21	12	00	20	42	10	44	10	-8	22	28
			10																					
			09																					
24	10	11	09	26	01	27	12	52	20	47	23	26	119	55	11	08	00	28	11	47	20	36	23	20
25	18	57	09	03	01	50	13	12	20	58	23	25	19	42	10	48	00	51	12	08	20	48	23	2
26	18	42	08	41	02	14	13	31	21	08	23	23	19	20	10	27	01	14	12	20	20	50	23	2
27	18	26	08	19	02	37	13	51	21	18	23	21	19	15	10	of	101	38	12	49	21		23	
			07					10	21	28	23	19	119	02	09	45	02	01	153	09				
	17				03		14	28	21	38	23	16	18	4.8	09	23	02	25	13	29	21		23	
30	17				03	47	14	47		47	23	12	18	33	109	02	OZ	48	13	49	21	41	23	1
31	17	21	1		04	10	1		21	56	1		118	19	08	40	I		14	09	1		123	0

### A TABLE of the Sun's Declination for the Years 1768, 1772, 1776, and 1780.

M. Day		Jan.		Feb.		March		April		May		June	-	July		August		Septem.		October		Novem.		Dec.
_	Soi	uth	Soi	uth	Soi	uth	No	orth	No	orth	No	orth	No	orth	No	orth	No	orth	Soi	uth	Soi	uth	Soi	uth
1	23	02	17	10	07	17	04	50	110	18	22	10	23	0:	17	E 2	08	03	03	20	14	42	21	58
2	22	5/	16	54	06	54	05	13	15	36	22	18	23	01	17	37 21	97	41	03	52	15	01	22	00
4	22	46	16	17	06	08	06	00	15	54	22	25	22	50	17	05	07	-6	04	28	15	28	22	15
5	22	39	15	59	05	44	06	22	16	28	22	38	22	45	16	49	06	34	05	01	15	56	22	30
`	-				-	-	-	_	-	_	-	-	-	-	-		-	-	-	-	-	-	-	
7	22	25	15	2.2	04	-8	07	95	10	40	122	44	22	39	16	32 16	00	12	05	48	16	14	22	37
8	22	17	15	03	04	34	07	30	17	17	22	56	22	35	15	59	05	26	06	10	16	10	22	44
9	22	08	14	44	04	11	07	52	17	22	22	01	22	18	15	41	05	04	06	33	17	07	22	56
10	22	00	14	24	03	47	08	14	17	49	23	05	22	11	15	24	04	41	06	56	17	23	23	01
11	21	51	14	05	03	24	08	36	18	04	23	00	22	03	15	06	04	18	07	10	17	40	23	of
12	21	41	13	45	03	00	08	58	18	19	23	13	21	54	14	48	03	50	07	41	17	56	23	10
13	21	31	13	25	02	37	09	19	18	34	23	10	21	40	14	29	03	32	08	04	18	12	23	14
14	21	21	13	05	02	13	09	41	18	59	23	19	21	37	14	11	03	10	08	26	18	28	23	17
15	21	10	12	44	01	49	10	02	19	03	23	22	21	27	13	52	02	46	08	48	18	43	23	20
16	20	59	12	24	01	26	10	24	19	16	23	24	21	17	13	33	02	22	09	11	18	58	23	23
17	20	47	12	03	01	02	10	46	19	30	23	25	21	07	13	14	OI	59	09	33	19	12	23	25
18	20	35	11	42	00	38	11	05	19	43	23	26	20	57	12	54	01	36	09	54	19	27	23	2
19	20	22	11	20	NT-	14	11	20	19	50	23	27	20	45	12	34	00	13	10	10	19	40	23	27
_	20	10	10	59	NO	.09	_	47	20	68	23	28	20	34	12	15	00	40	10	38	19	54	23	28
21	19	57	10	37	00	33	12	07	20	20	23	28	20	22	11	54	00	26	10	59	20	07	23	28
22	19	43	10	10	00	50	112	27	20	32	23	27	20	10	11	34	00	02	11	20	20	20	23	28
21	19	29	20	54	01	20	12	47	20	43	23	20	19	58	11	14	301	121	11	41	20	32	23	27
25	19	01	09	09	02	07	13	26	21	05	23	24	19	32	10	53 32	00	08	12	23	20	56	23	24
26	18	15	28	47	02	21	12	15	21	16	22	22	10	10	-	12	21	21	12	12	71	07	22	22
27	18	20	08	25	02	54	14	04	21	26	22	10	10	20	00	50	CI	55	12	93	21	18	22	10
		15	08	02	23	18	14	23	21							29		18				29	7 8	16
29			07	39	03	41	14	42	21	44	23	13	18	33	20	08				41	19.00	39	-	12
30		42			04	04	15	oc	21	53	23	10	18	23	08	46	03	05	14	03		48		08
	17	26	-46		04		S.F.		22		1	1	18	08	08	24	22		14	23			23	00

A	TA	B	LE	of	the	Variation	of	the	Sun's	Declination	to
				ever	y I	o Degrees	of	Lor	gitude.		

Degrees of Longitude from the Meridian of LONDO	Degrees of	Longitude	from	the	Meridian	of ]	LO	N	D	0	N
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Daily Vari.	10	20	30	40	50	60	70	80	90	100	110	120	130	140	150	160	170	180
Min.	min	min	min	min	min	min	min	min	min	min	min	min	min	min	min	min	min'	m:n
2	-0	0	0	0	0	0	0	0	0	I	I	1	I	I	1	1	I	I
3	0	0	0	0	0	0	I	1		I	I	I	I	I	I	I	I	I
4	0	0	0	0	1	I	I	I	1	I	I	I	I	2	2	2	2	2
3 4 5	0	0	0	0	I	1	1	I	I	1	I	2	2	2	2	2	2	2
6	0	0	0	I	I	I	I	1		2	2	2	2	2	2	2	3	3
7	0	0	I	I	I	1000		1 .7	10 70	2	2	2	3	3	3	3	3	3 4
7	0	0	1	1	I	I	I	1		2	2	3	3	3	3 4	3	4	4
9	0	0	1	I	I	I	2	2	2	2	3	3	3 3	3 3 3	4	4	4	4
10	0	1	1	1	1	1000	1. 1. 1. 1.		3	3	3	3	4	4	4	5	5	5
II	0	1	1				1	3	3	3	3	4	4	4	5	5	5	5
12	0	1	1		1 3				3 3 3	3 3 4	4	4	4	5	5 5	5 5	6	6
13	C	1	I	I	2	2	2	3	3	4	4	4	5	5	5	6	6	6
14	C	1	I	2	2		3	3	3 4	4	4	5	5	5	6		7	7
15	0	1	I				33333	3 3	3 4	4	1 5	5	5	6		7	7 8	78
	0		I	and the		1 3	3 3	3 4	1 4	H 5	5 5	5	1			7 7	7 8	1 8
17	0	1	I	2	2	3	3	3 4	1 4	1 5	5	6	6	7	7		8	
18	,	1			3	3	3 4	1 4	4	5 5	5 6	6	1 7	7	7	7 8	8 9	9
19	1	1	2	2	3 33 3	3 3	3 4		1	5 5 5	5 6			7 7 7 8	7 7 8	7   8		1 9
20	1	[ ]	1 2	2				1 4						7 8		3	ol c	IIC
21	1	1 .1	2	2 2	2	3 4	1 4	1 .	5	5	6 6	5 7	7 8	3 8	3 9		910	10
22		1	1 2	2	2	3	4	4	5	6	6	7 7 7 8	3 8	3 9	9	9 1	010	1.
23		I		2 3	3 3	3 4	4	4	5 5	6	6 3	7 8	3 8	3 9	9 10	I	010	I
24		I	1 2	2	3	31.	4	5	<b>J</b> 1	61 N	71	71 8	3 6	9 0	9/10	110	II	1 1:

# To find the Sun's Declination, by the foregoing TABLES.

ACH Page of the foregoing Tables contains the Sun's Declination for the four Years that it is mark'd with at the Top, and is divided into thirteen Columns; the first of which to the Left-Hand, shews the Day of the Month, and the other Twelve the Months of the Year, so that if it be required to find the Sun's Declination for any Day, at suppose for Example, on the 21st of August, 1767: First I look for that Table that has 1767. at the Top of it, and then right against the 21st Day of the Month, and under August, I find 12, 10. which shews the Sun's Declination to be 12 Degrees 10 Minutes North; according to the Title at the Top of the Column.

The Sun's Declination in these Tables being calculated for the Meridian of London, if you should be considerable to the Eastward, or to the Westward of London, it will cause some Alteration in it; to correct

which, the

Table of Variation of the Sun's Declination is to be used as follows.

First, Look out the Declination for the given Day of the Month, and for the Day following it, and subtract the lesser from the greater, the Remainder is the daily Variation.

Second, Observe whether the Declination be increasing or decreasing, which you may know thus; if the Declination for the Day following the given Day be biggest, than it is increasing; but if it be least, it is decreasing.

Third, Look for the Daily Variation in the first Column of the Table, and see what Number stands right against it, and under the given De-

grees of Longitude; which Number is to be used as follows.

If the Difference of Longitude be Easterly, and the Declination increasing, it must be substracted from the Declination found in the Tables for the given Day; but if the Declination be decreasing, it must be added.

If the Difference of Longitude be Westerly, and the Declination increasing, it must be added; but if the Declination be decreasing, it must be substracted; the Sum in one Case, and the Remainder in the other will be the Sun's Declination at Noon in the Longitude required.

# A TABLE of the Sun's Right Ascension.

-		Jan.		Feb.		1	March		April		May		June		Tuly			Augult		Septem.		Othohor			Novem.		Dec.	
-	Н	M	H		M	H	M	H	N	NE	IN	A I	1 1	ME	İ	M	H	M	H	D	A	1	M	H	N	1 H	1	IV
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4	19	0	3 2	I	14	23	0	100	5	5 0	2 4	7 0	4	4	6	50	00	02	2 10	0 0	7	12	46	1.	4 4	3 1	6	9
5	19	07	7 2		10	23	0		5	9	2 5	-	4	1		77	_		_		_		_	-		- -		_
7	-					-	0		1 (	2	2 9	40	4	0	07	03	09	06	5 1	1 (	I	12	49	1	4 4	7 1	6	53
		-			-		-	- 10		201/	12 1					<b>U</b> /			-			-		_				
		-	-10		-			-10		1 21/	72 (	- M	1		$\mathbf{u}$		100				1					,,,		
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											03																	
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	1			111					_	_	-	-	-	-	7.7		_			100	Variation.					3 3		
16	1			22	0	1/2	2 4	16	10	39	03	34	05	40	07	4	40	9 4	14	11	37	1	3 2	6	15	28	17	3
20	0 2	0	12	22	1	7 0	0	00	91	54	03	49	05	5/		_	_	9	29		3.		, ,				_	-
2	-		7				À		~	- 9	03	F 2	06	01	108	0	4	10	03	11	55	1	3 4	15	15	49	18	C
2	1 2	0	10	22	2		0	04	02	01	03	57	06	0	08	0	8	10	06	11	59	1	3	19	15	53	18	9
2	2 2	0	20	22	2	3	00	11	OZ	05	04	01	06	0	08	1	2	10	10	12	0	2 1	3 5	53	15	57	18	C
2	1 2	0	20	22	2 3	2	00	15	02	00	04	06	06	1	3 08	1	6	10	14	12	0	6 1	3	57	16	02	18	
2	5 2	0	33	21	3	6	00	19	02	1	04	10	06	1	7 08	3 2	20	10	17	12	0	9 1	4 '	00	10	00	10	
2	6 2	20	37	2	2 3	9	00	22	02	16	5 04	14	100	2	2 0	0 2	23	10	21	12	1	3	4	08	16	14	18	3
2	7/2	05	41	2:	2 4	131	00	20	02	2	0104							10									18	
					2 4	17	00	30	02	2	9 04	2	5 0	2	40	8	35	10	32	12	2	4	14	10	10	2	118	3
	9						00	33	10	2 2	8 04	20	000	5 3	8 0	8	39	10	36	1:	2 2	7	14	20	16	2	7 1 1	)
	31	20					00			,	04	1 3	4	,	2	8	43	10	39	1			14	24	1		13	8

# A TABLE of the Right Ascension and Declination of some of the most noted Fixed Stars.

The Names of the Stars.		ght en.	Dec	lina- on
The Ivames of the Stars.		M.	D.	M.
The Bright Star of Aries	01	53	22	17 N
Medusa's Head, Algol	02	52	39	59 N
The Bright-side of Perseus	03	07	48	58 N
The Bull's Eye, Aldebaran -	04	22	15	59 N
The Goat Star, Capella	04	59	45	43 N
The Bright-foot of Orion, Regal -	05	01	08	28S
The Northern Horn of the Bull -	05	09	28	21 N
Orion's Left Shoulder	05	10	06	04 N
The Southern Horn of the Bull -	05	21	20	56 N
Middle Star in Orion's Belt -	05	22	10	25S
Orion's Right Shoulder—————	05	52	07	20 N
Auriga's Right Shoulder — — — — — Bright Foot of Gemini — — — — — — — — — — — — — — — — — —	05	44	44	54 N
Bright Foot of Gemini-	06	20	16	38 N
The Dog Star, Syrius -	06	34	16	23S
Castor, or the Head of the Northermost Twin -	07	17	32	24 N
The little Dog Star, Procyon-	07	24	05	49 N
Pollux, or the Head of the Southermost Twin	07	28	28	36 N
Hydra's Heart	09	16	07	37 S
The Lyon's Heart, Regulus-	09	53	13	09 N
The Lower of the Pointers —	10	45	57	41 N
The Upper of the Pointers -	10	46	63	03 N
The Lyon's Tail, Deneb	11	35	15	55 N
Upper of the two last in the square of Great Bear	12	02	58	35 N
The first in the Great Bear's Tail-	12	41	57	18 N
The Virgin's Spike ——————	13	12	09	52 S
The middle of the three in the Great Bear's Tail-	13	11	56	22 N
Last but one in the Tail of Hydra -		04	21	43 S
Last in the Great Bear's Tail -	13	36	50	31 N
Areturus — — — — — — — — — — — — — — — — — — —	14	03		30 N
Bright Star in the Southern Ballance-	14	35		53 S
Foremost Guard ————————————————————————————————————	15	51	75	15 N Brigh

## A TABLE of the Fixed Stars.

		ght		lina-
The Names of the Stars.	Afc	en.	ti	on
	H.	М.	D.	M.
Bright Star of the Crown -	15	22	27	33 N
Bright Star in Serpent's Neck -	15	31	07	18 N
The Scorpion's Heart, Antares -	16	14	25	5 · S
The Head of Hercules —	17	03	14	40 N
In the Head of Serpentarius ————	17	22	12	47 N
Bright Star in the Dragon's-Head-	17	50	51	32 N
Lyra, or the Harp —	18	27	38	33 N
Swan's Beak —————	19	17	27	29 N
Bright Star in the Eagle	19	39	08	14 N
The Swan's Tail	20	33	44	19 N
Pegasus's Mouth	21	27	08	39 N
Fomelhaut — — — — —	22	42	30	55 S
Pegasus's Wing, Marchab	22	53	13	53 N
Pegasus's Leg, Scheat	22	52	26	43 N
Capbus's Knee — — —	23	20	76	07 N
The Head of Andromeda	23	54	27	34 N
End of Pegasus's Wing, Algenib	23	58	13	39 N
Pole Star	00	42	88	00 N
Girdle of Andromeda	00	53	34	05 N
A TABLE of the Right Ascension		ght	Dec	clina-
and Declination of the Crosiers.		cen.	t	ion
and Decimation of the crojurs.	H.	M.	D.	М.
The Westermost of the two middle Stars	12	03	57	11 S
The Eastermost	12	33	58	06 S
The Northermost or highest Star -	12	16	55	30 5
The Southermost or lowest	12	12	61	31 8
				T

To work an Observation, or to find the Latitude of the Place by the Tables of the Sun or Stars Declination, and their Zenith Distance, &c.

Note, WHEN you take an Observation of the Sun, by the common Sea Quadrant, the Degrees and Minutes that your sight Vane stands at, being added to the Degrees that your Shade or Glass Vane stands at, will give the Zenith Distance (or Complement of the Meridian Altitude) with which and the Declination found in the Tables, you may find the Latitude as follows.

First, Take Notice whether the Sun or Star be to the Northward or to the Southward of you at the Time of Observation; if they are to the Northward, call your Zenith Distance North; or if they are

to the Southward, call it South. Then,

Second, If the Zenith Distance and Declination are both North, or both South, substract the lesser from the greater, the Remainder will be the Latitude you are in, of the same Name with the Declination, if that be greater than the Zenith Distance, otherwise of a contrary Name.

Example 1st, Being at Sea on the 23d of August, 1767, I observed at Noon, and had on my Quadrant 8.34, (and the Sun to the Northward of me) what Latitude am I in?

Zenith Distance — 8. 34 North
Declination — 11. 30 North
Latitude by Observation — 2. 56 North

Example 2d, Being at Sea on the 23d of December, I took the Altitude of the Dog Star Syrius, (on the Meridian to the Southward of

me) 60 00, I would know the Latitude?

Note, In all Cases (except where the Object is observed on the Meridian below the Pole) if the Meridian Altitude be given instead of the Zenith Distance, (as it is in this Example) then subtract it from 90.00, and the Remainder will be the Zenith Distance.

Meridian Altitude from 90. 00, leaves the Zen. Dift. 30. 00 South Star's Declination, (by the Table) — 16. 23 South Latitude by Observation — 13. 37 North

T

#### To work an Observation.

Case the 2d, If the Zenith Distance and Declination be one North, and the other South, add them together, and their Sum will be the Latitude in, of the same Name with the Declination.

Example 1st, Being at Sea, on the third of November, 1767, I observed at Noon, and had on my Quadrant 8.17, (and the Sun to the Northward

of me) I demand the Latitude?

Zenith Distance — — — — 08. 17 North Declination — — — 15. 06 South Latitude by Observation — — 23. 23 South

Example 2d, Being at Sea on the 21st of June, 1769, I took the Altitude of the Bright Star in the Harp, Lyra, (on the Meridian to the Southward of me) 51.00. I demand the Latitude.

Complement Altitude, or Zenith Distance — 39.00 South Star's Declination — 38.33 North Latitude by Observation — 77.33 North

The foregoing Rules are for observing by the Sun or Stars, when they are at their greatest Altitude, or upon the Meridian above the Pole; but as in some Parts of the Earth the Sun does not set for several Days, but some Stars never set; in that Case they may be observed upon the Meridian, twice in the 24 Hours, that is, once at their greatest Height (as before) and again, when they are at the lowest, or upon the Meridian below the Pole; to work which Observation take the following Rule.

Add the Complement of the Declination to the Meridian Altitude, the Sum is the Latitude of the same Name with the Declination.

Example, Being at Sea, I took the Altitude of the Pole Star on the Meridian below the Pole, 46. 21, I demand the Latitude?

Meridian Altitude — 46.21
Complement Declination — 01.56 North
Latitude by Observation — 48.17 North
The

Remarks by the Reviser. The Author in the above Rules and Examples, takes the Sum of the Numbers found on his Quadrant, and works with it, as if true, to find the Latitude: But the Latitude so obtained will be several Minutes from the true Latitude. For obtaining which, the Zenith Distance as found by the Quadrant, must be first corrected, as shewn in the Mariner's Compass Restified.

The Use of the TABLES of the Sun's and Stars Right Ascension, in finding what Time any known Star will be upon the Meridian, on any given Day.

Rule, Look for the Right Ascension of the Sun and Star in the foregoing Tables, and subtract the Sun's Right Ascension from the Star's; but if the Sun's Right Ascension be biggest, add 24 Hours to the Star's Right Ascension, and then subtract the Sun's from it, the Remainder will be the Time of the Star's coming to the Meridian after Noon.

Example 1st, What Time will the Lion's Tail be upon the Meridian, on the 14th of April? h. m.

Stars Right Ascension — — — — 11. 35
Sun's Right Ascension — — — — 01. 32

Time the Star will be on the Meridian - 10.03 at Night. Example 2d, What Time will the Bull's Eye be on the Meridian, on the 26th of October?

Star's Right Ascension 4h. 22m. add 24h. makes - 28. 22

Sun's Right Ascension — — — 14.04

Time the Star will be on the Meridian — — 14.18Asternoon

that is, at 18 m. past 2 in the Morning.

To find what Star will come upon the Meridian, at any given Time. Rule, Add the Time from Noon, to the Right Ascension of the Sun, the Sum will be the Right Ascension of the Star required to be known, with which enter the Table of the Star's Right Afcension, and find what Star's Right Ascension agree with, or comes the nearest to it, and that is the Star required.

Example 1st, I would know what Star would be on the Meridian,

about Eight at Night, on the 7th of April.

Sun's Right Afcension — — 01.06

Time from Noon — — 08.00

Right Asc. of the req. Star, the nearest to which og. o6 is Hydra's Heart Example 2d, I would know what Star would be on the Meridian, at

Rt. Asc. of req. Star, nearest to which in the Tables 20. 37 is Swan's Tail.

# A TABLE of the Latitudes and Longitudes of Places accounting the Longitudes from the Meridian of LONDON.

Places Names,	La	titude	Lon	gitude	Places Names.	La	titude	Lor	gitude
The Coast of England.	D.	м.	D.	м.	Tage (	D.	м.	D.	М.
DErwick	55	48	01	45W	Aberdeen -	- 57	24 N	01	40W
D Newcastle —		12	01	30W	Dundee	-1;6	28 N		40W
Stockton	54	33	10	25 W	Edinburgh -	-155	58 N	02	59W
Spurn ———	53	45	00	13 E					100
Yarmouth —	52	40	01	40 E	The Coa	ft of	Irelana	<b>!</b> .	
London-		32	00	00	And the street of				
North Foreland—		25	10	24 E	Dublin	- 53	12 .	06	56
Beachy Head —	50	46_	co	25 E	Wexford -	- 52	13	07	27 .
Dunnose -	50	38 0	101	23	Waterford——	- 52	99 North	08	40 €
Portland -	50	30 =	02	44	Cork——	- 51	49 7	09	30 €
Start ———	50	07 -	03	47	Cape Clear —	- 51	17	111	10
Lizard ———		57 8	05	14	Limeric —	- 52	23 2	09	35 3
Land's End —		06 2	06	00 €	Galway ———	- 53	07 ₹	09	400
St. Mary Scilly-	149	57 6	06	10 %	Slime Head -	- 53	Latitude 23 07 20	11	500
Hartland Point-		06	04		Londonderry —	- 55	00	07	500
Lundy Isle -	51	20	04	35 5	Bellfast ———	- 54	39	06	30
Briftol	51	33	04	35 gitud	The Coast of H	I.11.	dand 1	Flan	down.
St. David's Head -	-51	50	05	22 5	The Coalt of I.	ioiiani	a and I	· tuni	4613.
Barfey Isle ———		44	05	000	Scaw —	-157	30	110	20
Holy-head -	153	23	04	50	Helighland —		24	08	35
Liverpool —	53	20	03	00	Hambrough	- 52	41		
Whitehaven -	- 54	25	03	30	Embden	123	41 Z	07	35 H
Carlifle	-154	47	103	05	Hambrough ————————————————————————————————————	- 153	15 5	07	30
					The Texel	- 3	15		109
The Coaft	of .	Scotlan	d.		Amsterdam -	- 52	23 0	05	0409
			-		Rotterdam	- 51			30 5
Classow	55	52	04	05	The Brill		55 de	04	00 0
Glafgow ———— N. Part of Sky Isle —	22	3-	05	05	01 .	-51	14	03	43
N. Part of Lewis Isl		45 Z	07	45 W	Calais	-150	58	01	54
St. Kildry———	-57	52 3	00	45 =				-	
Farra Head —	- 58			100	The Coast of F	rance	and P	ortu	gal.
Isles of Orkney.	59	34 10	.02	45 Longia	Diep-	-149	56 N	loi	09 I
Shetland S. Point-		04 8		00 0	Cape de Hague-	- 49	47 N		00 W
Buchaness -	100000		01	18 6	Gaskets -	- 19	50 N		20 W
Buchaners -	57	45 "	1		Guernsey	-49	33 N		20 W

# A TABLE of Latitudes and Longitudes.

Places Names.	La	titude	LOI	gitude	Places Names.	La	titude	Lon	gitude
The Coast of France and Portugal.	D.	м.	D.	М.		D.	М.	D.	м.
Morliax ————	48	33	03	49	Ancona —	43	40	14	26
Jihant ———	48	30	05	02	Venice —	45	25	12	10
Breaft	48	23	04	25	· · · · · · · · · · · · · · · · · · ·	38	10	22	52
Penmark -	47	48	04	24			33	22	41
Bell-Ifle	47	20	03	16	Cape St. Angelo -		32	23	56
Vantz —	47	14	01	39	Athens -	37	58	24	05
fland Dieu -	46	34 Z	02	13 5	Cape Martelo S. ]	I A Is			
fle of Ree	46	10 3	10	300	part of Negropont	38	07	25	03
Rochel —	46	105	10		Cape Monte Sancto	40	26	25	02
Bourdeaux	44	50 2	00	3800	Gallipoly —	40.			20
Bilboa ———	43	29 =	02	2800	Constantinople -		33 North	28	56
Cape Ortegal -		04 8	07	48 6	Smyrna	38	28 5	27	25
Cape Finister -	43	12	09	400		38	01 2	27	5300
Oporto ———		10	09	25	Antiocheta -	36	30 =	132	530
Burlings	139	35	09	24	Scanderoon -		34 de	36	30
Rock of Lisbon -		54	09	50	Tripoli -	34	38	36	15
Cape St. Vincent -		53	09	06	Alexandria -	21	10	30	19
Cadiz —	36	33	06	01	Cape Rufato-	32	48	21	25
Cape Trefalgar -		10	06	01	Cape Miserato	32	21	16	17
					Tripoly-	32	54	13	10
					Cape Bona -	37	03	11	04
On the Main Contin	ient	within	the	Straits	Bona —	37	02	108	19
					Algier ———	37	05	03	16
011 1	-6		los	117	Cape de Tres Forcas		30	02	04 V
Gibralter -		12	04	53W	Tetuan	35	27	05	06V
Cape de Gat	30	40	10	40W	Ceuta	35	54	0.4	45 V
Cape Paul	30	46	00	05	Tangier -	35	42	05	22V
Cape Martin ——			00	40	8	2)		-,	
Barcelona —		267		and the second	Iflands withi	n th	e Sina		
Marfeilles		18 9	105	27 East	The state of the s		Corra		
Toulon ———	43	075	100	42 1	Alboran	1		1	- 17
Genoa	44	25 2	100	43 Long 3509	Alboran	35	54	02	29 V
Degnorn —	43	20 2	12	3500	Formentaria ———	30	33 Z	101	55
Rome — — — Naples — —	- 40	25 Latitude 54 c	14	45 itude	Yvica ————————————————————————————————————	30	500		40
Cape Spartuventuro		2.	16	40 6	Port Mahon —	139	30 =		03
Cape Collone —		55	18	55	Gallita —	139	42 2	100	12
Cape Contone		20		05	Canala Co. III i	137	41 2	08	4400
Gallipoli -	272	56	118	43	S. end of Sardinia-	- 0	46 6	-	12

Places Names.	Lai	titude	Lon	gitude	Places Names.	La	titude	Lon	gitude
Islands within the Straits.	D.	M.	D.	М.		D.	М.	D.	М.
Gorgona —	43	34	09	38	Affinee	04	15	02	17W
Captia ———	43	03	14	54	Cape three Points -			10	50W
Lilboa ———	42	45	11	00	River Volta -			03	25
Messina		07	16	20	River Formosa -		005	07	20
Maritimo — —	38	12	17	09	Cape Formofa -		. 15	05	40
Cape Passaro	36	387	15	40日	New Callabar -		42 =	08	33 tz
Malta ————	35	53 9	14	32 =	Old Callabar		105	00	45
Malta ———— Corfu ———	39	425	20	06 H	River Camaroons -		250	10	10
Zephalonia -	- 38	15 5	21	00.9	River Angra-	00	50	10	01 9
Zant	37	15 Lat	21	1409.	Cape Lopez	00	55.0		5500
Morea —	136	52 5		32 5	River Congou -		40	15	55 gitude 56
Lemnos-	-39	590	25	37 0	Angola — '	08		115	560
Scio ———	138	22	26	12	Cape Negro -		26 2	12	31
C. St. John West- ]			1.		Cape St. Thomas-	- 24	10 di	114	43
end of Candia	35	15	24	00	Cape BonaEsperance		07 6	10	35
CapeSolomonEast ]				-0				1/	- 3 3
end of Candia	35	00	27	08	The West	ern	Iflands		
City of Rhodes -	136	42	28	05					
West end of Cyprus	5 34	57	32	23	Corvo ———	lan		lan	
East-end of Cyprus	35	31	35	00	Flores —	39	54	30	55
	1		1		Fial —	39	32 V 53 T	130	54 5
	-		51.51		Pico —		53 3	20	15 =
The Coast of B	arbo	arv and	Gu	inev.	St. George	10	40	27	0300
					Tercera —	130	52 Tautude	20	303
Cape Spartel -	las	50	los	40	St. Michael		572	25	34 2
Sallee —	35		05	49					30 6
Cape Cantin——	33		1 200		ot. Maries	-136	59	23	38
Cape de Geer —	- 32 - 30		09		m 0	,			
Cape Bajadore —			1 4 6		The Cana	ary I	mands	100	
Cape Olerado —			15		Farro	7-	-	12	2000
Cape Blanco			prop l			27		17	45
Senegal —		32		35 Long	Palma	- 28		17	36
Cape de Verde	- 15	20 2	110	2000	Gomera	- 28		17	28
River Cambia	- 14	43 08 08 08 08 08 08 08 08 08 08 08 08 08	17	20 2	Tenariff	- 28			28
River Gambia — Sierralion —		08 5	5 15	31 40	Madera West-end-	10	44	17	26 540
Cape Monferado -	VIC. 1	30	12	57	Porto Sancto-	100		15	540
Cabe ivionierado -			10	THE RESERVE OF THE PARTY OF THE	Canaria	- 27	523	15	10
	15 1000								
Cape Palmas	- 04		06		Forteventura   Lancerota	- 28 - 29	The latest of the	13	36

Places Names.	La	titude	Lor	ngitude	Places Names.	La	titude	Lon	gitud
Cape de Verde Islands.	D.	М.	D.	м.		D.	м.	D.	м.
St. Vincent -	-	04	24	39	Visegapatam ——	17	43	8.	57
St. Lucia ———		00 1		39	Cape Palmiras —	20	42		52
St. Nicholas				30 €	Rengal -	20	4-		-
		500			Bengal ————————————————————————————————————	.6	17		21
Brava	114	28 5		- H	Malacas	10	23 Z	93	00
Fuego ————————————————————————————————————	- 14	50 5	23	41 9	Malacca ———			102	10
St. Jago ———	-15				Siam Entrance	14	185		55 8
Isle of May -				02 2	Cambodia Entrance				000
Ifle Sal ————		,	1	08 m	Cochin ———	14	°5 €		56
Bonavista	-116	05	22	07	Canton —				
					Amoy or Quemoy-	24	35	116	
The South	hern	Mands	. 0.1		Nanquin ——	29	59	120	35
				5 9 (30)	Nanquin ——	32	55	120	01
St. Matthews -	-lei	30 8	106	OIW		311		467.44	ms:
Ascension —				25 W	Islands in the	Fa	A_ Indi	00.	
St. Hellena -	-16	00 8	106	14W			,	L	to the s
Fernandepo —				30 E				1	
Princes ———					Madagascar 7 S. end	,25	47	46	10
St. Thomas -			08	15 E 20 E	or St. Lau-			1	
Annabona —	- 02	10 5	1000		rence - N end	12	10	SI	05
Annaoona	-102	10 5	107	27 E	Mayetta —	13	10	45	38
				TWO IS A	Mohilla ———	12	05	44	23
The Coast on the	A		tinei	nt in	Comero	11	400		
the E	aft-In	dies.			St. Juan de Nova -	16	30 5	42	40
	. 7				Mauritius —	20	10	52	55
Cape Lagulias -	-134	54 8	5 21	20	Diego Roys -	10	50 8	61	30
	- 23	40 5	136	17	Romiras de 1	1			10.00
Mosambique-		04 5		10	Romiras de Castelamas	28	45 5	67	17
River de Fugos-	-00	14	41		Amsterdam -	38	40	72	4.5
Cape Bassos —	-	06	4 7	38	St. Brandon -	16	38	64	450
	04		47	3° E		08		68	45 30° 25 36
Cape Guardasoy -	- 11	44	51	Eaft	Quabella —	03	1343 BRE 1 - 9	1000	25
Cape Rofulgat —	- 22	41 32 45 10	159	45 Longit	Bassos de Chagos -	06		68	
Cape Muca —	- 23	32 2	159	45 9			2		45
Buffera ———	- 29	45 =	49	2009	Yas de Diego Rays	00	The state of the s	72	00
Surrat -	- 21	10	72	25 itude 50 e	Maldivia N. end	107	14.	73	04
Goa	- 15	31	73 75 75	500	[S. end	00	, , ,	76	22
Callicut -	- 11	16	75	30	Malique -	109	00	72	58
Cochin ———	-09	54 8	75	55	Sacatra ———	12	21 5	54	05
		and the last of the last		12 - 27 2 1 / 3	Abdeleur -	1	_ 0		
	-07	50	177	25	Abdeleur	12	04	153	04
Cape Camarine— Fort St. George—	- 07 - 13	50	77	32	Abdeleur -	12	04	53	04

Places Names.	Latitude	Longitude	Places Names.	Latitude	Longitude
Islands in the East- Indies.  C. Gallo, in Zeloan Yas de Amber — Andaman — Nicobar — Sumatra NW. end Verkins Island — Nassau Island — Bencola —	06 07 North Latitude 07 11 10 22 22 22 22 22 54	52 30 93 32 93 40 94 50 94 07 99 32	The Coast of America in the South Sea.  Cape St. Sebastians Cape St. Lucia— Cape Corientes— Aquapulco— Aquatulco— Guatimala— Panama— Bay Bonaventura—	D. M.  42 45 North Latitude 17 05 14 25 14 25 08 50 03 24	127 55 111 46 109 30 104 18 102 03 101 00 Well 81 52 H
Sumatra SE. end —  Engano Selam Princes Island —  Bantam in Java—  Batavia —  Java E. end Straits of Sundy —  Banca S. end Borneo S. Point—  Bandy Isles  Celebes  S. end N. end	05 22 05 50 08 20 60 06 30 11 06 16 16 08 32 10 06 02 06 03 20 03 54 04 55 05 10	105 10 101 43 102 13 104 02 105 555aft Longitude 105 46 113 37 6 106 45 113 37 6 127 17	Baldivia ———————————————————————————————————	06 30 12 15 South Latitude 29 00 Latitude 33 15 Ad 50 de 52 00 57 58	84 50 iii 77 30 6 73 10 76 22 83 18 81 10 82 36 83 10 79 55
Mindano W. point Borneo N. point Luconia SW. point NE. point E. point Formosa S. point N. point Piscadore Isles Island Chusan Japan SE. point SW. point	06 40 07 10 112 30 18 35 19 30 19 55 22 00 19 55 22 30 23 30 38 135 30	119 15	Magellan E. end — River Julian — Cape Blanco near   River Camaroons   Buenos Ayres or   River Plate —   River Grand — St. Katherines — Cape Frio — Spirito Sancto — P. Segura — Bay Modos Sanctos River St. Francisco	36 10 10 10 10 10 10 10 10 10 10 10 10 10	7 <sup>2</sup> 07 5 57 54 5 52 00 9

Places Names.	Lat	itude	Lon	gitude	Places Names.	La	titude	Lon	gitude
The Coast of Brazil, &c.	D.	М.	D.	м.	18 11 12 13	D.	М.	Ď.	М.
Cape St. Augustine	08	35 S	35	zoW	St. Bartholomew —		52	62	c6
Cape Roque	05	00 S	35.	47 W	St. Martins ——	18	06	52	10
Triffian de Cunha-		05 S	13.	24 W	Anguilla ———		17	52	13
Trinidada — —	20	30 S	30	oo W	Virgins	18	30 Z		25 8
					St. Cruz ———		527		30 €
Main Continent i	n th	e West-	-Ind	ies.	Bieque		-	33	15 5
					Porto Rico St Johns		30 au	65	157 gitude
R. Amazons Ent	00	co	19	56	St. Domingo Hisp Port Royal Jamaica	10	25 Hitude	59	30 =
North Cape	02	05	19	56	East end of Cuba -		40 6		32 0
Surinam	36	25	56	50	Havanna —		15	73	55
Oronoque-	08	157	59	25 8	Bay of Hondy		40	82	55
Cape Conquibaca -	12	400	170	42 C	Cape St. Anthony—		45	100	40
Carthagena -	10	285	75	21	Cape ot. Mithony	121	45	185	32
Scots Settlement -		30	78	45 21					
Nicaragua Entrance		30 Latitud	84	15 gitude	Baham	710	ands		
Cape Catoche -	- 2 I	10 8	86	10 2					
Campeachy —	19	300	92						
La Vera Cruz		12	97	48	Bermudas -	132	25	163	40
	30	20	89	30	N. point of Baha- 1	1		and a	
Cape Florida —	- 24	57	(80	30	ma Bank —	28	00	78	35
					Bahama Island —		50	79	36
The Carib	bee	Islands	5.		Abacco S. point -	126	00	73	46
					Harbour Island-	25	37	76	47
Trinidado	-10	15	160	17	Andros N. point -	- 25	10		50
Tobago W. end -	-11	10	159	10	Providence	25	00 6		20
Granado	- 11	57	60		Illathera S. point -	-24	40 5	75	56
Barbadoes -	- 12	58	58		Cat Illand	- 24	25 t	- 75	3500
St. Vincent		122	160	12 €	Watling Island-	- 24	25 Land	74	350
St. Lucia -		55 5	60		Rum Key —	23	45 5	174	50
Martinico -	-14			545	Exuma —	- 23	22 0	175	50 5
Dominico —	-115	23	60	30 5	Crooked Island	122	-6		
Marigallante ———	-115	58 2	60	20 1	N. point —	22	56	74	12
Guardalupe -	-16	23 58 10	61	Longitude	Atkins Key —	- 22		74	.05
Monferat	-16	45	62	15	I Wiciapai vouz	- 21	58	74	45
Antigua	-17	05	61	45	Atwoods Key —	- 23	10	173	35
	1	05	52	32	French Keys-	- 22	40	73	40
Nevis -	-17	0						1/3	4-
		13	52		Mayaguana ———————————————————————————————————	- 22		72	46

Places Names.	Lat	itude	Lon	gitude	Places Names.	La	titude	Lon	gitud
Bahama Islands.	D.	М.	D.	м.	The Coast of Hud- Jon's Bay and Straits	D.	м.	D.	M.
Heneago —	20	52 N	73	46W	Buttons Isle	60	25	66	27
Caicos Bank N. ]		100	33.		Cape Charles -		10	75	35
Point -	21	50 N	71	15 W		52	35	77	55
Turks Island -	21	35 N	70	o8W	Mansfield Isle -	51	42	80	30
Abrolho N. point-	21	35 N		o6W	Cape Jones		55	78	58
Plate Wreck		ION		15W	Ruperts River -	SI	30 2	70	26 :
	•		- / - 10		Albany River -		26 2	84	50
The Coast of Caro	lina	Virgi	nio	Mary-	The Cubbs -	154	105	82	40
The Coak of Caro	u,	1.18	,,,,,	1.14.	C. Henrietta Maria	55	07 4	10	20
land, Pensilvania	. N	ew En	glan	d, and	Port Nelson -	57			580
					Cape Churchill-				20
Newfoundland.					Cape Southampton	61		86	48
					Shark Point	64		82	
Charles Town up-	1		1		Nottingham Isle -				55
	32	45	78	46	Q. Ann's Foreland	1 -		79	53
on Afhly River	1		1	20	Resolution Isle			74	55
Cape Hatteras —		15	74	20				65	04
Cape Henry		00	75	24	Cape Farewell —	-159	45	146	45
Cape Charles -	-37	16	74	16		***		7334	4116
Cape Hinlopen-	-38	50	74	56	The Coast of Icela	ind	Greenl	and.	Non
Long Island -	40	50	72	45	The Count of Ith	,,,,	G/ ttm	,,,,	1100
New York		58	73	53	Zembla, and	No	rthern	Tiles	
Cape Cod	-42	12	68	55	Ziemota, alla	140	tuein	11103	
Boston ———	-42	30	169					14	100
Cape Sable —		502	64	58 ₹	Sound Royal -	- 66	22	14	33
Isle Sable ———	-44	207	159		Bargazar Point-	- 65	.20	16	35
								20	33
		00 -		30 0	Whales Back -	- 65	27		33
Cape Britain-	-46			30 L 48 h	Whales Back — Merchants Forelan			7. 7.00	
Cape Britain———————————————————————————————————	46			30 Longi	Whales Back — Merchants Forelan Halliford —	d 63	25	17	05
Cape Britain———————————————————————————————————	46 46 52			Jongitud 57	Whales Back Merchants Forelan Halliford Fair Foteland	d 63	25	17	05
Cape Britain  Quebec  Bay of Breft  Bell Ifland	-46 -46 -52 -52	55 10 07 07 07 07 07 07 07 07 07 07 07 07 07	69	Longitude 57 358	Whales Back Merchants Forelan Halliford Fair Foreland Grims Island	d 63 - 64 - 66	25	17	05
Cape Britain  Quebec  Bay of Breft  Bell Ifland  Cape St. John	-46 -52 -52 -50	55 10 07 e	56	48 57 35 48	Merchants Forelan Halliford Fair Foreland Grims Island	d 63 - 64 - 66	25 30 20 15	17 34 26 22 22	05 43 27 34
Cape Britain  Quebec  Bay of Breft  Bell Ifland  Cape St. John  Cape Bonavifta	-46 -52 -52 -50 -49	55 10 07 07 15 ·	56	48 57 35 48 48 12	Merchants Forelan Halliford Fair Foteland Grims Island Westmania Isles	d 63 - 64 - 66 - 67 - 63	25 30 20 15	17 34 26 22 22	05 43 27 34
Cape Britain  Quebec  Bay of Breft  Bell Ifland  Cape St. John  Cape Bonavifta  Trinity Bay Ent.	- 46 - 46 - 52 - 52 - 50 - 49 - 48	55 10 07 07 15 · 42	55 52 52	48 57 35 de 12 20	Merchants Forelan Halliford Fair Foteland Grims Island Westmania Isles Isles of Fero	d 63 - 64 - 66 - 67 - 63 - 62	25 30 20 15 30	17 34 26 22 22 22	05 43 27 34
Cape Britain  Quebec  Bay of Brest  Bell Island  Cape St. John  Cape Bonavista  Trinity Bay Ent  Conception Bay	- 46 - 46 - 52 - 52 - 50 - 49 - 48	55 10 07 07 15 · 42 20	69 56 55 52 52 52	48 00 mg/r udc 57 35548 12 20 08	Merchants Forelan Halliford Fair Foreland Grims Island Westmania Isles Isles of Fero Beerenberg, or	d 63 - 64 - 66 - 67 - 63 - 62	25 30 20 15 30	17 34 26 22 22 22	05 43 27 34 24 00
Cape Britain  Quebec  Bay of Breft  Bell Ifland  Cape St. John  Cape Bonavifta  Trinity Bay Ent.  Conception Bay  St. John's Harbour	46 46 52 52 50 48 48	55 10 67 67 15 15 42 20 00	69 56 55 52 52 52 52 51	48 57 3548 12 20 08 39	Merchants Forelan Halliford Fair Foreland Grims Island Westmania Isles Isles of Fero Beerenberg, or John Main's Isle	d 63 - 64 - 66 - 67 - 63 - 62	25 30 20 15 30 45	17 34 26 22 22 05	05 43 27 34 24 00
Cape Britain  Quebec  Bay of Breft  Bell Island  Cape St. John  Cape Bonavista  Trinity Bay Ent.  Conception Bay  St. John's Harbour  Bay of Bulls	46 46 52 52 50 48 48 48	55 10 07 07 15 15 . 42 20 00 50	56 55 52 52 52 51	48 57 3548 12 20 08 39 29	Merchants Forelan Halliford Fair Foteland Grims Island Westmania Isles Isles of Fero Beerenberg, or John Main's Isle Point Look-out	d 63 - 64 - 66 - 67 - 63 - 62	25 30 20 15 30 45	17 34 26 22 22 05 04 15	05 43 27 34 24 00 30
Cape Britain Quebec  Bay of Brest Bell Island Cape St. John Cape Bonavista Trinity Bay Ent. Conception Bay St. John's Harbour Bay of Bulls Cape Race	46 46 52 52 50 48 48 48 47	55 10 07 07 15 15 . 42 20 00 50 40	56 55 52 52 52 51 51	48 57 35 48 1 2 2 0 8 3 9 2 9 5 2	Merchants Forelan Halliford Fair Foreland Grims Island Westmania Isles Isles of Fero Beerenberg, or John Main's Isle Point Look-out Horn Sound	d 63 - 64 - 66 - 67 - 63 - 62 - 76 - 76	25 30 20 15 30 6 45	17 34 26 22 22 22 05 04 15	05 43 27 34 24 00 30 36 36
Cape Britain  Quebec  Bay of Brest  Bell Island  Cape St. John  Cape Bonavista  Trinity Bay Ent  Conception Bay  St. John's Harbour  Bay of Bulls  Cape Race  Cape St. Mary	46 - 46 - 52 - 50 - 49 - 48 - 48 - 48 - 46 - 47	55 10 07 07 15 15 · 42 20 00 50 40 10	56 55 52 52 52 51	48 57 35 48 12 20 8 39 29 5 2 23	Merchants Forelan Halliford Fair Foreland Grims Island Westmania Isles Isles of Fero Beerenberg, or John Main's Isle Point Look-out Horn Sound Fair Foreland	d 63 - 64 - 66 - 67 - 63 - 62 - 76 - 76	25 30 15 30 45 25 45 20	17 34 26 22 22 22 05 04 15 13	05 43 27 34 24 00 30 36 36 52
Cape Britain Quebec  Bay of Breft Bell Ifland Cape St. John Cape Bonavifta  Trinity Bay Ent. Conception Bay St. John's Harbour Bay of Bulls Cape Race	46 - 46 - 52 - 50 - 49 - 48 - 48 - 46 - 47 - 47	55 10 07 15 15 15 42 20 00 50 40 10 45	56 55 52 52 52 51 51	48 57 358 48 12 20 08 39 25 23 23 23 23 23 23 23 23 23 23 23 23 23	Merchants Forelan Halliford Fair Foreland Grims Island Westmania Isles Isles of Fero Beerenberg, or John Main's Isle Point Look-out Horn Sound	d 63 - 64 - 66 - 67 - 63 - 62 - 76 - 76 - 76 - 79	25 30 15 30 45 45 20 55	17 34 26 22 22 22 05 04 15	05 43 27 34 24 00 30 36 36 52

1			gitude	Places Names.	La	titude	Lor	gitude
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	78 77 76 74 75 70 69 65 64 66 68 69 71 70 68 63 62 60 57 80 80 80 80 80 80 80 80 80 80 80 80 80	77 18 76 18 76 18 74 30 75 05 70 00 69 05 64 30 11 68 10 68 10 69 30 71 23 67 05 70 25 68 15 63 55 62 10 60 10 57 45  Sound and	78 05 23 77 18 21 76 18 23 74 30 18 75 05 54 70 00 61 69 05 43 66 31 Latitude 66 31 Latitude 71 23 6 68 10 34 69 30 11 71 23 6 68 15 09 63 55 10 64 10 05 67 45  Sound and Ball 58 19 N 08 58 54 N 09 59 20 N 10	78 05 23 25 77 18 21 30 76 18 23 45 74 30 18 08 75 05 54 50 70 00 61 20 69 05 North Lattitude 66 31 Lattitude 71 23 de 71 05 15 30 68 15 09 30 63 55 10 15 62 10 04 38 60 10 57 45  Sound and Baltick.    58 19 N   08 57 E 58 54 N   59 20 E 59 20 N   10 00 E	78 05 23 25 77 18 21 30 76 18 23 45 74 30 18 08 75 05 54 50 70 00 61 20 69 05 42 35 65 43 07 40 30 FF 64 30 77 40 30 FF 66 31 1 36 33 5 68 10 1 34 45 07 68 10 1 34 45 07 69 30 FF 71 05 16 40 70 25 15 30 68 15 09 30 69 30 50 69 30 50 69 30 50 69 30 50 69 30 60 69 3	78 05 23 25 77 18 21 30 76 18 23 45 74 30 18 08 75 05 54 50 70 00 61 20 69 05 42 35 65 43 07 40 30	78 05 23 25 77 18 21 30 76 18 23 45 74 30 18 08 75 05 54 50 70 00 61 20 69 05 42 35 65 43 07 40 30 10 66 31 1 36 33 10 68 10 134 45 50 69 30 11 31 20 11 71 23 6 23 02 6 71 05 16 40 70 25 15 30 68 15 09 30 69 30 11 20 12 60 10 55 40 60 10 55 40 60 10 55 40 60 10 05 40 60	78 05 23 25 77 18 21 30 76 18 23 45 76 18 23 45 74 30 18 08 75 05 54 50 70 00 61 20 42 35 65 43 07 40 30 ft 64 30 ft 64 30 ft 66 31 1 36 33 10 68 10 10 34 45 07 1 23 de 23 02 de 71 05 16 40 70 25 15 30 68 15 09

The Latitudes of any two Places being given, to find the Diffrence of Latitude between them.

Rule, If the Latitudes are both North, or both South, subtract the Lesser from the Greater, the Remainder will be the Difference of Latitude.

But

But if one Latitude be North, and the other South, then add them together, and their Sum will be the Difference of Latitude.

Example ift. What is the Difference of Latitude between the

Lizard, and Barbadoes.

Lizard, in Latitude — 49° 57' N.

Barbadoes, in Lattiude — 12 58 N.

The Difference of Latitude - 36 59

Example 2d. What is the Difference of Latitude between Jamaica and Cape Bona Esperance.

Jamaica, in Latitude 17 40 N. Cape Bona Esperance, in Latitude 34 07 S.

The Difference of Latitude — 51 47whichDegrees being multiplied by 60, and the odd 47 Min. 60 taken in, will give the Difference of Lat. in — 3107 Miles.

### Rules for Latitude.

The Latitude fail'd from, and the Difference of Latitude being

given, to find what Latitude the Ship is come into?

Case the 1st. When you sail from North Latitude to the Northward, or from South Latitude to the Southward, add the Difference of Latitude (it being first brought into Degrees, if need be, by dividing it by 60) to the Latitude sail'd from, the Sum will be the Latitude you are come into, of the same Name with the Latitude sail'd from.

Example 1st. A Ship from a Place in the Latitude 14 10 N. sails to the Northward till she makes her Difference of Latitude 04 21 a What Latitude is she come into?

Latitude fail'd from \_\_\_\_\_\_\_ 14 10 N.

Difference of Latitude \_\_\_\_\_\_ 04 21

Latitude come into \_\_\_\_\_\_ 18 31 N.

Example 2d. A Ship from Latitude 29 17 S. sails to the Southward, till she makes her Difference of Latitude 374 Miles: What Latitude is she come into?

Latitude fail'd from

Diff. of Lat. 374 Miles, divided by 60 makes

Latitude come into

35 31 S.

Case the 2d. When you sail from North Latitude to the Southward, or from South Latitude to the Northward, Subtract the Difference of Latitude, if least, from the Latitude sail'd from, the Remainder is the Latitude come into, of the same Name with the Latitude you fail'd from.

But if the Difference of Latitude be biggest, then subtract the Latitude from the Difference of Latitude, the Remainder will be the Latitude come into, of a contrary Name to the Latitude you

failed from.

Example 1st. A Ship from Latitude 49 14 N. fails to the Southward, till her Difference of Latitude be 521 Miles: What Latitude is the come into?

> Latitude fail'd from 49 14 N. Diff. of Lat. 521 Miles, divided by 60, makes 08 41

> Latitude come into 40 33 N.

Example 2d. A Ship from Latitude 4 18 S. fails to the Northward, till her Difference of Latitude be 10 24: What Latitude is The come into?

> Latitude fail'd from --Difference of Latitude -Latitude come into

## Rules for Longitude.

The Longitudes of any two Places being given, to find the Difference of Longitude between them..

Rule. If the Longitudes are both East, or both West, subtract the leffer from the greater, the Remainder will be the Difference of

Longitude.

But if one Longitude be East, and the other West, then add them together, and their Sum (if less than 180 Degrees) will be the Difference or Longitude; but if it be more than 180 Degrees, then fubtract it from 360.00, and the Remainder will be the Difference of Longitude.

Example ift. What is the Difference of Longitude between Cape Cafe

Finister and Antigua?

Cape Finister, in Longitude \_\_\_\_\_ 09 40 W.

Antigua, in Longitude \_\_\_\_\_ 61 45 W.

The Difference of Longitude \_\_\_\_\_ 52 05

Example 2d. What is the Difference of Longitude between Barcelona and the Rock of Liston?

Barcelona, in Longitude 02 18 E.
Rock of Liston, in Longitude 09 50 W.
The Difference of Longitude 12 08

Example 3d. What is the Difference of Longitude between the S.E. Point of Japan, and the Island of St. Christophers.

Exceeds 180 00 203 10
Subtract it from 360 00

Remains the Difference of Longitude ------ 156 50

The Longitude fail'd from, and the Difference of Longitude be-

ing given, to find what Longitude the Ship is come into?

Case 1st. When you sail from East Longitude to the Eastward, or from West Longitude to the Westward, add the Difference of Longitude to the Longitude sail'd from, the Sum (if less than 180 Degrees) is the Longitude come into, of the same Name with the Longitude you sail'd from.

But if the Sum should be more than 180 Degrees, then subtract it from 360.00, and the Remainder will be the Longitude you are come into, of a contrary Name to the Longitude you fail'd from.

Example 1st. A Ship from Longitude of 48 on E. Tails to the Eastward, till she makes her Difference of Longitude 287 Miles. What Longitude is she come into?

Example 2d. A Ship from the Longitude of 178-47 West, sails to the Westward till her Difference of Longitude be 12 17: What Longitude is she come into?

P 2

Longi-

## Rules for Longitude.

Longitude fail'd from	- 178	47 W.
Difference of Longitude	- 12	17
Exceeds 180.00	- 191	04
Subtract it from-	- 360	00
Remains the Longitude come into -	- 168	56 E.

Case the 2d. When you sail from East Longitude to the Westward, or from West Longitude to the Eastward, subtract the Difference of Longitude (if it be least) from the Longitude you sail'd from, and the Remainder will be the Longitude come into, of the same Name with the Longitude sail'd from.

But if the Difference of Longitude be the biggest, then subtract the Longitude from the Difference of Longitude, and the Remainder will be the Longitude come into, of a contrary Name to the Longitude sail'd from.

Example 1st. A Ship from Longitude 98 17 East, sails to the Westward till she makes her Difference of Longitude 14 21: What Longitude is she come into?

Longitude fail'd from -	98	17 E.
Difference of Longitude	14	21
Longitude come into-	83	56 E.

Example 2d. A Ship from Longitude 44 21 West, sails to the East-ward till her Difference of Longitude be 81 42: What Longitude is she come into?

Longitude fail'd from	-	21 W.
Difference of Longitude ———	81	42
Longitude come into	37	21 E.

Here follows a Table of Meridional Parts, to every Degree and Minute of Latitude

M	od	1	d) a	z dj	3 d	4 d	5 d	6d 7	di	8,4	9 4	10 d	11	1 12		301	M
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1	4			24	184	244	304			486	546	607	66	200	129	791	4
5	. 5	1	65 1	125	185	245	305			487	547	608	66		130	792	5
6	6		66	126	186	246	306	367	427	488	548	600			734	793	6
7	7	1	67	127	187	247	307	368		489	549	6H		7 1000	732	794	7
8	8			128	188	248	308			49C	5.5C	611			733	795	8
9	9		69	129	189	249	309		43cl	491	551	612	-		735	796	9
10	10		70	130	190	250	310	371	431	492	552	613			736	797	10
11	11			131	191	251	311		432	493	553	614	67		737	798	11
12	12	100		132	192	252	312	373	433	454	554	61			738	799	12
13	13		73	133	193	253	313	374	434	495	555	616			739	800	13
14	14		74	134	194	254	314	375	435	496	556				740	801	15
15	15		75	135	195	255	315	376	436	497	557				741	803	15
16	10	5	76	136	196	250	,16	377	437	498	558			80	742	804	17
17	1,	7	77	137	197	257	317	378	438	499	559		-	82	743	805	18
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25		5	85	145	205	265	325	387	446	507 508				91	752	813	.6
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27			87	147	207	267	327	389	448	510	4 3 7 12			93	754	816	28
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3	852	911	9,6	38	01	65	28	92	57	22	87	53	20	87	3
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5	854	916	978	41	' 03	67	30	95	59	24	90	56	22	89	8
6	855	917	979	42	05	68	32	96	60	25	91	57	- 23	90	6
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15	855	927	18,	52	15	78	42	05			02	68	34	01	16
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144	894	956	19	81	4,	51 0	72	30	0		32	1600	60	33	13
145	895	957	20	82	4	0	73	3	0		33	1600	6	34	4
1+6	89	558	2		4	10	74	35			3.	0	68	35	14
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2	53	22	91	60	31	02	74	47	20	95	7,1	48	25		1 :
3	55	23	92	62	32	03	75	48	22	96	7,2	49	27	06	
4	56	24	93	63	33	04	76	49	23	98		50			
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56	5.8	26	95		35	07	79	52	25	2400	75	53	31	10	1 8
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13	66	34	03	73	44	15	87	60	34	09	85	6:	40	19	113
44	68	3.5	05	74	45	16	88	61	35	10	86	-63	41	20	14
15	68	37	06	76	45	17	90	63	37	11	87	64	42	22	115
	69	38	07	77	47	19	91	64	38	13	89	66	44	23	16
7	70	39	c8	78	48	20	92	65	39	14	90	67	45	24	17
18	72	40	09	79	50	21	93	66	40	15	91	68	46	26	11
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5	80	48	17		58	29	02	75	49	74	2500	77	55	35	25
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	86	25	24	94	65	37	09	82	56	32	08	85	63	2742	
2	87	55	25	95	66	38	10	83	58		co	86	65	43	3
3	89	57	27	97	67	39	11	85	59	33	10	88	66	44	32
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3	113	80	50	20	91	63	26	09	84	50	36	14	92	72	52
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2	84	66	49	33	18	06	95	85	78	72	-68	67	68	71
3	86	67	50	34	20	07	.96	87	79	74	70	69	70	73
4	87	69	51	36	21	09	98	88	81	75	72	70	71	75
5	88		53	37	23	10	99	50	82	77	73	72	73	7
6	90		54	38	21	12	3301	91	8+	78	75	74	75	78
7	91	73	56	40	26	100	01	93	85	80	77	75	77	80
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12	98	80	63	47	33	20	: 09	1400	93	88	85	84	85	8
13	99	81	64	48	34	22	11	02	95	90	86	85	87	9
14.	2801	82	65	50	36		12	03	96	91	88	87	89	9
15	02	84	67	51	37		14	05	98	93	90	85	90	94
16	03	85	68	53	39		16	07	99	94	91	90	92	90
17	05	. 86	7	54	40	28	17	c8	3501	96	93	92	94	9
18	06	88	71	55	42	29	19	10	03	98		94	95	9
19	07	- 89	72	_57	43	31	20	_11	_04	99	96	95	97	400
20	2809	2891	2574	3058	3144	3232	3322	3413	3506	3601	3698	3797	99	400
21	10	92	75	60	46	34	23	14	07	02	99	99	3901	0
22	11	93	76	61	47		25	16	09	04		380c	02	0
23	13	95	78	63	49		26	17	10	06		02	04	0
24	14	96	79	64			28	19	12	07		0,	06	10
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41 42 43	37	19	03	88	75 76 78	63	53	45	39	34	32	32	35	4
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44	41	24	07	93	79	68	50	50	43	35	37	38	40	4
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54	5.5	37	21	07	94	83	. 73	65	59	55	54	55	58	6
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2	77	86	98	13			7.	09	44	84	28	79	36	5800	
3	79	88	4300	15	1		81	12	46	86	31	82	39	03	
4	81	90	01		35	57	84	14	49	83	33	84	41	06	1
5	83	92	04		37	60	86		51	10	36	8;	44	09	
6	85	94	06	1000	39	62	88		53	93	38	89	47	11	
7	80	95	08		41	64	90	20	55	95	41	92	50	14	
8	88	97	CO	25	43	66	91	23	58	98	43	95	52	17	
9	90	9	11	27	45	68	94	25	60	5200	46	97	55	20	1
0	4092	1201	4313	4429	4547	+670	4790	4927	5062	52.03			5658		1
1	94	03	15	31	49	72	95	29	65	35	5348	02	60	1823	10
2	95	05	17	33	51	74	4801	31	67	07	51	05	63	25	1
3	97	07	19	34	53	76	03	3+	69	10	56	07	66	11 12 12	13
4	99	08	20	36	55	78	05	36	71	12	58	10	68	31	1
5	4101	10	23	3.8	57	80	07		74	14	61	13	71	34	1
6	03	12	25	40	59	82	09		76	17	63	15	74	37	1
7	04	14	27	42	6:	84	Ti	43	78	15	66	18	76	39	10
8	06	16	28	44	64	87	14	45	81	22	68	20	79	42	1
9	c8	18	30	46	66	_89	16		83	24	71	23	82	45	
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2	13	23	36	52	72	95	22	54	100000	29	76	28	90	54	2
3	15	25	38	54	74	97	1.16	56	90	31		31		56	2:
4	17	27	40	56	70	99	24		92	34	80	33	93	59	2
5	19	29	42	58	79	4701	1.30	60	95	36	83	36	95	62	24
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7	22	32	46	62	82	05	33	65	5102	41	88	41	4 4 3 30	68	20
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1	30	40	53	70	90	14	42	74	11	53	5401	54	15	82	3
2	32	42	55	74	92	18	44	76	13	55	03	57	17	85	32
3	33	44	59	76	94	20	46	78	15	58	06	59	20	88	3
4	35 37	47	61	78	98	22	48	18	18	60	08	62	23	91	34
5	39	49	63	80	4600	24	50	83	20	63	11-	65	25	94	3!
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5	55	66	80	97	18	43	72	C.5	43	87	36	91	53	22	4.
2	57	68	82	99	20	45	74	08	46	89	38	94	56	25	46
5 7 8	59	70	84	4501	23	47	76	10	48	92	41	96	58	25	47
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1	72	83	58	15	37	62	92	25	65	99	59	15	75	46	5
5	73	85	99	17	39	64	94	28	67	11	61	17		48	54
6	75	87	1401	19	41	66	96	30	69	14	64	20	81	51	5.5
7	77	85	03	21	43	69	98	33	72	16	66	23	83	54	50
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1	69	49	38	38	49	7+	14	72	49	51	81	45	53	14	. 1
2	72	52	41	41	53	78	18	76	54	55	87	52	60	22	2
1	75	55	.45	45	57	82	22	81	59	61	93	58	61	31	3
4	78	58	48	49	60	86	27	85	64	67	98	65	74	39	4
5	181	61	51	52	64	90	31	90	69	72	3404	71	82	47	5
. 0	84	64	54	55	68	94	3.5	54	74 78	83	16	78	89	55	6
7	85	67	58	5	71 75	97	- 35	7503	83	83	22	84	96	72	7 8
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113	5001	83	74	76	93	21	64	25	08	15	51	23	40	14	13
14	07	85	85	79 83	97	25	68	30	13	20	57	30	48	23	14
115	10	92	84	85	5801	29	73	35	17	25	63	36	55	31	15
1	13	95	87	90	04	33	77	39	22	31	69	43	62	40	16
117	16	98	90	93	08	37	81	44	27	36	74	49	70	48	17
118	19	6231	94	9	12	41	85	48	32	41	80	56	77	57	18
15	22	05	57	6600	15	45	8,	53	37	47	86	63	85	65	15
20	5015	6298	5400	6.03	.819	7048	7294	7557	7842	8152	8492	8869	9291	9774	20
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24	37	20	13	17	3+	64	11	76	62	74	16	96	22	09	24
25	100000	23	17	21	38	68	15	80	67	79	22	8903	30	17	25
26		26	20	24	41	72	15	85	72	85	28	09	37	26	26
27		30	23	28	45	76	23	8)	77	90	34	16	45	35	27
28	49	33	27	31	49	80	28	94	82	96	40	23	53	44	28
129		36	30	35	53	84	32	99	87	8201	46	30	60	52	25
30	1055	6239	5433	6639	6856	7088	7336	7603	7892	8207	8552	8936	9368	9861	30
131	58	42	37	42	60	92	4	08	57	12	58	43	76	70	31
3:	61	45	40	46	64	.96	45	12	7902	18	65	50	83	79	32
133	64	49	43	49	68	7100	49	17.	07	23	71	57	91	88	33
34	67	52	47	53	71	04	53	22	12	29	77	63	99	97	34
13.5	70	55	50	56	75	08	51	26	17	34	83	70	9407	9906	35
13:	73	58	53	60	73	12	62	31	22	40	89	77	14	15	36
137	76	61	57	63	83	16	60	36	27	45	95	84	22	24	37
138	79	64	60	67	86	20	71 75	40	32	51	36c1	98	30	33	38
13	82	68	63	70	90	24		45	37	51 56 8262	07		38	42	39
10	5085	6271	467	6674	90 6894	7128	7379	7650 54	7942 48	8262	3614	9005	9445	9951	40
+1	88	74	70	77	98	32	84	54	48	67	20	12	53	1 60	41
4	91	77	73	81	6901	36	188	59	53	73	26	18	61	69	42
+3	94	80	77	85	05	40	92	64	58	79	32	25	69	78	43
4.	. 97	83	80	88	09	45	97	68	63	84	38	32	77	87	44
1+5	5100	87	83	92	13	49	7401	73 78	68	90	44	39	85	9995	45
46	03	90	87	95	17	53	06		73 78	95	51	46	93	10005	46
14	06	93	90	99	20	57	IC		78	8301	57	53	950!	10015	47
+8	09	96	94	6702	24	61	14		83	07	63	60		10024	48
49	12	99	97	06	28		19	92	89	12	69	67		10033	49
150	6115	6303	5500	6710	6932	7169	7423	7697 7702	7994	8318	3676	9074	9525	10043	50
51	18		04	13	30	73	27	7702	99	24	82	81	1 .33	10052	51
52	21	0)	07	17	40	77	32	06	8004		88	88	41	10001	52
55	2	12	11	20	43	81	36		09		95	96			53
5-	27	. 15	14	24	47	85	41		14		8701	9103		10080	54
155	30	19	17	28	5	89	45	21	20		07	10		10089	
156	33	22	21	31	5.5	94	49		25	52	14	17		10099	5
57	36	25	24	35	52	98	54	30			20		81	80101	5
155	40	28	28	58	63	7202	58		35	64	26		89	10118	5
59	43	72	31	1 42	66	1 00	63	40	40	1 09	33	1 40	20	110127	55

.

INI	84 d	85 d	86 d	87 d	88 d	89 d	M
0	10137	10765	11533	12522	13916	6300	0
1	147	775	547	541	945	357	1
8	157	788	561	561	974	416	2
3	166	799	5.6	580	14003	476	3
4	175	811	550	599	033	537	4
5	185	822	605	61)	c63	595	5
5	195	834	620	639	093	662	0
	205	846	634	659	123	726	7
7 8	214	858	649	679	154	7.2	3
. 9	22	869	664	6,9	184	858	9
10	10234	10881	11679.	12719	14216	10926	10
11	241	893	694	739	247	9:6	11
.12	254	505	700	759	279	1;06:	12
13	261	917	724	780	311	135	13
14	273	919	739	801	343	213	14
15	283	941	755 770	8+2	408	366	15
16	293	965	785	863	442	445	17
17	303	978	801	884	475	526	18
18	324	990	816	506	500	605	1
19	-	11002	11832	12927	14543	17653	20
20	10334	014	848	949	578	781	21
21	344 354	027	863	970	613	870	27
22	364	039	879	992	648	562	23
23	374	052	895	13014	684	18056	24
25	385	064	911	036	720	153	25
26	395	077	927	059	756	252	26
27	405	089	943	081	793	355	27
28	416	102	959	104	830	461	28
29	426	115	976	126	868	57C	29
30	10437	11127	11992	13149	14906	1868:	50
31	447	140	12008	172	943	795	31
32	457	153	C25	195	983	920	
33	468	166	041	219	15022	1504:	33
34	478	179	058	242	062	174	34
35	489	192	075	266	102	305	35
36	500	205	092	290	143	450	
37	510	218	109	314	226	596 749	37
38	521	231		338 362	268	509	39
19	532		143		15311		_
+0	10512	11257	12160	13386	354	253	
41	553	270	177	411	358	439	41
42	564	297	194	461	442	635	
43	586	310	229	486	487	843	44
45	597	324	247	511	532	21065	45
46	608	337	264	537	579	303	
1473	619	351	282	1 663	625	557	47
481	630	365	300	589	673	832	48
49	641	378	318	615	721	22132	49
50	10652	11392	12336	13641	15770	22459	
51	663	406	354	668	819	22821	51
52	674	420	373	695	869	23226	52
53	685	434	391	721	920	2368	53
54	696	448	409	749	972	242)5	54
55	708	462	428	776	16024	24842	
56	719	476	447	804	078	25600	
57	730	490	465	832	132	27992	
58	742 758	504	484	888	243	30175	
28	1 / 10	510	303	. 500	,		1.07

The Use of the Table of Meridional Parts.

IN this Table the first and last Column of every Page mark'd M, beginning at o, and ending at 59, contain the Minutes answering to every Degree of Latitude, the other Columns mark'd id, 2d, &c. contain the Meridional Parts. answering to the Degree of Latitude they fland under.

So that if you would find the Meridional Parts answering to any Latitude, suppose for Example, the Latitude 51.32, look in the Column under 51d. and right against 32 (in the Column for Minutes) you will find 20, to which prefix 36, the two Figures in the fame Column that stands above 20 towards the Left-hand, and it: makes 3620, the Meridional

Parts required.

Two Latitudes being given, to find the Meridional Difference of Latitude.

Case 1st, If both Latitudes be North or both South, subtract the Meridional Parts of the Leffer, from the Meridional Parts of the Greater, the Remainder will be the Meridional Difference of Latitude.

Case 2d, If one Latitude be North and the other South, then add their Meridional Parts together, and the Sum will be the Meridional Difference of Latitude. Q 2

A TABLE of Amplitudes, from the Latitude oo deg. oo min. to the Latitude 12 deg. either North or South.

					1											10.2									
Declination.	Degrees	_		2		3		4		5	-	-	5	7	-	8		9			0	·	•		2
n.	•	D	M	D	M	D	M	D	M	D	M	Ď	M	D	M	D	M	D	M	D	M	D	M	D	M
	c	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00
	1	22	00	01	00	01	00	01	00	01	00	02	00	32	00	02	00	01	00	01	01	01	01	01	01
	3	23	00	03	00	03	00	03	00	03	00	03	01	23	01	03	01	03	02	03	03	03	03	03	04
	4	34	00	94	00	04	00	04	00	04	01	04	01	04	02	04	02	04	03	04	04	04	04	04	05
1	5	05	0	05 05	00	05	00	05	00	05	01	05	01	05	02	05	0	05	03	05 06	05	05	05	o6	07
	7	27	00	07	00	07	01	07	01	07	02	07	02	07	.03	07	04	07	05	07	07	07	07	07	00
	5	29	00	09	00	08	01	08	01	08	02	09	03	08	04	09	05	08	07	09	09	09	10	08	11
-	10	10	oc	10	00	10	01	10	01	10	02	10	03	10	04	10	05	10	07	10	10	10	11	10	13
	11	11	00	11	00	11	01	11	01	11	03	11	03	11	05	11	c6	11	08	11	11	iI	12	11	15
	12	12	00	12	00	12	01	12	01	12	03	12	04	12	05	12	08	12	05	12	12	12	13	12	16
																								14	
	15	15	00	15	00	15	01	15	02	15	04	15	05	15	07	15	09	15	11	15	15	15	17	15	21
	10	17	00	17	01	17	01	17	02	17	04	17	05	17	08	17	10	17	12	17	17	10	18	16	22
	18	18	00	18	01	18	01	18	02	18	04	18	06	18	08	18	11	18	14	18	18	18	21	18	25
	19	19	00	19	01	19	01	19	03	19	04	19	06	19	09	19	11	19	15	19	19	19	22	19	26
4 1	A A A					100													. X Y					20	28
199									1 1 1				10000	100				21		THE RESERVE AS A SECOND		1 1 1 1 7			29
						0.00							-			1 1 1 - 1	0 0 0 0	22				23		1000	31
23,																					-	23	57	24	02

A TABLE of Amplitudes, from the Latitude 13 deg. oo min. to the Latitude 24 deg. either North or South.

	-							1	he	D	eg	ree	S	ot	L	atit	ud	e.	<u> </u>						-
0		•	3		4		5		16		7		8		19		20	•	1		22	,	13	2	24
ation.		D	M	D	М	Ď	M	D	М	D	м	D.	М	D	M	D	M	D	М	D	M	D	M	D	М
	2	02	03	01 02 03	03	01 02 03	04 06	01 02 03	00 02 05 07 10	01 02 03	05	01 02 03	06	01 02 03	03 07 10	01 02 03	08	01 02 03	08	01 02 03	04	01 02 03	10	01 02 03	11
	6 7 8	06 07 08	10 11 12	06 07 08	11	06 07 08	13	06 07 08	12 15 17 19 22	06 07 08	16	06 07 08	19 22 25	06 07 08	21 24 28	06 07 08	23 27 31	o6 o7 o8	26 30 34	06 07 08	28 33 38	06 07 08	31 36 42	06	49
1	12	11 12 13	17	11 12 13	22	11 12 13	23 25 28	11	24 27 29 32 34	11 12 13	30 33 36	11	34 38 41	11 12 13	38 42 47	12	43 47 52	11 12 13	48 52 58	11 12 14	52 57 04	11	58 03 10	12 13 14	10
	16	16	28	17	32	17	37	17	37 40 42 45 48	17	45 48 51	17	51 54 57	18	57	117	03 07	17	15	17	18 23 28	18	25 31 37	17 18 19	40
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	21	21 22 23	35 37 38	21 22 23	43 45	21 22 23	45	21 22 23	51 53 56 *59 29	23	04	22	12	22 23 24	20	23	29	22 23 24	34 39 44	22 23 24	50	24 25	55 01 07	23 24 25	1

A TABLE of Amplitudes, from the Latitude 25 deg. oo min. to the Latitude 36 deg. either North or South.

	1		1	1	1		45		1				1						1						-
Degrees of		2	5	1	6	2	7	2	8	2	9	3	0	3	1	3	2	3	3	3	4	3	5	3	6
. c		D	М	D	M	D	M	D	М	D	М	D	M	D	М	D	М	D	м	D	М	D	М	D	M
	2	)1 )2	06	01	07	01	07	01	08	01	08	01	18	01 02	10	00 01 02	10	01	23	02	12	01	13	01	1 2
																04									
	7 8	o6 o7 o8	37 43 50	06 07 08	41 48 54	05 07 08	44 51 59	06 07 09	48 56 04	06 08 09	52 00 09	06 08 09	56 05 15	97 08 09	10 21	05 07 08 09	04 16 27	07 08 09	ος 21 33	07 08 09	15 27 39	07 08 09	20 33 47	07 08 09	3 5
1	c	11	02	11	07	11	I 4 2 2	II 12	20	11	26 36	I I 12	33 43	11	41 52	11 13 14	48	11	56	12	04	12	13 28	12	2 3
1	13	14	23	14	31	14	38	14	46	14	54	15	03	15	13	15	23	15	33	15	44	15	56	16	0
1	17	17	42 49 56	18	51	18	01	19	20	18	31 41	19	33 43 54	19	45 56 08	17 18 20 21 22	10	19 20 21	11 24 37	19 20 21	39 53	19 20 22	39 54 10	19 21 22	5 1 2
	21 22 23	23 24 25	18	2 2 2	3 3° 4 3° 5 4°	23 24 5 26	4:	25	57	24	32	24 25 26	38	24	43 55 97	23 25 26 27 28	13	25 26 27	18 32 46	25 26 28	51	27	13 29	27 28	3 5

A TABLE of Amplitudes, from the Latitude 37 deg. oo min. to the Latitude 48 deg. either North or South.

		1					T	he	D	)eg	ree	3	of	L	atit	ud	e.	_	-		ı —			-
Degrees Declinati		7	3	8	-	39		10	4	1		42 	•	13		14		1-5		46		47		48
grees of	D	M	D	М	D -	М	D	М	D	М	D.	М	D	М	D	M	D	М	D	M	D	М	D	M
	00	00	-00	00	00	00	00	00	00	00	- 30	00	-00	- 00	- 00	00	20	00	00	- 00	00	00	00	00
	01																							
	02																							
	03																							29
4	05	00	05	05	05	08	05	13	05	18	05	23	05	28	05	34	25	40	05	40	05	52	05	59
5	06	15	06	21	06	26	06	32	06	38	06	44	06	51	06	58	07	05	07	12	07	20	07	20
6	07	31	27	37	07	43	07	50	07	57	08	05	08	13	08	21	08	30	08	39	08	49	08	59
7	08	40	80	54	09	01	09	09	09	17	09	20	99	35	09	45	39	50	10	24	10	10	10	30
9	11	17	11	27	11	37	11	47	11	57	12	09	12	21	12	34	12	47	13	01	13	16	13	3
10	12	32	12	43	12	54	13	05	13	18	13	31	13	44	13	58	14	13	14	28	14	44	15	0:
11	13	49	14	01	14	12	14	25	14	39	14	53	15	07	15	22	15	38	15	56	16	15	16	34
12	15	05	15	18	15	31	15	45	16	00	16	15	16	31	16	48	17	06	17	25	17	45	18	0
13	16	38	16	35 53	16	49	17	24	17	42	17	37	17	55	18	13	18	33	18	54	19	16	19	39
-	-	_	-	-	-	-	-		-		1	-	-	-	-	_	-	-	-	-	-		-	
15	20	14	20	28	20	46	21	05	21	25	21	23	22	08	22	22	22	56	23	23	23	50	24	2
17	21	28	21	46	22	06	22	26	22	47	23	10	23	34	23	59	24	25	24	53	125		25	5
18	22	46	23	05	23	26	23	47	24	10	24	34	24	59	125	26	25	54	26	25	19	57	27	3
19	24	03	24	24	24	46	25	09	25	33	25	58	26	25	26	54	27	25	27	58	28	32	29	0
20	25	2 }	25	43	26	06	26	31	26	56	27	24	27	53	28	23	28	56	29	31	30	07		
21	26	39	27	03	27	27	27	53	128	21	28	50	29	20	29	53	30	27	31	03	31	42	32	
22	27	58	28	23	28	49	29	10	29	45	30	10	130	48	31	22	31	58	32	37	33	18	34	
23,29	129	17	29	43	29	11	30	40	31	11	31	43	132	01	132	40	33	20	34	01	34		35	

ATABLE of	Amplitudes,	from	the Latitude	49 deg.
oo min. to the	Latitude 60 d	leg. eit	her North or	South.

**	1		1	7.2	AHÍ		1	-	ne	ע	egi	ree	1	1	La	titt	lae	•	1		1		1		
Degrees of	Porton	4	9		0	5	1	5	2	5	3	5	4	5	5	5	6	5	7	5	8	5	9	6	0
9 6		<b>D</b> .	М	D	M	D	М	D	M	D	М	D	М	D	М	D	М	D	М	D	М	D	М	D	M
	2 0	23	31 03 34	01	33 06 40	01	35 10 46	01	37 15 52	01	39 20 59	01	42 24 06	03	45 29	00 01 03 05 07	47 34 22	01	50 40	01	53 46 40	01	53	04	00
	78	10	10 42 14	10	55	11	33 09 45	11	24	11	40	10	15 57 41	10	30	08 10 12 14 16	47 35 24	11	04 56 48	11 13 15	18	11	41 41	12 14 16	00
	12	18	28	18	52	17	39 18 57	19 21	44	20	12	18 20 22	57 43 30	19 21 23	15	18 19 21 23 25	56 49 43	20 22 24	29 25 23	21 23 25	04 04 07	21 23 25	43 47 54	22 24 26	3 4
. 1	17	24 26 28	28	25 27 28	03	25 27 29	41	28	21	27 29 30	04	27 29 31	58	28 30 32	43 39	27 29 31 33	3 <sup>2</sup> 3 <sup>1</sup>	30 32 34	24 27 34	33	28	32 34 36	32 53	33 35 38	4 0
	21 22 23	33 34 36	48	33	3 3 20	34 736 538	30	35 37 39	27	38	29	37 39 41	32 26 40	38 40 42	47	37 39 42 44 45	04	41 43 45	27	42	34 59 30	144	40	145	4 3 2

## A TABLE of Amplitudes from the Latitude 61 Deg. 00 Min. to the Latitude 66 Deg. either North or South.

De De			Th	e I	Degr	ees	of	Lati	tud	е.			The Use of the TABLES of Amplitudes.
Degrees of Declination.	6	1	6	2	6	3	6	4	6	5		66	The Amplitude of the Sur or anyStar, is fo many Degree
	D.	M	D	M	D	М	D	M	D	M	D	M	Distance as they Rise or Set from the East or West Point
-	00	00	00	00	00	00	00	00	00	00	00	00	of the Horizon, either North
U.S	02		02		02		02		02		02	27	erly or Southerly.
2	04		04		04	24	04		04		04	55	Note, When the Sun or Star
	06		06	24	06	37	06		97		07	23	hath North Declination, ther
4	08	17	08	32	08	50	09	09	09	30	09	52	the Amplitude found by these Tables must be reckoned from
5	10	21	10	41	11	04	11	28	11	54	12	22	the East toward the North a
6	12	27	12	52	13		13	47	CONTRACT.	11.5	14	53	their Rifing; or from the Well
7	14	34	15	02	15		16		16	- T. C.	17		toward the North at thei
	16		17	14			18		19	13	20	00	Setting.
9	18	49	19	28	20	c9	20	54	21	43	22	37	
						_		-0					clination, then the Amplitude
	20		21	40	1		23		24		25	14	must be reckoned from the East
	23		23	-17	24		25 28		26		27	58	toward the South at their Ri-
	27		28	37	29		30		32		30	44	fing, or from the West toward
A CONTRACTOR	29		31		32		33		34		36	34	the South at their Setting.
- 15	32	16	33	27	34	45	36	11	37	46	39	31	To find the true Amplitud
	34		35	57	37		38		40		42	40	by the Tables.
17	37	05	38		40	05			43		45	58	Look for the given Latitude
18	39		41	10	42	54	44	49	46	59	49	26	at the Top of the Table, and
19	42	11	43	54	45	49	47	57	,0	23	53	11	the Declination in the first
	44		46		48	-	51		54	02		14	Column to the Left-hand and in the Common Angle
	47		49		52	07	54		57		61	47	of Meeting, you will find the
	50		52		55	30	58		62	2 10 40	67	04	Amplitude required, in Do
	53		56		59	24	63		67		73	52	grees and Minutes.
23,29	15	17	58	04	31	22	65	22	70	33	78	25	Brees and Iramates.

Case 1st. When the Latitude and Declination are both given in even Degrees, as for Example. Suppose I would know the Sun's true Amplitude at his Rising, in the Latitude of 40 oo, his Declination being 17 oo N.

Under Latitude 40, and right against Declination 17 I find 22 26, which is the Sun's true Amplitude, to be counted from the East towards the North (because it is at his Rising, and the Declination

is North) that is E. 22 26 N.

Case 2d. When the Latitude is given in even Degrees, and the Declination in Degrees and Minutes, as for Example. Suppose I would know the Sun's true Amplitude at his Setting, in the Latitude of 57 00, his Declination being 11 33 S.

Find his Amplitude as before, for the Latitude 57, and for

the Declination { 11 deg. } which will be { 20 29 } then

fubtract the Lesser from the Greater, the Dist. is 1 56 or 116 m. to which put two Cyphers, and it makes 11600, which Number must be divided by the Number standing against the odd Minutes of Declination (in the following Table) which in this Case is 181, and the Quotient gives the Proportional Parts in Minutes, which Parts are always to be added to the Lesser of the two Amplitudes that you took the Difference of, and the Sum gives the true Amplitude as follows.

181)11600(64 Proportional Parts in Minutes, 740 makes 1 Degree 4 Minutes.

Lesser of the Amplitudes — 20 29
Proportional Parts to be added — 01 04
True Amplitude — W. 21 33 S.
because at Sun-setting, and the Declination South.

Case 3d. When the Declination is given in even Degrees, and the Latitude in Degrees and Minutes, as for Example. Suppose I would know the Sun's true Amplitude at his Rising, in the Latitude 51 14, his Declination being 14 00 S.

Find his Amplitude as before, to 14 Degrees Declination, and for the Latitude  $\begin{cases} 51 & \text{deg.} \\ 52 & \text{deg.} \end{cases}$  which will be  $\begin{cases} 22 & 37 \\ 23 & 08 \end{cases}$  and fubtract

the Lesser from the Greater, the Difference is 0 31 Minutes.

To

To the Difference of Amplitudes found on the foregoing Side, which is 31, put two Cyphers and makes it 3100, which must be divided by the Number standing against the odd Minutes of Latitude (in the following Table) which in this Case is 428, and the Quotient gives the Proportional Parts in Minutes, to be added to the Lesser of the two Amplitudes, as in Case the 2d.

428)3100(7 Proportional Parts in Minutes.

104		
Leffer of the Amplitudes -		22 37
Proportional Parts to be added		00 07
True Amplitude	——Ē	E:22 44 S.

Case 4th. When the Latitude and Declination are both given in Degrees and Minutes, as for Example. Suppose I would know the Sun's true Amplitude at his setting, in the Latitude 49 18, his Declination being 19 41 N.

First find his Amplitude for Latitude 49 Degrees, and Declina-

tion 19 41 (as in Case the 2d) which will be 30 53.

In the same Manner find his Amplitude for Latitude 50 Degrees, and Declination 19 41, which will be 31 35.

Then from the Greater Amplitude \_\_\_\_\_\_ 31 35
Subtract the Leffer \_\_\_\_\_\_\_ 30 53
Remains the Difference \_\_\_\_\_\_ 00 42 Minutes.

Put two Cyphers to this Difference it makes 4200, which must be divided by the Numbers standing right against the odd Minutes of the given Latitude, (in the following Table) which in this Case is 333, the Quotient gives the Proportional Parts in Minutes, to be added to the Lesser of the two Amplitudes, &c.

333)4200(12 Proportional Parts.
870

The Leffer Amplitude

Proportional Parts to be added

True Amp. for Lat. 49 18, and Decl. 19 41 NW. 31 05 N.

R 2

A TABLE of Numbers for finding the Proportional Parts, to the odd Minutes of Latitude or Declination, in finding the Sun's true Amplitude.

Odd	Num- bers.	Odd	Num- bers.	Odd Minutes	Num- bers.	Minutes	Num- bers.
-	6000	16	375	31	193	46	130
2	3000	17	353	32	193	47	127
3	2000	18	333	33	181	4.8	125
4	1500	19	316	34	176	49	122
5	1200	20	300		171	50	120
6	1000	21	285	35 36	166	51	118
7 8	857	2.2	273	37	162	52	115
8	750	2.3	261	38	158	53	113
9	666	24	250	39	154	54	111
10	600	25	240	40	150	55	109
11	545	26	230	41	146	56	107
12	500	27	222	42	143	57	105
1.3	461	28	214	43	139	58	103
14	428	29	207	44	136	59	101
15	400	1 30	200	1 45	133		1

The Use of this Table is to find a Number to divide the Difference of Amplitudes by, in order to find the Proportional Parts, when the Amplitudes is required for any Latitude or Declination that is given in Degrees and Minutes, (as in the foregoing Cases) to find which Number, look in some of the Columns under the Title of odd Minutes, for your given Minutes of Latitude or Declination, as suppose for 37 Minutes, and right against that you will find 162, which is the Number required.

#### To find the Variation of the Compass by an Amplitude.

To do this, you must have given both the true and magnetical

Amplitudes.

The true Amplitude is to be found by the Tables us before taught. The magnetical Amplitude is to be found by the Compais, at the Time of the Sun's Rifing or Setting, and is so many Degrees and Minutes as you find it to rise from the East, or to set from the West, either to the Northward or to the Southward: As for Examp. Suppose being at Sea, I find by setting the Sun with my Compass, that he rises 10 deg. 15 min. to the Northward of the East, then the magnetical Amplitude is E. 10 15 N. Or Suppose I find by the Compass, that he sets 14 deg. 12 min. to the Southward of the West, then the magnetical Amplitude is W. 14 12 S.

Then if your true Amplitude, and magnetical Amplitude, are both to the Northward, or both to the Southward, subtract the Lesser

from the Greater, the Remainder is the Variation.

But if one be to the Northward, and the other to the Southward, add them together, and the Sum will be the Variation.

And thus having found how much the Variation is, it is remains in the next Place to find which way it is, that is, whether it be Easterly or Westerly.

Rule, If the Amplitude be taken at Sun-rising, and the magnetical Amplitude be farther from the North than the true Amplitude is, then the Variation is Westerly, but if it be nearer to the North, it is

Easterly.

If it be taken at Sun-setting, if the magnetical Amplitude be farther from the North than the true Amplitude is, then the Variation is Easterly, but if it be nearer to the North it is Westerly, as may be seen by the two foregoing Examples.

By By keeping a Journal is meant, keeping such an Account of the Ship's Way, that at any Time you may be able to know what La-

titude and Longitude the Ship is in.

When a Ship is bound from any one Place to another that lies so far from it, that she is obliged to go out of sight of the Land for any considerable Time, as suppose from England to Barbadoes, then at the Time she leaves the Land, she is said to take her Departure, and that part of the Land, she then leaves, as suppose the Start, the Lizard, the Land's-end, &c. is said to be the Place they take their Departure from. And at the Time of taking such Departure, the Captain or Mate generally takes the Bearing and Distance of that Land (according to his Judgment) and sets it down on the Log-Board, or in the Log-Book against the Time it was taken, thus,

Lizard, N. by W. Distance 5 Leagues. Or, Start, N. N. E. Distance 6 Leagues, &c.

And in the same manner for any other Place, Bearing and Distance,

as you will fee in the first Day's Log, of the following Journal.

The Log-book being mark'd as follows, with Columns for Course, Distance, Northing or Southing, Easting or Westing, Latitude by Dead Reckoning, Latitude by Observation, Meridian Distance, Longitude made, and Longitude in, you are to take Notice.

That in the Column for Course, you are always to set down the Course you have made by your Reckoning for that 24 Hours (that is from the Noon of the Day before, to the Noon of the Day you Work on) the Sea Account being always kept from Noon to Noon.

In the Column for Distance, you are to set down the Distance

made by your Reckoning for that 24 Hours.

In the Column of Northing or Southing, you are to fet down the Difference of Latitude made that 24 Hours, marking the Column with N. if the Difference of Latitude be Northerly, or with S. if it be Southerly.

In the Column of Easting or Westing, you are to set down the Departure made that 24 Hours, marking the Column with E. if the

Departure be Easterly, or with W. if it be Westerly.

In the Column mark'd Lat. by D. R. you are to set down the Latitude you reckon yourself in on that Day.

In the Column mark'd Lat. by Obs. you are to set down the Latitude you find yourself to be in by Observation, if you have one, if not, then let it stand open.

In the Column for Mer. Dist. you are to set down (in Degrees and Minutes) how much Departure you have made in all, from the

Place you took your Departure from.

In the Column of Long. made, you are to fet down (in Degrees and Minutes) how much Difference of Longitude you have made in all from the Place you took your Departure from.

In the Column of Long. in, you are to fet down what Longitude

you find yourfelf to be in on that Day by your Reckoning.

Note, The Account of Longitude made, being what is always kept in His Majesty's Navy. And the Account of Longitude in, being most generally kept on Board the Merchant Ships: I shall in this Treatise shew how to keep them both, and shall leave it to the Practitioner's Choice which he will make use of, they both being equally true, and there being no Occasion to keep more than one of them.

And not having (I think) given a fufficient Account of Things that are to be fet down in the feveral Columns, I shall lay down these few necessary Rules following, and then proceed to shew how they are all to be found, or the Method of Working a Days Work at Sea.

Rule 1st, Variation, if there be any, (as most commonly there is,) must be allowed upon all Courses steered, and upon all Bearings, &c. that are taken by the Compass, that is, if it be Easterly Variation it must be allowed to the Right-hand: But if Westerly Variation, then to the Lest-hand of the Course or Bearing: Supposing your self placed in the Center of the Compass, and looking directly forward to the Point you are to allow the Variation from.

Example. Suppose I steer SW. and there is one Point Westerly Variation, then my true Course will be SW. by S. or suppose I set a Point of Land, and find it to bear by my Compass ESE. and I know there is half a Point Easterly Variation, then the true Bearing is SE. by E. ½ E.

Rule 2d, Lee-way (which I shall not here describe, because sufficiently known to every Seaman) must be allowed to be the Righthand of the Course steer'd, when the Larboard Tacks are Aboard, and to the Lest-hand when the Starboard Tacks are Aboard.

Ex-

Example. Suppose I steer N. E. by E. with my Larboard Tacks Aboard, and make one Point Lee-way, then my Course made good is E.N.E.

Rule 3d. Lee-way and Variation, when they are both to be allow'd one way, that is, both to the Right-hand, or both to the Left, add them together, and allow their Sum the same way they were to be allow'd.

But if they are to be allow'd one to the Right-hand, and the other to the Left, subtract the Lesser from the Greater, and allow the Remainder the same way as the Greater of them was to be allowed.

Example. Suppose I steer NNW. with my Starboard Tacks Aboard, and make one Point Lee-way, there being at the same Time half a

Point Westerly Variation, I would know my true Course?

Lee-way to the Left-Hand — 1 Point. Variation to the Left-Hand — 0 ½ Point.

Their Sum to be allowed to the Left-Hand 1 1 Point makes

the true Course NW. by N. 1 W.

Example 2d. Suppose I steer SW. by W. with my Larboard Tacks Aboard, and make 2½ Points Lee-way, and I have 1½ Points Westerly Variation, what is my true Course?

Lee-way to the Right-Hand — 2 ½ Points Variation to the Left-Hand — 1 ½

The Remainder to be allowed to the Right-hand 1 4 Points, makes

the true Courfe WSW. 4 W.

Rule 4th. When a Ship is lying too under a Main-sail, Mizen, &c. then observe how she comes up and falls off, and take the middle between the two Points, and from that allow the Lee-way and Variation, as in Rule 3d.

Example. Suppose a Ship lying too under a Main-fail, with the Starboard Tack Aboard, comes up E. by S. and falls off to NE. by E. there being 1 Point Westerly Variation, and she making 5 Points

Lee-way, what Course does she make good?

The middle between E. by S. and NE. by E. is E. by N. from which allowing 6 Points to the Left-Hand, (by Rule 3d.) the true

Course will be N. by E.

Rule 5th. Currents, the way they set you, and the Distance you suppose you are driven by them, is to be set in the Traverse Table for the Day, as any other Course and Distance.

Ex-

Example, Suppose I try the Current and find it to set W. by N. per Compass i Mile per Hour, the Variation being one Point Easterly, then if I fail in that Current 24 Hours, I fet down in the Traverse Table, as a Course WNW. distant 24 Miles.

Rule 6th, Heave of the Sea, is to be accounted for in the same manner as Currents: As fuppose, there is a great Sea heaving toward the SW. by my Compass, there being 1 Point Westerly Variation. I then fet down in my Travense-Table SW. by S. 1 W. with so much Distance as I judge the Sea has heav'd the Ship.

Rule 7th, At leaving the Land, the opposite Point to the Bearing (with the Variation allow'd upon it) and the Distance you judge yourself from it, must be set down in the Traverse-Table, as a

Course and Distance.

Example, Suppose having 1 4 Westerly Variation, the Start bears by my Compass NNE. distant 4 Leagues: The opposite Point to NNE. is SSW. which with the Variation makes S. 3 W. for the Course to be fet in the Trhverse-Table, distant 12 Miles.

Rule 8th, When you make the Land, the Bearing itself (with the Variation allow'd upon it) and the Diftance you judge yourself from it are to be fet in the Traverse-Table, as a Course and Distance:

This needs no Example.

Note, If you keep only the Account of Longitude made, and would at any Time know what Longitude you are in, look out the Longitude of the Place you took your Departure from, and with that Longitude, and the Longitude made, taken as Difference of Longitude, find the Longitude in, by the Rules in Page 107 and 108. And the Longitude fo found must be counted from the same Meridian that the Tables you look'd out the Longitude of the Place departed from, counts it.

RULES to Correct the Dead-Reckoning by an Observation,

WHEN you have made all the proper Allowances you can, fuch as for Variation, Lee-way, Currents, &c. and still find that your Latitude by Dead-Reckoning will not agree with the Latitude by Observation, within five Minutes, then you must Correct as follows.

#### CASE the First.

If your Course found by Dead-Reckoning be due North, or due South.

Rule, First find the Difference of Latitude (in Miles) between the last Observation, and the Observation on the Day you Correct, which will be the true Difference of Latitude, then will your true Course be the same as the Course by Dead-Reckoning. Your true Distance the same as the true Difference of Latitude. Your Departure 00, and your Meridian Distance, Longitude made, (or Longitude in) will be the same as they were on the Day you had the last Observation.

#### CASE the Second.

If the Course found by Dead-Reckoning be less than 3 Points, or 33 Degrees.

Rule, First find the Difference of Latitude (in Miles) between the last Observation, and the Observation on the Day you Correct, which will be the true Difference of Latitude. Then make your true Course the same as the Course sound by Dead-Reckoning, since the last Observation, and with that Course, and the true Difference of Latitude, find the true Distance and Departure (as in Plain Sailing, Case the 2d,) then to find the Meridian Distance, the Longitude made, and the Longitude in, take the following Rule.

N. B. The Difference of Longitude is to be found by the true Course, and the Meridianal Difference of Latitude between the two Observations (as usual) and the Meridian Distance, Longitude made (or Longitude in) are to be found by adding, or subtracting the true Departure and Difference of Longitude to, or from the Meridian Distance, Longitude made (or Longitude in) on the Day you had the last Observation, which is the Day you always Correct from. Case

#### CASE the Third.

If the Course found by Dead Reckoning, be more than 3 Points, or 33 Degrees, and less than 6 Points, or 67 Degrees.

Rule, First find the Difference of Latitude in Miles between the last Observation, and the Observation on the Day you Correct, which will be the true Difference of Latitude: Then with the Couse found by Dead-Reckoning, since the last Observation, and the true Difference of Latitude, find a new Departure, (by the Second Case of Plain Sailing) add this new Departure to the Departure found by Dead-Reckoning since the last Observation, and take half their Sum for your true Departure: Then you have given the true Difference of Latitude and Departure to find your true Course and Distance, (by Plain Sailing, Case 6th) read here N. B. In Case the 2d.

#### CASE the Fourth.

If the Course found by Dead-Reckoning be more than 6 Points, or 67 Degrees.

Rule, First find the Difference of Latitude in Miles, between the last Observation, and the Observation on the Day you Correct, which will be the true Difference of Latitude, and make your true Departure the same, as the Departure found by Dead-Reckoning since the last Observation: Then you have given the true Difference of Latitude and Departure, to find the true Course and Distance (by Plain

Sailing, Case 2d.) read here the N. B. in Case the 2d.

Note, As the Knowledge of which Case you are to Correct by, depends upon knowing your Course by Dead-Reckoning, and as when you Correct only for one Day, that Course is always found by the difference of Latitude and Departure in your Traverse-Table for that Day; therefore if you are to Correct for a longer Time than one Day, you must take the Northing, Southing, Easting and Westing that you have made for every Day since the last Observation, (or if it be your first Observation, then for every Day from your leaving the Land) minding not to leave out the Difference of Latitude and Departure for the Day you are Correcting on, and bring them into a Traverse-Table; by which you will find the whole Difference of Latitude and Departure, made by Dead-Reckoning since the last Observation, and with that same Difference of Latitude and Departure

#### Rules to Correct the Dead-Reckoning, &c. 132

find the Course made by Dead-Reckoning, then observe which of the foregoing Cases that Course comes under, and Correct by the Rules

for that Case, finding every Thing except the Distance.

And when you have so corrected, you are to set down in your Book only the Latitude by Dead-Reckoning, the Latitude by Obfervation, the Meridian Distance and the Long. made (or Longitude in) and rub out the Course, Difference of Latitude and Departure.

Then you have given the Latitude by Observation on the Day you Correct, and the Latitude by Dead-Reckoning on the Day before it. to find the Difference of Latitude for the last 24 Hours, (by the Rules for Latitude, Page 105.) Also the Meridian Distance on the Day you Correct, and the Meridian Distance on the Day before it, to find your Departure, (by subtracting the Lesser from the Greater, if they are both East, or both West; or by adding them together, if one be East and the other West.) And with that Difference of Latitude and Departure find your Course and Distance, (by the 6th Case of Plain Sailing) which Course, Distance, Difference of Latitude and Departure are to be fet down instead of them you rubb'd out.

#### Rules to find the Meridian Distance.

Case of. If the Meridian Distance on the Day you Work from be East, and if you have fail'd to the Eastward; or if it be West, and you have fail'd to the Westward, then add the Departure to the Meridian Distance, and the Sum will be the Meridian Distance you have made, of the same Name with that you work'd from.

Example Meridian Distance-18 W. Departure Westerly 97 Miles, or- 1 55 W. Meridian Distance made in all -

Case 2d, If your Meridian Distance be East, and the Departure be Westerly; or if the Meridian Distance be West, and Departure Easterly, then subtract the Lesser from the Greater, the Remainder will be the Meridian Distance you have made, of the same Name with the Greater of the two.

Example 1st.	Meridian Distance————————————————————————————————————	7	34 16	w.
	Meridian Distance made in all	6	18	w.
Example 2d.	Meridian Distance-	1	34	w.
	Departure Eafterly —	3	17	
	Meridian Distance made in all	1	43	E.

A

# JOURNAL

OF

A VOYAGE from ENGLAND

TOWARDS

MADERA

## 134 A Journal from England towards Madera.

Н	K	HK	F	Courfes	Winds	Lee- way	Transactions, Thursday May the 1st, 1762.
4 6	The	Start	N	. by E.	dift. 6 1	Leag.	Moderate Gales and fair Weather, at 6 (p. m.) the
8	4 4 5	ı		SW.bW.	N E.		Start bore as per Log. from which I take my Departure, it being in the Latitude
2 4 6	5 5 5	1		s.w.			3 47 W. from London.
8	5 5 6	1					Variation 14 Point W.erly.

The Manner of working this Day's Work.

The opposite Point to the Bearing of the Land is S. by W. which with the Variation allow'd upon it (as before taught) makes S. \(\frac{1}{4}\) E. and Distance from the Land 6 Leagues, or 18 Miles, which are to be set down for the first Course and Distance in the following Traverse Table.

Then the first Course steer'd being SW. by W. the Variation allow'd upon it will make it SW. by S. & W and the Sum of all the Distances from 8 a Clock where that Course begins, to 2 a Clock where it ends, being 18 Miles and a half, I double that Sum, because the Book is mark'd only for every Two Hours) and it makes 37 Miles for the Distance belonging to that Course. But if the Book had been mark'd for every Hour, as it is in the Navy, and Aboard the East-India Ships, then I must have taken the Sum without doubling it for the Distance, and in the same Manner I reckon the other Course and Distance; all which will be as in the following Traverse-Table.

And then every Thing being found as on the other Side, I set them down in their proper Columns as above.

Course

Courfes.	Dift.	N.	S. 1	E.	W.
S. \(\frac{1}{4}\) E.	18		18.0	0.9	
SW. by S. 3 W.	37		27.4		24.8
SSW. 3 W	56		48.0		28.8
Difference	of Latiti	ide S.	93.4	9.9	53.6
					0.9
	ľ				52.7

Dep. W.

The feveral Courses and Distances in this Table, being look'd out and cast up as in the Rules for Traverse Sailing, (Page 52) I find my Difference of Latitude to be 93 Miles and 4 Tenths, and my Departure 52 Miles and 7 Tenths: Then I mark down (upon my Slate, or the Paper that I work upon) every Thing that is to be found, and as I find what they come to, I fet against them as follows.

Distance — 108 Miles Diff. of Lat. — 93 S. Departure By Latitude by D.R. 48 34 N Latitude Observation D.R. / Meridian Distance 00 53 W. Longitude made 01 22 W Longitude in

Course --- S. 30 00 W. Because the Diff. Lat. is S. and the Depar. W. Note, When the Tenths in any Side are more than 5, or half a Mile, you must call that Side 1 Mile more than you found it to be; but when they are less than 5, then you need take no Notice of them. As in this Case the Diff of Lat. being 93.4 I reject the 4 Tenths, and call it only 93 Miles, and the Dep. being 52.7, instead of the 7 os og W. Tenths I put I Mile to it, and call it 53 Miles.

But when you take the Difference of Latitude and Departure to find the Course by, then take them in Miles and Tenths,

Then in the first Place, with my Difference of Latitude 93.4, and my Departure 52.7 (as Taught in Plain Sailing, Case the 6th) I find my Course to be 30 Degrees, and my Distance 108 Miles, which I set down against Course and Distance as above.

Second, For the Latitude by D. R. 50 07 N. Take the Latitude fail'd from And the Diff. Lat. 93 Miles, or 1 33 Sub. (asperRules) gives Lat. D.R. 48 34 N. | Day's Dep. which here is o 53 W.

Third, For the Meridian Distance.

Note, The Meridian Distance on the first Day's Work, is always the same as that

Fourth, For the Difference of Longitude. The Meridional Parts of 3485 The Lautude fail'd from Of the Lat. by D. R. 3343

Then I look for my Course 30 Degrees, in the Tables of Diff. of Lat. and Dep. and for the Merid. Diff. of Lat. 142, in fome of the Diff. of Lat. Columns belonging to that Courfe, the Dep. 82 which anfwers to that Diff. Lat. is my Diff. Long.

Fifth, For the Longitude made.

Meridional Difference of Lat.

The Long. made on the first Day's Take the Longitude sail'd from Work, is always the same as that Day's And the Diff. Long 82 Miles, or Diff. of Long. which here is - 1 22 W. Sub (as perRules) gives Lon. in

Sixth, For the Longitude in. H.

н	K	нк	F	Courfes	Winds	Lee-	Transactions, Friday May the 2d, 1762.
2	6			sw.bw.	N.	-	
4	5	1					Moderate Gales and fair
6	5	3	1		NW.		Weather, at 8 (a. m.) faw
8	5	)					a Ship to the Northward.
10	4	1		S.W.			
12	4	1					
2	4	T					
6	4	1	1				
6	4	1					
8	5			SWb S.	WNW		
10	4	1					Variation 14 Point W.erly.
12	4					9	
Cou	ries	Dift.	S.	W Lat. b	y D.R. L	at. by O	b. Mer. Dift. Lon. made Lon. in
33	woo			61 46			1 54W 2 55W 6 42V

The Variation being allow'd, and the Distances summ'd up as before, the Traverse-Table will be as follows.

Course	Dift.	N.	8.	E.	W.
SWb SI W	43		31.9		28.9
SSW 3 W	45		38.6		23.1
S by WaW	27		25.4		0.1

First, With my Difference of Latitude 95.9 and Departure 61.1 (by Plain Sailing Case 6,) I find my Course to be 33 deg. and my Distance 114 Miles.

Second, For my Latitude by D.R.

Take the Latitude in yesterday 48 34 N.

And my Diff. Lat. 96 Miles, or 1 36

Gives the Latitude by D.R.—46 58 N.

Third, For the Meridian Distance,
Take the Mer. Dist. yesterday o 53 W.
And the Departure to-day \_\_\_\_\_\_ 1 01

Oives the Meridian Distance \_\_\_\_\_ 1 54 W.

	Courfe S. 33 00 W
	Diftance 174 Miles
	Diff. of Lat g6 S.
By	Departere 61 W.
	Latitude by D.R. 46 38 N.
DR.	Latitude by Observation
	Meridian Diftance - 1 54 W.
	Longitude made 2 55.W
and the same	Longitude in — 6 42 W

Fourth, For the Diff. of Longitude.

Take the Mer. Parts of yest. Lat. — 334

And of the Latitude to-day — 320

Gives the Mer. Diff. of Latitude — 14

with which and the Course (as in the first Day's Work) I find my Diff. of Longitude to be 93 Miles.

Fifth, For the Longitude made.

Take the Long. made yesterday 1 22 W.

And the Diff. of Long. to-day 1 33

Gives the Long. made to-day 2 55 W.

Sixth; For the Longitude in,

Take the Long. in yesterday 5 09 W.

And the Diff. of Long. to day 1 20 W.

And the Diff. of Long. to day 1 33

Gives the Longitude in 6 42 W.

Н	K	нк	F.	Courfes	Winds	Lee- way	May the 3d, 1762.
2 4 6	4 4 4			SW	WNW	-61	Moderate Gales and Cloudy.
8 10 12	54 64	I I		SWbS	W byN	1/2	
2 4 6	4 34 34	1		In 1ft Re SSW	ef both T	op-fails I	
8 10 12	34	1				1.7	Variation 1 Point W.erly.
Co	urfe	Dift	S.	W Lat.	byD.R.L	at. byO	b. Mer. Dift. Lon. made Lon. in
S 14	ooW	97	95	24 45	23 N		2 18W 3 29W 7 16W

The Lee-way and Variation being allow'd, as before taught, the Traverse-Table will be as follows.

Courfes	Dift.	N.	S.	E.	W.
SW. by S.	24		20.0		1.33
S by W I W	36		34.5		10.4
South	40		40.0	200	
			94.5		23.7

First, The Course and Distance found (by Plain-Sailing Case 6.) as before will be as in the other Column.

Third, For the Meridian Distance,
Take the Mer. Dist. yesterday 1 54 W.
And the Departure to-day — 0 24
Gives the Meridian Distance — 2 18 W.

in oc a	3 10110113.			
	Course S.	14	00 V	V.
	Distance —	97	Mile	s
	Diff. of Lat.—	95	S.	
By	Departure —			1
	Latitude by D.R.	45	23 N	1.
D.R.	Lat. by Observation			
	Meridian Distance		18 V	
	Longitude made			
	Longitude in-	7	16 V	٧.

Fourth, For the Diff. of Longitude.

The Mer. Parts of yesterdays Lat. — 3200
Of to-days Loticude — 3063
The Meridian Difference of Latitude 137
with which and the Course, (as before) I find the Difference of Lon. to be 34 Miles.

Take the Long. made yesterday 2 55 W. And the Diff. of Long. to-day 0 34 W. Gives the Longitude made 3 29 W. Sixth, For the Longitude in,

Take the Long. in yesterday 6 42 W. And the Difference of Longitude 0 34

Gives the Longitude in \_\_\_\_\_ 7 16 V

T

Th

H	K	нк	F.	Courfes	Winds	Lee- way	Transaction, Monday May the 4th, 1762.			
2	4			S	WSW	1	Moderate Cales and II-			
6	4	1					Moderate Gales and Hazy the first Part, the latter fresh			
8	4			In 2d Ree	f both T	op-fails	Gales with Rain.			
10	.4			SSE.	SW.	1 ½				
	4		_	•		-				
2 4	4						•			
6	4			Handed t	he Fore T	op-fail				
8	4	-		S by E	SW byW	1 2				
10	4 3	I			Tack'd		Variation 1 Point W.erl			
Cou	rses	Dift.	s	E Lat. b	yD.R. L	at. byO	b. Mer. Dift. Lon. made Lon. in			
39	oo E	93	72	60 44	11 N.		1 18W 2 07W 5 54W			

The Ship having her Starboard Tacks aboard, when the Leeway and Variation are allow'd (as before taught) the Traverse Table will stand as follows.

Courfes	Dift	N.	S.	E.	W.		Course — S. 39 00 E. Distance — 93 Miles
SSE	33		30.5	12.6			Diff. of Lat. 72 S.
SE ½ E	40		25.4	30.9		Ву	Departure———————————————————————————————————
SE	23 16.3 16.3 D	D.R.	R.   Latitude Observation				
			72.2	59.8			Meridian Distance 1 18 W Longitude made 2 7 W
							Longitude in 5 54 W

Having been very particular in explaining the Manner of working a Day's Work (in the three foregoing Days) and as all Days Works, where there is no Correction wanting, are to be work'd from the Difference of Latitude and Departure found by the Traverse Table (as before) I have here only set down the Traverse Table, and what all the other Things come to, and have left the finding of them to exercise the Learner.

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Н	K	нк	F.	Courfes	Winds	Lee- way	Transaction, Monday, May the 5th, 1762.
2 4 6	4 3 3			NWbyW	SW byW	2	Fresh Gales and Rain all these 24 Hours.
8 10 12	3 3 3	ı		Hand N N W	l Iain To  WSW		
4 6	3 3 3	I					
8 10 12	3 3 3			NW byN	W by S	$3^{\frac{1}{2}}$	Variation 1 Point W.erly.
Co	urſe	Dift.	N	W Lat.	byD.R.L	at. byO	b. Mer. Dift. Lon. made Lon. in
N29	ooW	75	65	36 45	16 N		1 54W 3 00W 6 47V

The Ship having her Larboard Tacks Aboard, when the Lee-way and Variation allow'd, the Traverse-Table will stand as follows.

Courfes	Dift.	N.	S.	E.	W.		Course—N. 29 00 W. Distance—75 Miles
NW	32	22.6			22.6		Diffance 75 Miles Diff. of Lat. 65 N.
NNW	33	30.5		Bern	12.6	By	Departure - 36 W.
N 1 W	12	119			1.2		Latitude by D.R. 45 16 N.
		65.0			36.4		Lat. by Observation Meridian Distance 1 54 W.
							Longitude made 3 00 W. Longitude in 6 47 W.

#### To find the Courfe.

Note, In this Case the Difference of Latitude being just 65 Miles without any Tenths, after you have put two Cyphers to the Departure, you must not divide it by 65, but by 650, the Cyphers being put to supply the Place of Tenths, as directed in the Rule for Plain-Sailing, see the Work.

T 2

Н	K	Н	K	F	Courfes	Winds	Lee- way	Transactions, Tuesday, May the 5th, 1762.
2	3				WNW	S W	3 1/2	Hard Gales and Squaly
6	3	-			Handed	the Fo	re-fail	with Rain.
8	L	ay to	00,	uj	NW.	off N.	5	
10	Dri	ft 1	1 2	M	iles per 1	Hour.		
2 4 6				Up	NbyW off	NEbyN		
8 10 12					NNW. o	The second second		Variation 1 Point W.erly.
Co	urfe	Di	ſŧ.	N	E Lat. b	y D.R. L	at. byOl	Mer. Dift. Lon. made Lon, in
N 8	ooE	3.5	5	34	5 45	50N.		1 49 W 2 53 W 6 40V

Having allow'd the Lee-way, and the Variation upon the first Course, and also from the Middle between what she comes up and falls off, (as taught in the Rules for laying too,) the Traverse Table will stand as follows.

Courses	Dift.	N.	S.	E.	W.		ourse — N. 8 00 Distance — 35 Mil
NW bN ‡W NNE NE by E	18	13.9			11.4	Ey Diff. of Lat.—34 Departure—5 Latitude by D.R. 45 Latitude Observation Meridian Distance 1 Longitude made—2	
	12	11.1		4.6	11.4		eparture 5 E.
	9	5.0		7.5			atitude Observation
NE	6	4.2		16.3			
		34.2					ongitude in—— 6 40
				11.4			
		Dep	artur	e 4.9	E.		

	1.6		
	-	100	
		-4	7
12		4	
-	-	_	

Н	K	нк	F.	Courses	Wind	s Lee- way	Transactions, Wednesday May the 7th, 1762.
4 6	3 3 3			N W WNW			Fresh Gales the first Part, the latter Moderate, with
8 10 12	3 3 3	1 1		Set M N W			fmall Showers.
4 6	3 4 4	1		Set Fo W by S			
8 10 12	4 4 4	1		Out 2d R W.	eef both	Topfails	Variation 1 Point W.erly.
Cou	ırfes	Dift	N	W Lat.	byD.R.	Lat. byO	b. Mer. Dift. Lon. made Lon. in
N <sub>54</sub>	oo W	72	42	58 46	32 N.		2 47W 4 17W 8 04W

Courfes	Dift.	N.	S.	E.	W.
N by W	12	11.8		14	2.3
NW by N	12	10.0			6.7
NNW	21	19.4			8.0
W	32			and a	32.0
WbNłW	9	0.9			9.0
		42.1			58.0

(	Courfe - N. 54 00 W.
	Distance — 72 Miles
	Diff. of Lat. 42 N.
By	Departure—-58 W.
	Latitude by D.R. 46 32 N.
D.R.	Latitude Observation
	MeridianDiftance 2 47 W.
	Longitude made 4 17 W.
	Longitude in 8 04 W.

Н	K	нк	F	Courfes	Winds	Lee- way	Transactions, I bursday May the 8th, 1762.
2	4	1		W byN	SWbS	1	
6	4 4	1		Out 1ft R	eef both7	Topfails	Moderate Gales and thick Hazy Weather.
8	4	1		W.	ISSW.	1 1/2	
10	4	I					
12	4	I					
2	4			W by S	S by W	1/2	
4 6	4 4						
8	4 3	ı		WSW	S	<u>I</u>	Variation 1 Point W.erly.
12	3					2	, mindon 2 2 onic tricily.
Co	urfe	Dift.	S	W Lat. 1	y D.R. L	at byOb	Mer. Dift. Lon. made Lon. in
882	oo W	95	13	95 46	19N.		4 22 W 6 33W 10 20V

Courfes	Dift.	Dift.	Dist.	Dist.	Dist.	Dift.	Dift.	Dist.	Dist.	Dist.	N.	S. 1	E.	W.		Course ————————————————————————————————————
W by N	26	5.1			25.5		Diff. of Lat 13 S.									
$\overline{WbS\frac{1}{2}W}$	27		2.6		26.9	Ey	Departure 95 W Latitude by D.R. 46 19									
WSW <sup>1</sup> / <sub>2</sub> W	32	33 14-1	9.3	1	30.6	D.R.	Latitude Observation									
SW by W	13	13	13		6.1		11.5		Meridian Distance 4 22 Longitude made 6 33							
6.24		5.1	18.0		94.5		Longitude in — 10 20									
	*	1	5:1			1										
Difference	of Lat	itude	12.9													

H	K	нк	F	Courses	Winds	Lee- way	Transactions, Friday May the 9th, 1762.
2	2	1		WSW	- S.		
4	2	1					Little Wind and fmall
6	2	1					Showers of Rain.
8	2						
10	2		1				
12	2						A great Swell from the
2 .	I	I					SW. for which I allow 6
4	1	1	100	SWbW	S by E		Miles
6	I	I					
8	I						
10		1	13				Variation 1 Point W.erly.
12		1					

Courfes	Dift.	N.	S.	E.	W.	1	Course————————————————————————————————————
SWbyW	30		16.7		24.9		Diff. of Lat 19 S
SW	10		7.1		7.1	Ву	Departure 29 W Latitude by D.R. 46 c
NE by N	6	5.0		3.3		D.R.	Lat. by Observation
		5.0	23.8	3.3	32.0		Meridian Distance — 4 5 Longitude made — 7 1
			5.0		3.3		Longitude in 11 o
			18.8		28.7		

Note, In this Day's Work the Swell coming from the SW. heaves the Ship towards the NE. and the Variation allowed upon it makes NE. by N. for the last Course in the Traverse-Table.

H	K	н к	F	Courfes	Winds	Lee- way	Transactions, Saturday, May the 10th, 1762.
4 6				Calm			Tried the Current and
6							found it to set W.S.W. I
8		N. V.					Mile per Hour, at which
10							Rate I allow it for this 24
12							Hours.
2	4						Zenith Distance 27 52 S.
4 6							Declination —— 17 41N.
8	1	1		SSW	W.		
10	2		1				Variation 1 Point W.erly.
12	2	1					

Courfes	Dift	N.	S.	E.	W.
S by W	4.00		10.8		2.1
SWbW	24		13.3		20.0
			24.1		22.1

Course — S. 42 00 W. Distance — 32 Miles Dist of Latitude 24 S. Departure — 22 W. Latitude by D.R. 45 36 N. Latitude Observ. 45 33 N. Meridian Distance 5 13 W. Longitude made 7 50 W: Longitude in — 11 37 W.

Note, The Current setting W.S.W. 1 Mile per Hour, I allow the Variation upon it, which makes it SW. by W. and set it in the Traverse Table, with 24 Miles Distance, as above.

Н	K	нк	F.	Courfes	Winds	Lee- way	Transactions, Sunday May the 11th, 1762.		
4 6	3 3 4	1.		S by W	W by S		Moderate Gales and fair Weather, at 9 (a. m.) spoke		
8 10 12	4 4 4			•			with a Ship from Barbadoe and bound for London.		
4 6	4 4 4								
8 10 12	4 4 4						Variation r Point W.erly.		
Cot	ırfe	Dift	s	Lat. b	yD.R. La	t. byOt	Mer. Dift. Lon. made Lon. in		
Sou	oth	103	103	- 44	00 N. 43	50N	1. 5 13W 7 50W 11 37V		

fince	Course — South Distance — 93 Miles Diff. of Lat. — 93 Departure — 00 Latitude by D.R. — 44 00N. Latitude Observation 43 50N.	Cor- rected	Course————————————————————————————————————
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In this Day's Work, there being 10 Miles Difference between the Latitude by Dead-Reckoning and Observation, I am to Correct, and therefore I do not find the Meridian Distance, &c. by (D.R.) as I did when there was no Correction; but I mark them all down again as above, and Correcting (as in Case the First, of the Rules for Correcting) because my Course by D.R. since the last Observation was due South, I set them all down, as in the above Correction.

Н	K	нк	F.	Courfes	Winds	Lee- way	Transactions, Monday, May the 12th, 1762.
2	4			SWbS	WNW		
4 6	4	I					Moderate Gales and
6	4	τ					fine clear Weather.
8	4	1					
10	4						
12	4						
2	4	1	.7.				
4	4	1		SSW			
6	4						
8	4						
10	4						Variation 1 Point W.erly.
12	4	I					
Co	urfe	Dift.	S	W Lat. 1	yD R. L	at. byOl	b. Mer. Dift. Lon. made Lon. in
18	ooW	112	106	35 42	13 N 4	2 04 1	N 5 48W 8 37W 12 24V

Courfes	Dift.	N.	S.	E.	W.		Course S. 18 00 W Distance 112 Mile
SSW	60		55.4		23.0		Diff. of Lat 106 S.
S by W	42		41.2		8.2	Cor-	Departure 35 W. Latitude by D.R. 42 13 N
			96.6		31.2		Lat, by Observation 42 04 N

Having found as far as to the Latitude by Dead-Reckoning and Observation, I see they differ 9 Miles, therefore I Correct (by Case the 2d.) because my Course found by Dead-Reckoning since the last Observation, is less than 33 Degrees, and the result is as above.

Н	K	нк	F.	Courfes	Winds	Lee- way	Transactions, Tuésday May the 13th, 1762.
4 6	4 4 4	1		SW	NW		Moderate and Fair.
8 10 12	4 3 4	1		swьw		an North	
2 4 6	4 3 5	1	•		. N		
8 10 12	3 3 3	III			NE		Variation 3 Point W.erly.
		10000		The state of the s	The state of the s		Mer. Dist. Lon. made Lon. in 6 45W 9 53W 13 40

Courfes	Dift.	N.	S.	E.	W.		Course S. 47 Distance 78
SWb S W	33		26.5		19.7		Diff. of Lat 53
SW 4 W	58		38.9		43.0	Cor-	Departure 57 Latitude by D.R 40
			65.4		62.7	rected	Latitude Observation 41 Meridian Distance 6

Ву	Course ————————————————————————————————————	New Departure 51 ] Departure by D.R 63
fince	Diff. of Lat. — 65 S. Departure — 63 W.	Their Sum-114
last Obser.	Latitude by D.R. — 40 59N. Latitude Observation 41 11N.	½ Sum, or True Dep. 57 Miles

In this Case, the Course by D.R. since last Observation being more than 33, and less than 67 Degrees, I corrected by Case the 3d.

U 2

Н	K	HK	F.	Courfes	Winds	Lee- way	Transactions, Wednesday, May the 14th, 1762.
2	4			W	SE		
4	4						Cloudy the first Part, the
6	4						latter Moderate and Fair.
8	4						*
10	4		1		E		
12	4						
2	4						
4	4						
6	4					100	
8	3	1					
10	3	I					Variation 1/2 Point W.erly.
12	3	1			NNE		
Col	arfe	Dift	-	W Lat. b	yD.R.L	t. byOb	Mer. Dift. Lon. made Lon. in
We	eft	93	=	93 41	02 N 4	IIIN	8 18W 11 56W 15 43V

Courses		S.	E.	W.
$\overline{WbS_{\frac{1}{2}}W}$	93	9.1		92.6
		 ff L	at.	Dep.

Corrected by Case the 4th, the Course by D. R. being more than 6 Points.

fince	Course — W. by S. ½ W. Distance — 93 Miles Disterence of Lat. — 9 S. Departure — 93 W. Latitude by D.R. — 41 02 N. Latitude Obser. — 41 11 N.	Cer- rected.	Distance — 93 Miles Diff. of Lat. — 00 Departure — 93 W. Latitude by D.R. 41 02 N. Lat. by Observation 41 11 N. Meridian Distance — 8 18W. Longitude made — 11 56W. Longitude in — 15 43W.
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Note, When the Course is due East or due West, as in this Case, then the Difference of Longitude cannot be found by the Course, and Meridional Difference of Latitude as before, but must be found as follows; look in the Tables of Difference of Latitude and Departure, for the nearest Degree to your Latitude, which here is 41, and in some of the Difference of Latitude Columns belonging to that Degree find your Departure, which in this Case is 93, the Distance answering to that which is 123, gives your Difference of Longitude.

H

Н	K	нк	F	Courses	Winds	Lee- way	Transactions, I bursday May the 15th, 1762.
2 4 6	4 3 3	1		S by W	N.		Little Wind and Hazy all these 24 Hours.
8 10 12	3 3 3			ss w	NW		
2 4 6	3 3 3			S bW ½ W	WNW		
8 10 12	3 3 3						Variation 1/2 Point W.erly.
Co	urle	Dift.	3	W Lat.	by D.R. L	at byO	b. Mer. Dift. Lon. made Lon. in
SII	Noo	76	74	14 39	57N.		8 32 W 12 15W 16 02W

Courses	Dift.	N.	S.	E.	W.	1	Course S. 11 00 V Distance 76 Miles
S <sub>1</sub> W	28		27.9		2.7	1. 33. 53	Diff. of Lat. 74 S.
S b W W	24		23.0		7.0	Ву	Departure14 W. Latitude by D.R. 39 57 h
S by W	24		23.5		4.7	D.R.	Latitude Observation
			74.4		14.4		Meridian Distance 8 32 V Longitude made—12 15 V
							Longitude in 16 02 V

Note, Having in the foregoing Day's Work given an Example to every Case of correcting, (for a single Day) I shall now set down two or three Days Work by D.R. and then shew how to correct them all together by an Observation, that is, how to correct for a longer Time than one Day.

Н	K	НК	F	Courfes	Winds	Lee- way	Transactions, Friday, May the 16th, 1762.
2	3	1		SSW	W by N	10/6	
4	3	1					Little Winds and Cloudy.
6	4						
8	4	and the second	7 7 10				
10	4			S by W	W		
12	3	I					
2	3	1					
4	3	1					
6	3			S	WSW		
8	3						
10	3		1	S bW ½ W	W		Variation 4 Point W.erly.
12	3	1	1		0.0		
Cou	rfe (	Dift.	S.	W Lat. b	y D.R. La	t. byOb	Mer. Dift. Lon. made Lon. in
12 0		83	_		35N.		8 49W 12 38W 16 25V

Courses	Dist.	N.	S.	E.	W.	
S b W <sup>3</sup> / <sub>4</sub> W	30		28.2		10.1	
S 3/4 W	29		28.7		4.3	F
S 1/4 E	12		12.0	0.6		D.
SbW <sup>1</sup> / <sub>4</sub> W	13		12.6		3.2	
			81.5	0.6	17.6	
					0.6	
			Ι	ep.	17.0	

Course -		S. 12	00 W.
Distance -			
Diff. of La			
Departure		- 17	W.
Latitude b			
Lat. by Ol	ervation		
Meridian	Distance	- 8	49W.
Longitude	made -	-12	38W.
Longitude	in	- 16	25 W

Н	K	нк	F Courfes	Winds	Lee- way	Transactions, Saturday May the 17th, 1762.
2 4 6	3 3 3	I I I	S bW &W	W by N		Little Wind and fair Weather.
8 10 12	3 3 3	1				
2 4 6	3 2 3		S by W	w.		
.8 10 12	3 3 3					Variation & Point W.erly.
Co	urfe	Dift		1. 4	at byO	b. Mer. Dift. Lon. made Lon. in
S14	00 W	7 74	72 17 37	23N.		9 06W 13 1W 16

Ву

D.R.

Courfes	Dift.	N.	S.	E.	W.
S by W ½ W	46		44.0		13.3
S 3/4 W	28		27.7		4.1
en en en e		146.9	71.7	1 6	17.4

Course 18 .	117
CourseS. 12	Miles
Distance ——74	ivilles
Diff. of Lat.——72	
Departure17	
Latitude by D.R. 37 Latitude Observation	
Meridian Distance 9	o6 W.
Longitude made - 13	or W.
Longitude in16	48 W.

H	K	H	F	Courses	Winds	Lee-	Transactions, Sunday, May the 18th, 1762.
2	4		77	S by W	W by N	G134 7	
4	4				19-	100	Moderate Gales and Fair.
6	4	1					
8	4						
10	4						
12	4						
2	4			S bW W			
4	4						A company of the second
6	4						
8'	4	7-17					
10	4						Variation 4 Point W.erly
12	4						

Courles	Dift.	N.	S	E.	W.
S 3 W			47.5		7.0
S by W	48		47.1		9.4
			94.6		16.4

By	Course S. 10 00W.
DR.	Distance - 96 Miles
fince	Diff. of Lat. 95 S.
yester-	Departure - 16 W.
day	Latitude D.R. 35 48 N.
Noon.	Latitude Obser. 35 36 N.

Now being to correct from the last Observation, which was on Wednesday, May 14th, I take the Northing, Southing, Easting and Westing for every Day since, and bring them into a Traverse Table as follows,

By D.R	•
fince the	
last	
Obser-	
vation.	

N.	S.	E.	W.
	74		14
	82		17
	72		17
	95		16
	N.		74 82

Gives Course by D.R. fince last Observ. S. 11.00W.

### [ 153 ]

My Course found by D.R. since the last Observation, being S. 11 co W. which is less than 33 Degrees, I am to correct by Case the 2d, and to find every thing except the Distance, as follows.

#### First, For the true Difference of Latitude.

Take the Latitude last Observation	41	11	N.
And the Latitude by Observation To-day-	35	36	N.
Gives the Difference of Latitude	5	35	
Which multiplied by 60, makes -	33	5M	iles.

#### Second, For the true Courfe.

The Course by D. R. since the last Observation, being S. 11 00W. I set it down for the true Course, as per Rule in Case 2d.

#### Third, For the Departure.

With the true Course 11 Degrees, and the true Difference of Latitude (divided by 2, because too big to be found in the Tables) which makes it 167.5 (by Plain Sailing, Case the 2d) I find the Departure 32.6 which multiplied by the same Number the Difference of Latitude was divided by, viz. 2, gives 65.2 Tenths for the true Departure.

#### Fourth, For the Meridian Distance.

Take the Meridian Distance last Observation -	8	18	W.
And the true Departure ———————	1	05	
Gives the Meridian Distance To-day	9	23	W.

#### Fifth, For the Difference of Longitude.

Take the Meridional Parts of last	
And Meridional Parts of To-days	Observation — 2288
Gives Meridional Difference of Las	itude
With the Half of which -	214

(because the whole is too big to be found in the Tables) and the True Course 11 Degrees, I find the Difference of Longitude 41.6, which doubled because the other was halv'd gives for the whole Difference of Longitude 83 Miles.

X

Sixth

Cinal	T	11.	T	,
SIXLII,	FOT	The	Longitude	maae,

Take the Longitude made last Observation ————————————————————————————————————	ıtı	56 W.
Gives the Longitude made —	13	19 W.

#### Seventh, For the Longitude in,

And the whole Difference of Longitude -	15 43 W.
Gives the Longitude in	17 06 W.

	Course — S. 11 00 W. Distance — S. 11 00 W. D	
Corrected	Latitude by D. R. —— 35 48 N. Latitude by Observation 35 36 N.	
	Meridian Distance — 9 23 W. Longitude made — 13 19 W.	
	Longitude in 17 06 W	

The Course, Difference of Latitude and Departure as above, being what has been made since the last Observation (which was 4 Days ago) and as it is usual to set them down only as they are made from Noon to Noon, therefore they are to be rubb'd out, and found again as follows;

First, Take the Latitude by D. R. Yesterday \_\_\_\_\_\_ 37 23 N. And the Latitude by Observation To-day \_\_\_\_\_\_ 35 36 N. Gives the Difference of Latitude \_\_\_\_\_\_ 1 47

Second, Take the Meridian Distance Yesterday \_\_\_\_\_ 9 06 W.

And the Meridian Distance To-day \_\_\_\_\_\_ 9 23 W.

Gives the Departure — 0 17

Then with the Difference of Latitude 107, and the Departure 17 Miles, (by *Plain-Sailing*, Case 6.) I find the Course to be 9 Degrees, Distance 108 Miles as above.

Н	K	H	K	F	Courses	Winds	Lee- way	Transactions, Monday May the 9th, 1762.
2 4 6	5 6 6		ı		S by W	N.		By Reckoning I make my Course from the Start to the Island of Madera,
8 10 12	7 7 8		1					S. 32 00 W. Distance 420 Leagues; Meridian Distance and Difference of
2 4 6	8 8 8		ı					At Noon faw the Island of <i>Madera</i> , bearing S.W.
8	8 9		1					by W. Distance 14 Leag. Variation 00.

Courses	Dift.	N.	S.	E.	W.
S by W	182		178.5		35.5
SWbyW	42		23.3		34.9
			201.8		70.4

The Bearing of the Land being SW. by W. distant 14 Leagues, or 42 Miles, I set them in the Traverse Table as a Course, &c.

Course - S.	19	ooW.
Distance -		Miles
Diff. of Latitude	202	S.
Departure ——	70	W.
Latitude by D.R.	32	14 N.
Meridian Distance	10	33W.
Longitude made	14	43W.
Longitude in —	18	30W.
	712	4 5 1

It being Customary upon making the Land, to find what Course and Distance the Ship has made by Reckoning from the Place sail'd from, to the Place arrived at, it is to be done as follows.

CASE the First, When you keep the Account of Longitude in,

With the Latitude and Longitude of the Place you fail'd from; and the Latitude and Longitude you are in by your Reckoning, on the Day you make the Land, find the proper Difference of Latitude, the Meridional Difference of Latitude, and the Difference of Longitude in Miles, and with them find the Course and Distance (as it is shewn at large in Mercator's Sailing) Case the First, Page 55.

X 2

CASE the Second, When you keep the Account of Longitude made.

Then the proper Difference of Latitude, and the Meridional Difference of Latitude, are to be found as before, and the Difference of Longitude is to be found by bringing the Longitude made into Miles, with which proceed as in Case the First.

The Agreement between these two Ways may be seen as follows.

Place I fail'd from 3 47 E.

The Diff. of Longit. 14 43

Which multiplied by — 60

Makes - - 883 Miles

On the same Day my Longitude made was — 14 43 W. Which multiplied by — 60 Makes the Diff. of Lon. 883 Miles the same as in the other Case.

To find the Bearing and Distance of any Place from the Ship, upon any given Day.

Example. Suppose I would know how Madera bore off me, and what Distance on the 14th of May, by the foregoing Journal.

First, Supposing I kept only the Account of Longitude in,
Then, with the Latitude in 41 11 N.

And the Latitude of Madera 32 44 N.

I find the proper Diff. of Lat. 8 27

Which multiplied by 60 makes 507

M. D. L.

And the Lon. Madera 17 26W.

I find the Diff. Lon. 1 43

Which makes — 103 Miles.

Then with that Meridional Difference of Latitude, and Difference of Longitude, I find the Course to be S. 09 00 W. and the Distance 510 Miles, (as in Mercator, Case 1.)

But if I had kept only the Account of Longitude made, (which is

Difference of Longitude) Then,

With the Longitude sail'd from \_\_\_\_\_ 3 47 W:
And the Whole Diff. of Lon. or Lon. made \_ 11 56 W.erly
By the Rules for Longitude (Page 107) I

should have found the Lon. in to be — 15 42 W.

And then I have given the Latitude and Longitude in, &c. as before. I have in the foregoing Journal shewn how to Correct either for a single Day, or for a longer Time, and given Examples of every Case, for correcting from one Observation to another; but as it may happen that you may be some Days at Sea, from the Time of your leaving

leaving the Land before you have an Observation, and that when you get that first Observation you may have Occasion to Correct, (and there being much the same Difference between working the Correction from one Observation to another; and between the first Observation and the Land, as there is between working the first Day's Work and any of the following ones) I shall here give an Example from the foregoing Journal.

# To Correct from the Time of leaving the Land, to the First Observation.

Example. Suppose that in the foregoing Journal, on the 3d of May, I was by Observation in the Latitude 45 10 N. my Latitude by DR, being 45 23 N. my Southing by D.R. 95. and Westing 24.

Now being to correct, and having no Observation before To-day, I must correct from the very Beginning of my Journal, that is, from the Time of my leaving of the Land, by bringing the Northing, Southing, Easting and Westing, (for every Day I have been at Sea) into a Traverse-Table as follows.

By D.R. from the Time of leaving the Land

N.	S.	E.	W.
	93		53
	96	1.7	61
	95	111111111111111111111111111111111111111	24
	IN.	93	

Gives the Course by D.R. from the Time of leaving the Land S. 26.00 W.

The Course found by D.R. from the Time of leaving the Land, being less than 33 Degrees, I am to correct by Case the Second, and to find every thing except the Distance, as follows.

#### First, For the true Difference of Latitude.

Take the Latitude of the Place sail'd from 50 07 N.

And the Latitude in by Observation — 45 10 N.

Gives the true Difference of Latitude - 4 57 or 297 Miles.

#### Second, For the true Courfe.

The Course by D.R. since the Time of leaving the Land being S. 26 00 W. I set down for the true Course, as per the Rules for correcting, Case 2d.

Third

Third, For the true Departure,

With the true Course 26 Degrees, and half the true Difference of Latitude 148.5, (because the whole is too big to be found in the Tables ) by Plain Sailing, Case the 2d. I find the Departure 72.3, which being doubled (because the Difference of Latitude was halv'd) gives 144.6 for the true Departure.

Fourth, For the Meridian Distance,

Whenever you correct from the Time of your leaving the Land, (as you do here) the Meridian Distance will always be the same as the true Departure found by correcting, which in this Case is 145 Miles, or 2.25 W.

Fifth, For the Difference of Longitude,

Take the Meridional Parts of the Latitude fail'd from 3485 And of the Latitude in by Observation - 3044 Gives the Meridional Difference of Latitude -

With the half of which ----(because the whole is too big to be found in the Tables) and the true Course 26 Degrees, (as directed in the first Day's Work, p. 134) I find the Difference of Longitude 107.4, which doubled (because the other was halv'd gives the true Difference of Longitude 214,8.

Sixth, For the Longitude made,

Whenever you Correct from the Time of your leaving the Land, (as you do in this Case) then the Longitude made will always be the fame as the whole Difference of Longitude found by the Correction, which in this Case is 215 Miles, or 3.35 W.

Seventh, For the Longitude in,

Take the Longitude of the Place you fail'd from \_\_\_\_\_ 3 47 W. And the whole Difference of Longitude - 3 35 Gives the Longitude in \_\_\_\_\_\_

The Course, Difference of Latitude and Departure as above, being what has been made in the whole, from the Time of leaving the Land (which is three

Days)

Days) and it is usual to set them down only as they are made from Noon to Noon, therefore they are to be rubb'd out, and found again as follows.

First, Take the Latitude by D. R. Yesterday — 46 58 N.

And the Latitude by Observation To-day — 45 10 N.

Gives the Difference of Latitude — 1 48

Second, Take the Meridian Distance Yesterday — 1 54 W. And the Meridian Distance To-day — 2 25 W. Gives the Departure — — — — 0 31

Then with the Difference of Latitude 108, and the Departure 31 Miles, (by Plain Sailing, Case 6) I find the Course to be S. 1600W. Distance 113 Miles, as above.

Having in the preceeding Journal shewn how to find what Latitude and Longitude the Ship is in, on any Day, I shall in the next Place shew how,

#### By that Latitude and Longitude in, to prick off the Place of the Ship on the Mercator's-Chart.

Rule. Lay a Ruler a-cross the Chart, in the Latitude your Ship is in, then look upon the Equinoctial, or Line marked with the Degrees of Longitude, for the Longitude your Ship is in by your Reckoning, and setting one Foot of your Compasses in that Longitude, take the nearest Distance to some North and South Line, and from where that Line crosses the Edge of the Ruler that lays in the given Latitude, lay off that same Distance (by the Edge of the Ruler) to the Right-hand, if the Longitude you are in was to the Right hand of the North and South Line: Or to the Lest-hand if it was to the Lest, where this falls will be the Place of the Ship. But this will only do when the Longitude mark'd on the Chart and your Reckoning of Longitude in, are both counted from the same Meridian, therefore for a general Rule take the following, viz.

# By the Latitude in, and Longitude made, to prick off the Ship's Place, &c.

Rule. Set one Foot of your Compasses in the Place you take your Departure from, and take the nearest Distance to some North and South Line, and from where that Line salls upon the Equinoctial, or Line mark'd with the Degrees of Longitude, set off that Distance, the same way as the Place lays from it, (that is, to the Right-hand, if the Place lay to the Right-hand of the North and South Line, or to the Lest-hand if it lay to the Lest) and make a Mark with a Black Lead Pencil; this Mark will serve to prick off by, till you come to take a New Departure, and then you rub it out, and make a new one, as before.

Then lay a Ruler a-cross the Chart in the Latitude you are in, and taking so many Degrees in your Compasses (from the Line of Longitude) as your Longitude made comes to, set them off from your Black Lead Mark, to the Eastward, if the Longitude made be East, or to the Westward if it be West;

where this falls will be the Longitude the Ship is in by the Chart, from which take the nearest Distance to some North and South Line, and from where that

Line, &c. as in the first Case.

The Ship's Place on the Chart being found as before taught; it remains in the next Place to shew how to find the Bearing and Distance of any Place from the Ship; and First,

#### To find how any Place bears from the Ship.

Lay a Ruler from the Place of the Ship, to the Place you would know the Bearing of, then set one Foot of your Compass in the Center of some Compass near the Ruler, and take the nearest Distance to the Edge of the Ruler; then run one Foot of your Compasses along by the Edge of the Ruler, and observing what Point of the Compass the other comes nearest to, which will be the Bearing required.

#### To find the Distance of any Place from the Ship.

Case the 1st, If the Place be in the same Longitude that the Ship is in, (that is, if it bears due North or due South) then the Difference of Latitude between them, (found as by the Rules for Latitude, Page 105) and turn'd into Miles or Leagues will be the Distance.

Case the 2d, If the Place be in the same Latitude that the Ship is in, (that is, if it bears due East or due West) then take half the Distance between the Ship and the Place, in your Compasses, and setting one Foot (on the Line mark'd with the Degrees of Latitude) in the Latitude the Ship is in, see what Latitude the other Foot will reach to, both above and below it; the Difference between these two Latitudes, (found as per Rules for Latitude) will be the Distance required.

Case the 3d, If the Place be neither in the same Latitude nor Longitude with the Ship, then take the Difference of Latitude between them in Degrees, from the Equinoctial-line, and laying a Ruler from the Ship to the Place, apply one Foot of the Compasses so to the Edge of the Ruler, that the other Foot turn'd about may just touch some East and West Line, that is cross'd by the Ruler, then take the Distance along the Edge of the Ruler, from the Place where the Compasses rested, to the Place where the Ruler crosses the said East and West Line; that Distance measured on the Equinoctial, or Degrees of Longitude, will give the Distance in Degrees, which you may turn into Miles or Leagues, and in the same manner as you find the Bearing and Distance of any Place from the Ship; you may also find the Bearing and Distance of one Place from another.



FINIS.

